STORMWATER MANAGEMENT REPORT VOLUME I

PROJECT SITE: SALMON HEALTH AND RETIREMENT COMMUNITY ARCPUD SPECIAL PERMIT VILLAGE STREET MEDWAY, MASSACHUSETTS 02053

PREPARED FOR: CONTINUING CARE MANAGEMENT, LLC 1 LYMAN STREET WESTBOROUGH, MASSACHUSETTS 01581

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> JUNE 12, 2015 Revised: October 13, 2015

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B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



L'Alarte le/ 12/15 fature and Date

Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development

- Redevelopment
- Mix of New Development and Redevelopment

INTRODUCTION

Coneco Engineers & Scientists, Incorporated (Coneco) has completed a drainage analysis of the subject site, located at 259, 261, 261R, and 263 Village Street in Medway, Massachusetts, the results of which are contained herein. The purpose of this analysis is to quantitatively understand the impacts of the proposed development of the project site on the existing hydrologic conditions and to mitigate said impacts through the implementation of a stormwater management system that utilizes best management practices and is supported by an operations and maintenance plan as well as a long term pollution prevention plan.

STORMWATER MANAGEMENT SYSTEM OVERVIEW

The proposed stormwater management system consists of conventional curb and gutter drainage for the roadways including a series of catch basins, drain manholes and pipe which convey stormwater runoff from the roadway areas to a water quality device before entering the proposed infiltration system which will ultimately discharge any remaining runoff upstream of the bordering vegetated wetlands. Roof runoff from the proposed campus building and the majority of the residential units will be recharged through individual subsurface infiltration chambers. These chambers have been designed to accommodate flows from the 100-year storm event.

As previously mentioned the proposed roadway drainage discharges upstream of the bordering vegetated wetlands via a flared end and level spreader. The catch basins will have 4 foot deep sumps and oil/gas hoods. The deep sumps are intended to remove sediment, and the hoods are intended to remove oil and gas from the stormwater prior to release. The level spreaders have flared end inlets, a depressed center and a level outer rim. The depressed center promotes the removal of any residual sediment while the level outer rim dissipates the energy of the effluent by diminishing the velocity and eliminating the point discharge.

From an environmentally sensitive perspective, the aforementioned measures result in a low impact design that enhances the introduction of surface water into the ground while preserving the natural hydrologic conditions.

METHODOLOGY

Drainage calculations are performed to demonstrate that there is no increase in the rate of runoff from the subject site due to the proposed project. The rate of runoff is compared at a common point, referred to as the design point, for both the pre and post development condition (or the existing and proposed condition in the case of a redevelopment project). The hydrologic and hydraulic model created to analyze the pre and post development condition was developed using the Soil Conservation Service (SCS) Technical Release No. 20 (TR 20, SCS unit hydrograph procedures), SCS Technical Release No. 55 (TR 55, Time of Concentration (T_c) and Curve Number (CN)), SCS Technical Release No. 40 (TR 40, rainfall intensity) and the stormwater detention facilities were modeled using the SCS Storage Indication Method.

<u>Time of Concentration (T_c) </u> - is the time required for stormwater runoff to travel from the most hydraulically distant point in a drainage area or subcatchment to the design point. The T_c is calculated based upon slope, distance, surface cover and type of flow. A longer time of concentration will generally result in a smaller rate of runoff.

<u>Curve Number (CN)</u> - represents the amount of runoff expected from a particular segment of the drainage area. A higher curve number will be less permeable and therefore a larger rate of runoff. The CN is based upon three factors: soil type, soil cover, and cover condition. The soil type is graded A to D; A soil is the post permeable, D is the least. The soil cover (e.g. - vegetated, developed, farmland or impervious) ranges from 30-98, with more permeable soil covers having a lower value. The final factor is the condition of the vegetated soil cover (good, fair or poor), where vegetated cover in good condition is the most permeable and allows the least runoff.

<u>The Hydrologic Soil Group (HSG)</u> for the drainage areas was determined from the Soil Conservation Service Soil Survey of Norfolk County, Massachusetts. The soil survey contains maps which depict the extent of the various soil types. A soil type overlay plan is attached as Figure 6.

<u>Design Software</u> - To assist in the analysis, software entitled HydroCAD, Version 10.0 (developed by HydroCAD Software Solutions, L.L.C.) was utilized. The HydroCAD program calculates the runoff based on rainfall events and watershed characteristics, and produces a runoff hydrograph (a runoff rate versus time curve). If applicable, stage-storage-discharge curves for a specific detention facility are calculated.

<u>Peak Attenuation</u> - The peak rate of runoff at the design points was calculated for the existing and proposed conditions for the 2, 10, 25 and 100-year, 24-hour storm events. The peak rate of runoff was compared for each storm event to determine if there was an increase from the pre to post development condition.

<u>Runoff Volume</u> - The total volume of runoff for the entire site was calculated for the existing and proposed conditions for the 2, 10, 25 and 100-year, 24-hour storm events. The volume of runoff was compared for each storm event to determine if there was an increase from the pre to post development condition.

EXISTING CONDITIONS

Coneco compiled existing and proposed drainage areas from an existing topographic survey. A site visit was conducted to evaluate the existing drainage patterns and watershed areas for the site and the areas surrounding the site, which is located at 259, 261, 261R, and 263 Village Street in Medway, Massachusetts (Assessors Map 69 Lots 13-1, 14, 15-1, and 21). The site is situated on the south side of Village Street between Brookside Road and Charles River Road and is bounded on the west and south by the Charles River. The site is approximately 56.9 acres in size and consists of undeveloped land. Topography generally slopes from northeast to southwest at grades of approximately 0.5 to 10 percent.

There are no Areas of Critical Environmental Concern, Estimated Habitats of Rare Wildlife, or Priority Habitats of Rare Species located on-site. Two Certified Vernal Pools are found near the Charles River on the western side of the site. There are four Bordering Vegetated Wetlands totaling 13.0 acres of land found on site. The total length of Bordering Vegetated Wetlands line is approximately 10,344 linear feet. The site also contains 2,992 linear feet of the bank along the Charles River. The smaller of the two Certified Vernal Pools encompasses 6,055 s.f. of land area, has a 378 linear foot edge and is located approximately 600 feet south of Village Street and 320 feet east of the Charles River. The larger of the two Certified Vernal Pools encompasses 11,436 s.f. of land area, has a 462 linear foot edge and is located approximately 830 feet south of Village Street and 440 feet east of the Charles River. The wetlands lines were delineated by BSC Group on December 11, 12, and 18, 2014. These resource areas were identified in an ANRAD dated February 12, 2015, last revised May 5, 2015 by Coneco and approved via ORAD issued by the Medway Conservation Commission dated 5/21/2015. Both the ANRAD and ORAD are associated with the MassDEP File Number 2016-0845.

The Soil Conservation Service map for the area indicates that the site is made of seven soil types. Please refer to Table 1 for a summary of these soils.

Table 1

Existing Soil Classifications

SOIL MAP UNIT	NORFOLK COUNTY SOIL SURVEY MAP UNIT NAME AND DESCRIPTION	HYDROLOGIC SOIL GROUP
4	Rippowam silt loam, 0 to 3 percent slopes	D
5	Saco silt loam, 0 to 3 percent slopes	D
31A	Walpole sandy loam, 0 to 3 percent slopes	D
70A	Ridgebury fine sandy loam, 0 to 5 percent slopes	D
245B	Merrimac fine sandy loam, 3 to 8 percent slopes	A
260B	Sudbury fine sandy loam, 2 to 8 percent slopes	В
310B	Woodbridge fine sandy loam, 3 to 8 percent slopes	С

PROPOSED CONDITIONS

The proposed development consists of the construction of an Adult Retirement Community Planned Residential District (ARCPUD) consisting of a four story main residence building which has 40 memory care, 60 assisted living and 54 independent living residential units and 15 attached cottages (two bedroom) as well as 48 two bedroom and 8 three bedroom detached cottages, a two story medical office building, and a pavilion. The associated roadways, parking, site utilities, lighting, grading and drainage are also part of the project.

These changes significantly increase the overall impervious area found at the site. However, the proposed stormwater management system has been designed to capture, treat and infiltrate the generated stormwater runoff and meet all 10 of the stormwater standards.

STORMWATER MANAGEMENT STANDARDS REVIEW

As part of this drainage analysis, Coneco has performed an in-depth review of the subject site for conformance with the Massachusetts Department of Environmental Protection's Stormwater Management Standards. The following is a summary of our findings relative to our review of each of the standards. Please note that the actual text of each standard is italicized for clarity.

STANDARD 1: No new stormwater conveyances (e.g. outfalls) may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

The stormwater runoff from the roadway system shall be treated prior to release with deep sump catch basins with hoods. The deep sump will provide an area for sediment to settle out and the hood will provide oil and gas separation. Prior to discharge to the basins, the stormwater runoff will be directed through water quality units. Outlets have been designed to reduce erosion and eliminate scouring within the wetland areas. A plunge pool shall be installed at each discharge point. The plunge pool and level spreader will spread out the runoff over a larger area which slows down the velocity and therefore

reduces scour. The plunge pool will be lined with riprap and be depressed to form a pool which will enhance sediment removal prior to discharge.

STANDARD 2: Stormwater management systems shall be designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates. This Standard may be waived for discharges to land subject to coastal storm flowage as defined in 310 CMR 10.04.

The existing and proposed site conditions were analyzed for the 2, 10, 25 and 100-year 24-hour storm events using the aforementioned methodology (please refer to appendices A and B of this report for HydroCAD output support data). Based on these results, there is no increase in peak discharges for all storm events (refer to Table 2).

<u>Table 2</u>

Peak Rate of Runoff

Design Point: Offsite West

Storm	Existing Conditions		Proposed Conditions		Percent Decrease From Existing		
(in years)	Peak Runoff (CFS)	Total Volume (CF)	Peak Runoff (CFS)	Total Volume (CF)	Peak Runoff (CFS)	Total Volume (CF)	
	(0.0)		(0.0)	(0.)			
2	0.46	2,291	0.40	1,808	13.0%	21.1%	
10	1.51	6,000	1.12	4,203	25.8%	30.0%	
25	2.18	8,389	1.57	5,682	28.0%	32.3%	
100	3.29	12,346	2.29	8,077	30.4%	34.6%	

Design Point: Charles River

Storm Frequency (in years)	<u>Existing Conditions</u> Peak Total Runoff Volume (CES) (CE)		<u>Proposed Conditions</u> Peak Total Runoff Volume (CES) (CE)		Percent Decrease From Existing Peak Total Volume (CF) Runoff (CES)			
2	39.16	211,274	37.81	197,814	3.4%	6.4%		
10	86.05	444,528	80.62	418,121	6.3%	5.9%		
25	113.68	584,111	108.27	548,294	4.8%	6.1%		
100	157.20	806,433	149.08	757,504	5.2%	6.1%		

CLOSED DRAINAGE SYSTEM CALCULATIONS

Rational Method – Sizing pipes for the 25 year storm

The closed drainage system calculations determine the rate of runoff, the time of concentration and the rainfall intensity for the drainage subcatchment. The calculations were performed for a 25-year storm event. The following standards were used:

1. The Rational Formula (Q =CIA) was used to determine the flow to each structure.

Q = Flow cubic feet per second (CFS) C = Runoff coefficients I = Rainfall Intensity (inches per hour) A = Drainage Area (acres)

2. The runoff coefficients used are as follows:

Impervious (pavement and roofs) = 0.85 Grassed/Landscape = 0.40

3. The intensity for each area was determined by the Steel Formula for a 25-year frequency storm. The Steel Formula is:

I = k/(t+b) I = Intensity k = 230 (25 yr) t = Time of Concentrationb = 30 (25 yr)

- 4. The times of concentration were calculated using a spreadsheet which calculates flow time in the pipe with the Manning equation. A minimum time of concentration of five (5) minutes was utilized.
- 5. The Manning's formula was utilized to calculate the capacity of the individual pipes in the closed drainage system. The Manning's formula is:

 $\begin{array}{l} Q = (Ap) \; (1.486/n) \; (s^{1/2}) \; (h^{2/3}) \\ Q = Flow in CFS \\ Ap = Cross-sectional area of the pipe (square feet) \\ n = Roughness coefficient \\ s = slope of the pipe (ft/ft) \\ h = hydraulic radius = area/wetted perimeter (sf/ft) \end{array}$

The closed drainage system as designed is capable of handling the design flow as calculated, as well as maintaining a design velocity of between 2.0 feet per second (fps) and 10.0 fps. Two feet per second is considered "self cleansing velocity", and will prevent the pipes from accumulating sediment. Ten feet per second is considered a safe maximum velocity, to reduce scouring of the pipes. Please refer to Appendix C for the closed drainage system pipe sizing calculation spreadsheet.

STANDARD 3: Loss of annual recharge to groundwater shall be eliminated or minimized through the use of infiltration measures including environmentally sensitive site design, low impact development

techniques, stormwater best management practices, and good operation and maintenance. At a minimum, the annual recharge from the post-development site shall approximate the annual recharge from pre-development conditions based on soil type. This Standard is met when the stormwater management system is designed to infiltrate the required recharge volume as determined in accordance with the Massachusetts Stormwater Handbook.

Standard 3 requires that a certain volume of water be recharged to the site depending on existing soil types and square feet of total impervious area over each soil type. Please refer to Table 3 for a summary of the required recharge.

Hydrologic Group	Volume of Recharge (inches/SF)	Total Impervious Area (SF)	Required Recharge Volume (CF)
А	0.60	57,688	2,884
В	0.35	301,626	8,797
С	0.25	50,370	1,049
D	0.10	114,789	957
	13,688 CF		

Table 3 Recharge to Groundwater

Therefore, the on-site infiltration system must be designed with a minimum infiltration capacity of 13,688 cubic feet if all impervious on site is directed to a recharge system. The proposed design directs 94.5% of the impervious on site to recharge facilities resulting in a minimum infiltration capacity requirement of 14,489 cubic feet. As shown in the attached recharge calculations, this volume is solely by Infiltration Trench 18A (32,018 cf). The remaining infiltration trenches provide an additional infiltration capacity of 63,644 cf. Basin 1 provided 16,904 cf of infiltration capacity and Basin 2 provides 26,745 cf of infiltration capacity. The resultant onsite infiltration capacity of 139,311 cf well exceeds the required 14,489 cf.

Coneco has used the Simple Dynamic method for analyzing the infiltration BMPs. Please refer to Appendix C for this information as well as 72 hour drawdown calculation.

It should be noted that the proposed Infiltration BMPs do not adversely impact nearby wetland resource areas.

STANDARD 4: Stormwater management systems shall be designed to remove 80% of the average annual post-construction load of Total Suspended Solids (TSS). This Standard is met when:

a) Suitable practices for source control and pollution prevention are identified in a long-term pollution prevention plan, and thereafter are implemented and maintained;

- b) Structural stormwater best management practices are sized to capture the required water quality volume determined in accordance with the Massachusetts Stormwater Handbook; and
- c) Pretreatment is provided in accordance with the Massachusetts Stormwater Handbook.

TREATMENT OF SUSPENDED SOLIDS:

Catch basins will be equipped with hoods and four-foot sumps to limit sediment, oils, and grease from being discharged to the drainage system. The Water Quality Units will further reduce total suspended solids (TSS) entering the vegetated detention basins, achieving an 80% removal rate. Please refer to Table 4 – Total Suspended Solids Removal worksheet attached herein for this information.

Runoff from roofs will be considered clean which require no treatment. All other impervious areas will be collected in the closed drainage system which is routed through the proprietary treatment device and detention basin.

Please refer to Table 4 for a TSS removal summary.

Please note that a Long Term Pollution Prevention Plan has been developed as part of the analysis and can be found in Appendix D.

		Outlet: HW-1		
BMP	TSS Removal Rate	Starting TSS Load	TSS Removed	Remaining TSS Load
Deep Sump Hooded Catch Basins	0.25	1.00	0.25	0.75
Stormceptor	0.75	0.75	0.56	0.19
Grassed Swale 0.50		0.19 0.10		0.09
		Total Suspended S	91%	

Table 4 Total Suspended Solids Removal

Outlet: FES-2								
BMP	TSS Removal Rate	Starting TSS Load	TSS Removed	Remaining TSS Load				
Deep Sump Hooded Catch Basins	0.25	1.00	0.25	0.75				
Stormceptor	0.75	0.75	0.56	0.19				
Infiltration	0.80	0.19	0.15	0.04				
	96%							

Outlet: HW-2

BMP	TSS Removal Rate	Starting TSS Load	TSS Removed	Remaining TSS Load		
Deep Sump Hooded Catch Basins	0.25	1.00	0.25	0.75		
Stormceptor	0.75	0.75	0.56	0.19		
Infiltration	0.80	0.19 0.15		0.04		
		Total Suspended Solids Removed:				

Outlet: FES-6

BMP	TSS Removal Rate	Starting TSS Load	TSS Removed	Remaining TSS Load
Deep Sump Hooded Catch Basins	0.25	1.00	0.25	0.75
Stormceptor	0.75	0.75	0.56	0.19
Infiltration	0.80	0.19	0.15	0.04
		Total Suspended S	96%	

WATER QUALITY VOLUME:

See Appendix C for required water quality volume calculations based on impervious area.

Water Quality Volume = Total impervious area of post-development project x 0.5 inches.

Water Quality Volume = 524,473 sf impervious area x0.5 inches/12 inches per foot = 21,853 cubic feet

STANDARD 5: For land uses with higher potential pollutant loads, source control and pollution prevention shall be implemented in accordance with the Massachusetts Stormwater Handbook to eliminate or reduce the discharge of stormwater runoff from such land uses to the maximum extent practicable. If through source control and/or pollution prevention all land uses with higher potential pollutant loads cannot be completely protected from exposure to rain, snow, snow melt, and stormwater runoff, the proponent shall use the specific structural stormwater BMPs determined by the Department to be suitable for such uses as provided in the Massachusetts Stormwater Handbook. Stormwater discharges from land uses with higher potential pollutant loads shall also comply with the requirements of the Massachusetts Clean Waters Act, M.G.L. c. 21, §§ 26-53 and the regulations promulgated thereunder at 314 CMR 3.00, 314 CMR 4.00 and 314 CMR 5.00.

The project site is not a land use with higher potential pollutant loads, per the regulations.

STANDARD 6: Stormwater discharges within the Zone II or Interim Wellhead Protection Area of a public water supply, and stormwater discharges near or to any other critical area, require the use of the specific source control and pollution prevention measures and the specific structural stormwater best management practices determined by the Department to be suitable for managing discharges to such areas, as provided in the Massachusetts Stormwater Handbook. A discharge is near a critical area if there is a strong likelihood of a significant impact occurring to said area, taking into account site-specific factors. Stormwater discharges to Outstanding Resource Waters and Special Resource Waters shall be removed and set back from the receiving water or wetland and receive the highest and best practical method of treatment. A "storm water discharge" as defined in 314 CMR 3.04(2)(a)1 or (b) to an Outstanding Resource Water shall comply with 314 CMR 3.00 and 314 CMR 4.00. Stormwater discharges to a Zone I or Zone A are prohibited unless essential to the operation of a public water supply.

The project site is not within the Zone II or Interim Wellhead Protection Area of a public water supply and does not discharge near or to any other critical area. See Figure 5, Critical Areas.

STANDARD 7: A redevelopment project is required to meet the following Stormwater Management Standards only to the maximum extent practicable: Standard 2, Standard 3, and the pretreatment and structural best management practice requirements of Standards 4, 5, and 6. Existing stormwater discharges shall comply with Standard 1 only to the maximum extent practicable. A redevelopment project shall also comply with all other requirements of the Stormwater Management Standards and improve existing conditions.

The project is not considered a redevelopment project per the regulations and is therefore required to meet all 10 Stormwater Management Standards.

STANDARD 8: A plan to control construction-related impacts including erosion, sedimentation and other pollutant sources during construction and land disturbance activities (construction period erosion, sedimentation, and pollution prevention plan) shall be developed and implemented.

Please refer to Appendix E for the Erosion & Sedimentation Control Plan for to be implemented during the construction phase of this project.

A Stormwater Pollution Prevention Plan (SWPPP) will be prepared before the disturbance of any earth commences on the project site. The SWPPP will be prepared by others per EPA NPDES NOI guidelines and submitted under a separate cover.

STANDARD 9: A long-term operation and maintenance plan shall be developed and implemented to ensure that stormwater management systems function as designed.

Please refer to Appendix F for the Operation and Maintenance Plan for the proposed Stormwater Management System.

STANDARD 10: All illicit discharges to the stormwater management system are prohibited.

To our knowledge, no illicit discharges are made to the stormwater management system. Please refer to Appendix G for the Illicit Discharge Compliance Statement.

CONCLUSION/SUMMARY:

Based on the HydroCAD analysis for the 2, 10, 25 and 100-year storm events, the peak rate of runoff have decreased from the existing to the proposed condition. Furthermore, effluent water quality has been enhanced and widespread infiltration has been introduced to previously uncontrolled areas thereby promoting/preserving the natural hydrologic conditions. In addition to these improvements, all 10 of the DEP Stormwater Standards have been met.

AERIAL MAP



USGS TOPOGRAPHIC MAP



FIRM – FLOOD INSURANCE RATE MAP



NATURAL HERITAGE & ENDANGERED SPECIES HABITATS

Stormwater Management Report June 12, 2015 – REV 10/13/15

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PRIORITY HABITAT OF RARE	SPECIES	CERTI	EIED VERNAL PO	015			
ESTIMATED HABITATS OF RARE WILDLIFE							
 NOTES: 1. AREAS OF ESTIMATED AND PRIORITY HABITATS OF RARE WILDLIFE CAME FROM MASSGIS DATABASE LAST UPDATED OCTOBER 2008. 2. CERTIFIED VERNAL POOL LOCATIONS WERE TAKEN FROM MASSGIS DATABASE ON FEBRUARY 5, 2015. THIS DATA IS UPDATED CONTINUALLY AND SHOWN CONDITIONS MAY VARY FROM THIS DATA. 3. THERE ARE NO AREAS ESTIMATED OR PRIORITY HABITATS OF RARE WILDLIFE ON THE PROJECT SITE. 							
259, 261, 261R, AND 263 VILLAGE STREET, MEDWAY, MA 02053							
CONECO	PREPARED FOR: CONTI MANAC	NUING CARE GEMENT, LLC	PLAN SET: R	EPORT FIGURES			
Engineers & Scientists + First Street, Bridgewater, Massachusetts 02324 PHONE 508-697-3191 OR 800-548-3355; FAX 508-697-5996 WEBSTE: WWX-contecc.com	SCALE 1" = 500'	DATE 6/12/2015	PROJECT NO. 8548.0	FIGURE 4 NATURAL HERITAGE & ENDANGERED SPECIES HABITATS			

CRITICAL AREAS

NOTES: 1. AREAS OF CRITICAL ENVIRONMENTA 2. THERE ARE NO AREAS OF CRITICAL	AL CONCERN WEI	<image/>	HEAD PROTECTION	P ULLY 2014.			
259, 261, 261R, AND 263 VILLAGE STREET, MEDWAY. MA 02053							
	PREPARED FOR: CONTI	NUING CARE	PLAN SET:				
CONECO Engineers & Scientists + FIRST STREET, BRIDGEWATER, MASSACHUSETTS 02324	MANAC SCALE	EMENT, LLC DATE	PROJECT NO. 8548 0	EFURI FIGURES FIGURE 5 CRITICAL AREAS			
PHONE 508-697-3191 OR 800-548-3355; FAX 508-697-5996 WEBSITE: www.coneco.com	I = 200	0/18/2010	0010.0	CINITOAL AIMAD			

SOIL SURVEY MAP - NORFOLK COUNTY



EXISTING DRAINAGE AREAS



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	NO.			VILLAGE STREET MEDWAY MASSACHUSETTS 02053	WESTBOROUGH, MASSACHUSETTS 01581			
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ମ୍ 🗖	8 1.	ED:	4 FIRST STREET, BRIDGEWATER, MASSACHUSETTS 02324	REPORT FIGURES	EXISTING CONDITIONS			
	=100'	TLD SMO	WEBSITE: www.coneco.com					

PROPOSED DRAINAGE AREAS



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	RETIREMENT COMMUNITY	CONTINUING CARE MANAGEMENT, LLC	NO.	DATE	DESCRIPTION	DR/CK	
	VILLAGE STREET	WESTBOROUGH, MASSACHUSETTS 01581					
	MEDWAI, MASSACHUSEIIS 02035						
	PLAN SET:	DRAWNG:					
4 FIRST STREET, BRIDGEWATER, MASSACHUSETTS 02324 $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	REPORT FIGURES	PROPOSED CONDITIONS					
WEBSITE: www.coneco.com							

APPENDIX A

EXISTING HYDROLOGICAL CONDITIONS

2-YEAR STORM EVENT 10-YEAR STORM EVENT

25-YEAR STORM EVENT

100-YEAR STORM EVENT



8548.0 - Salmon Senior Community - Medway - Existing Conditions - REV1

Prepared by Microsoft

HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLC

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Area Listing (selected nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
21,633	70	1/2 acre lots, 25% imp, HSG B (AR, CR)
54,729	80	1/2 acre lots, 25% imp, HSG C (CR)
508,869	85	1/2 acre lots, 25% imp, HSG D (AR, CR)
123,178	61	>75% Grass cover, Good, HSG B (CR, OSW)
39,663	80	>75% Grass cover, Good, HSG D (CR, OSW)
4,799	72	Path, HSG A (CR)
83,393	82	Path, HSG B (CR)
1,145	87	Path, HSG C (CR)
14,267	89	Path, HSG D (CR)
6,183	98	Unconnected pavement, HSG B (CR, OSW)
4,151	98	Water Surface, HSG B (CR)
10,807	98	Water Surface, HSG C (CR)
48,913	98	Water Surface, HSG D (CR)
3,253	78	Wetland, HSG A (CR)
105,317	78	Wetland, HSG B (CR)
147,803	78	Wetlands, HSG C (CR)
235,351	78	Wetlands, HSG D (CR)
91,344	30	Woods, Good, HSG A (CR)
668,542	55	Woods, Good, HSG B (CR, OSW)
36,399	70	Woods, Good, HSG C (CR)
744,147	77	Woods, Good, HSG D (CR)
2,953,886	72	TOTAL AREA

Soil Listing (selected nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
99,396	HSG A	CR
1,012,397	HSG B	AR, CR, OSW
250,883	HSG C	CR
1,591,210	HSG D	AR, CR, OSW
0	Other	
2,953,886		TOTAL AREA

8548.0 - Salmon Senior Community - Medway - Existing Conditions - REV1

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Sub	Ground	Total	Other	HSG-D	HSG-C	HSG-B	HSG-A
Nur	Cover	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)
_	1/2 acre lots, 25% imp	585,231	0	508,869	54,729	21,633	0
	>75% Grass cover, Good	162,841	0	39,663	0	123,178	0
	Path	103,604	0	14,267	1,145	83,393	4,799
	Unconnected pavement	6,183	0	0	0	6,183	0
	Water Surface	63,871	0	48,913	10,807	4,151	0
	Wetland	108,570	0	0	0	105,317	3,253
	Wetlands	383,154	0	235,351	147,803	0	0
	Woods, Good	1,540,432	0	744,147	36,399	668,542	91,344
	TOTAL AREA	2,953,886	0	1,591,210	250,883	1,012,397	99,396

Ground Covers (selected nodes)

8548.0 - Salmon Senior Community - Medway - ExistinType III 24-hr 2-Year Rainfall=3.20" Prepared by Microsoft Printed 10/8/2015 HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLC Page 5

> Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment AR: Abutter Runoff	Runoff Area=449,581 sf 25.00% Impervious Runoff Depth>1.62" Flow Length=2,271' Tc=32.8 min CN=85 Runoff=11.52 cfs 60,817 cf
Subcatchment CR: Charles River	Runoff Area=2,444,000 sf 4.00% Impervious Runoff Depth>0.74" Flow Length=2,023' Tc=29.7 min CN=70 Runoff=27.64 cfs 150,457 cf
Subcatchment OSW: Off Site West Flow I	Runoff Area=60,305 sf 10.16% Impervious Runoff Depth>0.46" Length=200' Tc=13.9 min UI Adjusted CN=63 Runoff=0.46 cfs 2,291 cf
Reach TCR: Charles River	Inflow=39.16 cfs 211,274 cf Outflow=39.16 cfs 211,274 cf

Total Runoff Area = 2,953,886 sf Runoff Volume = 213,565 cf Average Runoff Depth = 0.87" 92.68% Pervious = 2,737,524 sf 7.32% Impervious = 216,362 sf

Summary for Subcatchment AR: Abutter Runoff

Runoff = 11.52 cfs @ 12.46 hrs, Volume= 60,817 cf, Depth> 1.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

A	rea (sf)	CN D	Description		
	1,629	70 1	/2 acre lots	s, 25% imp	, HSG B
4	47,952	85 1	/2 acre lots	s, 25% imp	, HSG D
4	49,581	85 V	Veighted A	verage	
3	37,186	7	5.00% Per	vious Area	
1	12,395	2	5.00% Imp	ervious Are	ea
т.	المربع مرالم	01	Mala alta	0	Description
IC (mim)	Length	Siope	Velocity	Capacity	Description
(min)	(teet)	(ft/ft)	(It/Sec)	(CTS)	
9.3	50	0.0400	0.09		Sheet Flow, Sheet AB
					Woods: Light underbrush n= 0.400 P2= 3.20"
1.5	252	0.0320	2.88		Shallow Concentrated Flow, Wooded BC
					Unpaved Kv= 16.1 fps
0.2	63	0.1111	5.37		Shallow Concentrated Flow, Wooded CD
					Unpaved Kv= 16.1 fps
21.6	1,862	0.0080	1.44		Shallow Concentrated Flow, Wetland/Strea/Pond DE
					Unpaved Kv= 16.1 fps
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River EF
					Unpaved Kv= 16.1 fps
32.8	2,271	Total			


Subcatchment AR: Abutter Runoff

Summary for Subcatchment CR: Charles River

Runoff = 27.64 cfs @ 12.47 hrs, Volume= 150,457 cf, Depth> 0.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

	А	rea (sf)	CN	Description		
		91,344	30	Woods, Go	od, HSG A	
*		3,253	78	Wetland, H	SG A	
*		4,799	72	Path, HSG	A	
	6	646,180	55	Woods, Go	od, HSG B	
		99,421	61	>75% Gras	s cover, Go	ood, HSG B
*	1	05,317	78	Wetland, H	SG B	
*		83,393	82	Path, HSG	В	
		4,151	98	Water Surfa	ace, HSG B	
		55	98	Unconnecte	ed pavemer	nt, HSG B
		36,399	70	Woods, Go	od, HSG C	
*	1	47,803	78	Wetlands, H	ISG C	
*		1,145	87	Path, HSG	С	
		10,807	98	Water Surfa	ace, HSG C	
	7	44,147	77	Woods, Go	od, HSG D	
	_	31,605	80	>75% Gras	s cover, Go	ood, HSG D
*	2	35,351	78	Wetlands, H	ISG D	
*		14,267	89	Path, HSG	D	
		48,913	98	Water Surfa	ace, HSG D	
		20,004	70	1/2 acre lot	s, 25% imp	, HSG B
		54,729	80	1/2 acre lot	s, 25% imp	
		60,917	85	1/2 acre lot	s, 25% imp	, HSG D
	2,4	44,000	70	vveighted A	verage	
	2,3	07.000		96.00% Pei	vious Area	-
		97,839		4.00% impe	ervious Area	a
		55			Shnecled	
	To	l onath	Slone	Velocity	Canacity	Description
((min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Description
	79	50	0.0600	0 10	(010)	Sheet Flow Sheet A-B
	1.0	00	0.0000	0.10		Woods: Light underbrush $n=0.400$ P2= 3.20"
	3.1	330	0.0120	1.76		Shallow Concentrated Flow, Wooded B-C
	0	000	0.0.20			Unpaved K_{v} = 16.1 fps
	18.5	1.599	0.0080	1.44		Shallow Concentrated Flow, Wetland/Stream/Pond C-D
		,				Unpaved Kv= 16.1 fps
	0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River D-E
						Unpaved Kv= 16.1 fps
	29.7	2,023	Total			



Subcatchment CR: Charles River

Summary for Subcatchment OSW: Off Site West

Runoff = 0.46 cfs @ 12.26 hrs, Volume= 2,291 cf, Depth> 0.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

	Area (sf)	CN /	Adj Desc	cription	
	22,362	55	Woo	ds, Good, I	HSG B
	23,757	61	>75%	6 Grass co	ver, Good, HSG B
	6,128	98	Unco	onnected pa	avement, HSG B
	8,058	80	>75%	6 Grass co	ver, Good, HSG D
	60,305	65	63 Weig	hted Avera	age, UI Adjusted
	54,177		89.8	4% Perviou	is Area
6,128 10.16% Impervic				6% Impervi	ous Area
	6,128		100.	00% Uncor	nected
_		-		- ·	
T	c Length	Slope	Velocity	Capacity	Description
(mir	i) (feet)	(ft/ft)	(ft/sec)	(cfs)	
12.	3 50	0.0200	0.07		Sheet Flow, Sheet A-B
					Woods: Light underbrush n= 0.400 P2= 3.20"
1.	4 98	0.0050	1.14		Shallow Concentrated Flow, Wooded B-C
					Unpaved Kv= 16.1 fps
0.	2 52	0.0500	3.60		Shallow Concentrated Flow, Wooded C-D
					Unpaved Kv= 16.1 fps
13.	9 200	Total			

Subcatchment OSW: Off Site West



Summary for Reach TCR: Charles River

Inflow A	Area =	2,893,581 sf,	7.27% Impervious,	Inflow Depth > 0.88"	for 2-Year event
Inflow	=	39.16 cfs @	12.47 hrs, Volume=	211,274 cf	
Outflow	/ =	39.16 cfs @	12.47 hrs, Volume=	211,274 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach TCR: Charles River

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment AR: Abutter Runoff	Runoff Area=449,581 sf 25.00% Impervious Runoff Depth>2.88" Flow Length=2,271' Tc=32.8 min CN=85 Runoff=20.17 cfs 107,880 cf
Subcatchment CR: Charles River	Runoff Area=2,444,000 sf 4.00% Impervious Runoff Depth>1.65" Flow Length=2,023' Tc=29.7 min CN=70 Runoff=65.88 cfs 336,648 cf
Subcatchment OSW: Off Site West Flow I	Runoff Area=60,305 sf 10.16% Impervious Runoff Depth>1.19" _ength=200' Tc=13.9 min UI Adjusted CN=63 Runoff=1.51 cfs 6,000 cf
Reach TCR: Charles River	Inflow=86.05 cfs 444,528 cf Outflow=86.05 cfs 444,528 cf

Total Runoff Area = 2,953,886 sf Runoff Volume = 450,528 cf Average Runoff Depth = 1.83" 92.68% Pervious = 2,737,524 sf 7.32% Impervious = 216,362 sf

Summary for Subcatchment AR: Abutter Runoff

Runoff = 20.17 cfs @ 12.45 hrs, Volume= 107,880 cf, Depth> 2.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN D	Description		
	1,629	70 1	/2 acre lots	s, 25% imp	, HSG B
4	47,952	85 1	/2 acre lots	s, 25% imp	, HSG D
4	49,581	85 V	Veighted A	verage	
3	37,186	7	5.00% Per	vious Area	
1	12,395	2	5.00% Imp	ervious Are	ea
Та	Longth	Clana	Valacity	Conosity	Description
IC (min)	(foot)	Siope		Capacity	Description
(11111)	(leet)	(1711)	(It/Sec)	(015)	
9.3	50	0.0400	0.09		Sheet Flow, Sheet AB
					Woods: Light underbrush n= 0.400 P2= 3.20"
1.5	252	0.0320	2.88		Shallow Concentrated Flow, Wooded BC
					Unpaved Kv= 16.1 fps
0.2	63	0.1111	5.37		Shallow Concentrated Flow, Wooded CD
					Unpaved Kv= 16.1 fps
21.6	1,862	0.0080	1.44		Shallow Concentrated Flow, Wetland/Strea/Pond DE
					Unpaved Kv= 16.1 fps
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River EF
					Unpaved Kv= 16.1 fps
32.8	2,271	Total			



Subcatchment AR: Abutter Runoff

Summary for Subcatchment CR: Charles River

Runoff = 65.88 cfs @ 12.44 hrs, Volume= 336,648 cf, Depth> 1.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

	A	rea (sf)	CN	Description		
		91,344	30	Woods, Go	od, HSG A	
*		3,253	78	Wetland, H	SG A	
*		4,799	72	Path, HSG	A	
	6	46,180	55	Woods, Go	od, HSG B	
		99,421	61	>75% Gras	s cover, Go	ood, HSG B
*	1	05,317	78	Wetland, H	SG B	
*		83,393	82	Path, HSG	В	
		4,151	98	Water Surfa	ace, HSG B	
		55	98	Unconnecte	ed pavemer	nt, HSG B
		36,399	70	Woods, Go	od, HSG C	
*	1	47,803	78	Wetlands, H	ISG C	
*		1,145	87	Path, HSG	С	
		10,807	98	Water Surfa	ace, HSG C	
	7	44,147	77	Woods, Go	od, HSG D	
		31,605	80	>75% Gras	s cover, Go	ood, HSG D
*	2	35,351	78	Wetlands, H	ISG D	
*		14,267	89	Path, HSG	D	
		48,913	98	Water Surfa	ace, HSG D	
		20,004	70	1/2 acre lot	s, 25% imp	, HSG B
		54,729	80	1/2 acre lot	s, 25% imp	, HSG C
		60,917	85	1/2 acre lot	s, 25% imp	, HSG D
	2,4	44,000	70	Weighted A	verage	
	2,3	46,162		96.00% Pei	vious Area	
		97,839		4.00% Impe	ervious Are	a
		55		0.06% Unc	onnected	
	Тс	Lenath	Slope	Velocitv	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.9	50	0.0600	0.10		Sheet Flow, Sheet A-B
						Woods: Light underbrush n= 0.400 P2= 3.20"
	3.1	330	0.0120	1.76		Shallow Concentrated Flow, Wooded B-C
						Unpaved Kv= 16.1 fps
	18.5	1,599	0.0080	1.44		Shallow Concentrated Flow, Wetland/Stream/Pond C-D
		·				Unpaved Kv= 16.1 fps
	0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River D-E
						Unpaved Kv= 16.1 fps
	29.7	2,023	Total			



Subcatchment CR: Charles River

Summary for Subcatchment OSW: Off Site West

Runoff = 1.51 cfs @ 12.21 hrs, Volume= 6,000 cf, Depth> 1.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN /	Adj Desc	ription	
	22,362	55	Woo	ds, Good, I	ISG B
	23,757	61	>75%	6 Grass co	ver, Good, HSG B
	6,128	98	Unco	onnected pa	avement, HSG B
	8,058	80	>75%	6 Grass co	ver, Good, HSG D
	60,305	65	63 Weig	hted Avera	ige, UI Adjusted
	54,177		89.8	4% Perviou	s Area
	6,128		10.1	6% Impervi	ous Area
	6,128		100.	00% Uncor	inected
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
12.3	50	0.0200	0.07		Sheet Flow, Sheet A-B
					Woods: Light underbrush n= 0.400 P2= 3.20"
1.4	98	0.0050	1.14		Shallow Concentrated Flow, Wooded B-C
					Unpaved Kv= 16.1 fps
0.2	52	0.0500	3.60		Shallow Concentrated Flow, Wooded C-D
					Unpaved Kv= 16.1 fps
13.9	200	Total			

Subcatchment OSW: Off Site West



Summary for Reach TCR: Charles River

Inflow /	Area =	=	2,893,581 sf,	7.27% Impervious	s, Inflow Depth > 1	1.84"	for 10-Y	ear event
Inflow	=	:	86.05 cfs @ 1	12.44 hrs, Volume=	= 444,528 cf			
Outflov	v =		86.05 cfs @ 1	12.44 hrs, Volume=	= 444,528 cf,	Atten=	= 0%, La	ag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach TCR: Charles River

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment AR: Abutter Runoff	Runoff Area=449,581 sf 25.00% Impervious Runoff Depth>3.58" Flow Length=2,271' Tc=32.8 min CN=85 Runoff=24.87 cfs 134,096 cf
Subcatchment CR: Charles River	Runoff Area=2,444,000 sf 4.00% Impervious Runoff Depth>2.21" Flow Length=2,023' Tc=29.7 min CN=70 Runoff=88.84 cfs 450,015 cf
Subcatchment OSW: Off Site West Flow I	Runoff Area=60,305 sf 10.16% Impervious Runoff Depth>1.67" _ength=200' Tc=13.9 min UI Adjusted CN=63 Runoff=2.18 cfs 8,389 cf
Reach TCR: Charles River	Inflow=113.68 cfs 584,111 cf Outflow=113.68 cfs 584,111 cf

Total Runoff Area = 2,953,886 sf Runoff Volume = 592,500 cf Average Runoff Depth = 2.41" 92.68% Pervious = 2,737,524 sf 7.32% Impervious = 216,362 sf

Summary for Subcatchment AR: Abutter Runoff

Runoff = 24.87 cfs @ 12.45 hrs, Volume= 134,096 cf, Depth> 3.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

A	rea (sf)	CN D	Description		
	1,629	70 1	/2 acre lots	s, 25% imp	, HSG B
4	47,952	85 1	/2 acre lots	s, 25% imp	, HSG D
4	49,581	85 V	Veighted A	verage	
3	37,186	7	5.00% Per	vious Area	
1	12,395	2	5.00% Imp	ervious Are	ea
Та	Longth	Clana	Valacity	Conosity	Description
IC (min)	(foot)	Siope		Capacity	Description
(11111)	(leet)	(1711)	(It/Sec)	(015)	
9.3	50	0.0400	0.09		Sheet Flow, Sheet AB
					Woods: Light underbrush n= 0.400 P2= 3.20"
1.5	252	0.0320	2.88		Shallow Concentrated Flow, Wooded BC
					Unpaved Kv= 16.1 fps
0.2	63	0.1111	5.37		Shallow Concentrated Flow, Wooded CD
					Unpaved Kv= 16.1 fps
21.6	1,862	0.0080	1.44		Shallow Concentrated Flow, Wetland/Strea/Pond DE
					Unpaved Kv= 16.1 fps
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River EF
					Unpaved Kv= 16.1 fps
32.8	2,271	Total			



Subcatchment AR: Abutter Runoff

Summary for Subcatchment CR: Charles River

Runoff = 88.84 cfs @ 12.43 hrs, Volume= 450,015 cf, Depth> 2.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

	A	rea (sf)	CN	Description		
		91,344	30	Woods, Go	od, HSG A	
*		3,253	78	Wetland, H	SG A	
*		4,799	72	Path, HSG	A	
	6	46,180	55	Woods, Go	od, HSG B	
		99,421	61	>75% Gras	s cover, Go	ood, HSG B
*	1	05,317	78	Wetland, H	SG B	
*		83,393	82	Path, HSG	В	
		4,151	98	Water Surfa	ace, HSG B	
		55	98	Unconnecte	ed pavemer	nt, HSG B
		36,399	70	Woods, Go	od, HSG C	
*	1	47,803	78	Wetlands, H	ISG C	
*		1,145	87	Path, HSG	С	
		10,807	98	Water Surfa	ace, HSG C	
	7	44,147	77	Woods, Go	od, HSG D	
		31,605	80	>75% Gras	s cover, Go	ood, HSG D
*	2	35,351	78	Wetlands, H	ISG D	
*		14,267	89	Path, HSG	D	
		48,913	98	Water Surfa	ace, HSG D	
		20,004	70	1/2 acre lot	s, 25% imp	, HSG B
		54,729	80	1/2 acre lot	s, 25% imp	, HSG C
		60,917	85	1/2 acre lot	s, 25% imp	, HSG D
	2,4	44,000	70	Weighted A	verage	
	2,3	46,162		96.00% Pei	vious Area	
		97,839		4.00% Impe	ervious Are	a
		55		0.06% Unc	onnected	
	Тс	Lenath	Slope	Velocitv	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.9	50	0.0600	0.10		Sheet Flow, Sheet A-B
						Woods: Light underbrush n= 0.400 P2= 3.20"
	3.1	330	0.0120	1.76		Shallow Concentrated Flow, Wooded B-C
						Unpaved Kv= 16.1 fps
	18.5	1,599	0.0080	1.44		Shallow Concentrated Flow, Wetland/Stream/Pond C-D
		·				Unpaved Kv= 16.1 fps
	0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River D-E
						Unpaved Kv= 16.1 fps
	29.7	2,023	Total			



Subcatchment CR: Charles River

Summary for Subcatchment OSW: Off Site West

Runoff = 2.18 cfs @ 12.21 hrs, Volume= 8,389 cf, Depth> 1.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

A	rea (sf)	CN A	Adj Desc	ription					
	22,362	55	Woo	ds, Good, I	HSG B				
	23,757	61	>75%	6 Grass co	ver, Good, HSG B				
	6,128	98	Unco	onnected pa	avement, HSG B				
	8,058	80	>75%	6 Grass co	ver, Good, HSG D				
	60,305	65	63 Weig	Weighted Average, UI Adjusted					
	54,177		89.8	4% Perviou	is Area				
	6,128		10.10	6% Impervi	ous Area				
	6,128		100.0	00% Uncor	nected				
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
12.3	50	0.0200	0.07		Sheet Flow, Sheet A-B				
					Woods: Light underbrush n= 0.400 P2= 3.20"				
1.4	98	0.0050	1.14		Shallow Concentrated Flow, Wooded B-C				
					Unpaved Kv= 16.1 fps				
0.2	52	0.0500	3.60		Shallow Concentrated Flow, Wooded C-D				
					Unpaved Kv= 16.1 fps				
13.9	200	Total							

Subcatchment OSW: Off Site West



Summary for Reach TCR: Charles River

Inflow /	Area =	2,893,581 sf,	7.27% Impervious,	Inflow Depth > 2.42"	for 25-Year event
Inflow	=	113.68 cfs @	12.43 hrs, Volume=	584,111 cf	
Outflov	v =	113.68 cfs @	12.43 hrs, Volume=	584,111 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach TCR: Charles River

8548.0 - Salmon Senior Community - Medway - ExisType III 24-hr100-Year Rainfall=6.70"Prepared by MicrosoftPrinted 10/8/2015HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLCPage 26

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment AR: Abutter Runoff	Runoff Area=449,581 sf 25.00% Impervious Runoff Depth>4.65" Flow Length=2,271' Tc=32.8 min CN=85 Runoff=31.93 cfs 174,253 cf
Subcatchment CR: Charles River	Runoff Area=2,444,000 sf 4.00% Impervious Runoff Depth>3.10" Flow Length=2,023' Tc=29.7 min CN=70 Runoff=125.32 cfs 632,180 cf
Subcatchment OSW: Off Site West Flow L	Runoff Area=60,305 sf 10.16% Impervious Runoff Depth>2.46" ength=200' Tc=13.9 min UI Adjusted CN=63 Runoff=3.29 cfs 12,346 cf
Reach TCR: Charles River	Inflow=157.20 cfs 806,433 cf Outflow=157.20 cfs 806,433 cf

Total Runoff Area = 2,953,886 sf Runoff Volume = 818,779 cf Average Runoff Depth = 3.33" 92.68% Pervious = 2,737,524 sf 7.32% Impervious = 216,362 sf

Summary for Subcatchment AR: Abutter Runoff

Runoff = 31.93 cfs @ 12.44 hrs, Volume= 174,253 cf, Depth> 4.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

A	rea (sf)	CN D	Description		
	1,629	70 1	/2 acre lots	s, 25% imp	, HSG B
4	47,952	85 1	/2 acre lots	s, 25% imp	, HSG D
4	49,581	85 V	Veighted A	verage	
3	37,186	7	5.00% Per	vious Area	
1	12,395	2	5.00% Imp	ervious Are	ea
Та	Longth	Clana	Valacity	Conosity	Description
IC (min)	(foot)	Siope		Capacity	Description
(11111)	(leet)	(1711)	(It/Sec)	(015)	
9.3	50	0.0400	0.09		Sheet Flow, Sheet AB
					Woods: Light underbrush n= 0.400 P2= 3.20"
1.5	252	0.0320	2.88		Shallow Concentrated Flow, Wooded BC
					Unpaved Kv= 16.1 fps
0.2	63	0.1111	5.37		Shallow Concentrated Flow, Wooded CD
					Unpaved Kv= 16.1 fps
21.6	1,862	0.0080	1.44		Shallow Concentrated Flow, Wetland/Strea/Pond DE
					Unpaved Kv= 16.1 fps
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River EF
					Unpaved Kv= 16.1 fps
32.8	2,271	Total			



Subcatchment AR: Abutter Runoff

Summary for Subcatchment CR: Charles River

Runoff = 125.32 cfs @ 12.42 hrs, Volume= 632,180 cf, Depth> 3.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

	A	rea (sf)	CN	Description		
		91,344	30	Woods, Go	od, HSG A	
*		3,253	78	Wetland, H	SG A	
*		4,799	72	Path, HSG	A	
	6	46,180	55	Woods, Go	od, HSG B	
		99,421	61	>75% Gras	s cover, Go	ood, HSG B
*	1	05,317	78	Wetland, H	SG B	
*		83,393	82	Path, HSG	В	
		4,151	98	Water Surfa	ace, HSG B	
		55	98	Unconnecte	ed pavemer	nt, HSG B
		36,399	70	Woods, Go	od, HSG C	
*	1	47,803	78	Wetlands, H	ISG C	
*		1,145	87	Path, HSG	С	
		10,807	98	Water Surfa	ace, HSG C	
	7	44,147	77	Woods, Go	od, HSG D	
		31,605	80	>75% Gras	s cover, Go	ood, HSG D
*	2	35,351	78	Wetlands, H	ISG D	
*		14,267	89	Path, HSG	D	
		48,913	98	Water Surfa	ace, HSG D	
		20,004	70	1/2 acre lot	s, 25% imp	, HSG B
		54,729	80	1/2 acre lot	s, 25% imp	, HSG C
		60,917	85	1/2 acre lot	s, 25% imp	, HSG D
	2,4	44,000	70	Weighted A	verage	
	2,3	46,162		96.00% Pei	vious Area	
		97,839		4.00% Impe	ervious Are	a
		55		0.06% Unc	onnected	
	Тс	Lenath	Slope	Velocitv	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.9	50	0.0600	0.10		Sheet Flow, Sheet A-B
						Woods: Light underbrush n= 0.400 P2= 3.20"
	3.1	330	0.0120	1.76		Shallow Concentrated Flow, Wooded B-C
						Unpaved Kv= 16.1 fps
	18.5	1,599	0.0080	1.44		Shallow Concentrated Flow, Wetland/Stream/Pond C-D
		·				Unpaved Kv= 16.1 fps
	0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River D-E
						Unpaved Kv= 16.1 fps
	29.7	2,023	Total			



Subcatchment CR: Charles River

Summary for Subcatchment OSW: Off Site West

Runoff = 3.29 cfs @ 12.20 hrs, Volume= 12,346 cf, Depth> 2.46"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

	Area (sf)	CN /	Adj Desc	cription					
	22,362	55	Woo	Woods, Good, HSG B					
	23,757	61	>75%	>75% Grass cover, Good, HSG B					
	6,128	98	Unco	Unconnected pavement, HSG B					
	8,058	80	>75%	>75% Grass cover, Good, HSG D					
	60,305	65	63 Weig	hted Avera	ige, UI Adjusted				
	54,177		89.8	4% Perviou	s Area				
	6,128		10.1	6% Impervi	ous Area				
	6,128		100.	00% Uncor	inected				
Т	c Length	Slope	Velocity	Capacity	Description				
(min) (feet)	(ft/ft)	(ft/sec)	(cfs)					
12.	3 50	0.0200	0.07		Sheet Flow, Sheet A-B				
					Woods: Light underbrush n= 0.400 P2= 3.20"				
1.	4 98	0.0050	1.14		Shallow Concentrated Flow, Wooded B-C				
					Unpaved Kv= 16.1 fps				
0.2	2 52	0.0500	3.60		Shallow Concentrated Flow, Wooded C-D				
					Unpaved Kv= 16.1 fps				
13.	9 200	Total							

Subcatchment OSW: Off Site West



Summary for Reach TCR: Charles River

Inflow /	Area =	2,893,581 sf,	7.27% Impervious,	Inflow Depth > 3.34	4" for 100-Year event
Inflow	=	157.20 cfs @	12.42 hrs, Volume=	806,433 cf	
Outflov	v =	157.20 cfs @	12.42 hrs, Volume=	806,433 cf, At	tten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach TCR: Charles River

APPENDIX B

PROPOSED HYDROLOGICAL CONDITIONS

2-YEAR STORM EVENT

10-YEAR STORM EVENT

25-YEAR STORM EVENT

100-YEAR STORM EVENT



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Area Listing (selected nodes)

Area	CN	Description		
(sq-ft)		(subcatchment-numbers)		
21,633	70	1/2 acre lots, 25% imp, HSG B (AR, CR)		
54,729	80	1/2 acre lots, 25% imp, HSG C (CR)		
508,869	85	1/2 acre lots, 25% imp, HSG D (AR, CR)		
28,093	39	>75% Grass cover, Good, HSG A (CR, MC)		
328,741	61	>75% Grass cover, Good, HSG B (CR, IR, MC, OSW, PD)		
758	74	>75% Grass cover, Good, HSG C (CR)		
120,996	80	>75% Grass cover, Good, HSG D (CR, IR, MC, OSW, PD)		
13,560	98	Cottages (IR)		
2,704	80	Path in Resource, HSG B (CR)		
6,129	80	Path in Resource, HSG C (CR)		
9,556	80	Path in Resource, HSG D (CR)		
1,048	80	Path(cover unknown) (OSW)		
205	72	Path, HSG A (CR)		
10,318	82	Path, HSG B (CR)		
3,310	87	Path, HSG C (CR)		
27,701	89	Path, HSG D (CR, PD)		
30,503	98	Paved roads w/curbs & sewers, HSG A (MC)		
130,655	98	Paved roads w/curbs & sewers, HSG B (IR, MC, PD)		
87,268	98	Paved roads w/curbs & sewers, HSG D (IR, MC, PD)		
3,642	60	Permeable Parking Area (OSW)		
185	98	Unconnected pavement, HSG B (OSW)		
4,112	98	Water Surface, HSG B (CR)		
10,807	98	Water Surface, HSG C (CR)		
45,917	98	Water Surface, HSG D (CR)		
3,253	78	Wetland, HSG A (CR)		
103,465	78	Wetlands, HSG B (CR)		
141,675	78	Wetlands, HSG C (CR)		
227,701	78	Wetlands, HSG D (CR)		
10,067	30	Woods, Good, HSG A (CR)		
206,096	55	Woods, Good, HSG B (CR, OSW)		
33,426	70	Woods, Good, HSG C (CR)		
483,730	77	Woods, Good, HSG D (CR, PD)		
34,660	98	impervious (CR)		
2,695,512	77	TOTAL AREA		

Soil Listing (selected nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
72,121	HSG A	CR, MC
807,909	HSG B	AR, CR, IR, MC, OSW, PD
250,834	HSG C	CR
1,511,738	HSG D	AR, CR, IR, MC, OSW, PD
52,910	Other	CR, IR, OSW
2,695,512		TOTAL AREA

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HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground
(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	Cover
0	21,633	54,729	508,869	0	585,231	1/2 acre lots,
						25% imp
28,093	328,741	758	120,996	0	478,588	>75% Grass
						cover, Good
0	0	0	0	13,560	13,560	Cottages
205	10,318	3,310	27,701	0	41,534	Path
0	2,704	6,129	9,556	0	18,389	Path in Resource
0	0	0	0	1,048	1,048	Path(cover
30,503	130,655	0	87,268	0	248,426	Paved roads
0	0	0	0	3,642	3,642	Permeable
0	105	0	0	0	105	Parking Area
0	100	0	0	0	100	pavement
0	4,112	10,807	45,917	0	60,836	Water Surface
3,253	0	0	0	0	3,253	Wetland
0	103,465	141,675	227,701	0	472,841	Wetlands
10,067	206,096	33,426	483,730	0	733,319	Woods, Good
0	0	0	0	34,660	34,660	impervious
72,121	807,909	250,834	1,511,738	52,910	2,695,512	TOTAL AREA

Ground Covers (selected nodes)

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Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
1	AR	0.00	0.00	40.0	0.0050	0.011	18.0	0.0	0.0
2	IR	0.00	0.00	593.0	0.0050	0.013	12.0	0.0	0.0
3	IR	0.00	0.00	46.0	0.0050	0.013	4.0	0.0	0.0
4	MC	0.00	0.00	211.0	0.0050	0.013	12.0	0.0	0.0
5	MC	0.00	0.00	397.0	0.0050	0.013	18.0	0.0	0.0
6	MC	0.00	0.00	490.0	0.0050	0.013	24.0	0.0	0.0
7	MC	0.00	0.00	42.0	0.0050	0.013	4.0	0.0	0.0
8	PD	0.00	0.00	1,006.0	0.0050	0.013	18.0	0.0	0.0
9	PD	0.00	0.00	197.0	0.0050	0.013	24.0	0.0	0.0
10	PD	0.00	0.00	62.0	0.0050	0.013	6.0	0.0	0.0
11	B1	174.00	173.50	36.0	0.0139	0.010	4.0	0.0	0.0
12	B3	168.00	166.94	53.0	0.0200	0.010	6.0	0.0	0.0
13	T18A	172.25	163.50	25.0	0.3500	0.010	24.0	0.0	0.0

Pipe Listing (selected nodes)

8548.0 - Salmon Senior Community - Medway - Propo Type III 24-hr 2-Year Rainfall=3.20"Prepared by MicrosoftPrinted 10/9/2015HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLCPage 6

Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment AR: Abutter R	unoff Runoff Area=449,581 sf 25.00% Impervious Runoff Depth>1.62" Flow Length=2,249' Tc=32.7 min CN=85 Runoff=11.54 cfs 60,819 cf		
Subcatchment CR: Charles R	Ever Runoff Area=1,756,054 sf 7.37% Impervious Runoff Depth>0.94" Flow Length=2,022' Tc=29.7 min CN=74 Runoff=26.27 cfs 136,991 cf		
SubcatchmentIR: Intermedia	ate Roadway Runoff Area=69,032 sf 72.77% Impervious Runoff Depth>1.86" Flow Length=1,790' Tc=17.9 min CN=88 Runoff=2.60 cfs 10,724 cf		
Subcatchment MC: Main Can	Runoff Area=267,248 sf 56.20% Impervious Runoff Depth>1.36" Flow Length=1,577' Tc=12.0 min CN=81 Runoff=8.55 cfs 30,208 cf		
Subcatchment OSW: Off Site	WestRunoff Area=31,028 sf0.60% ImperviousRunoff Depth>0.57"Flow Length=178'Tc=7.7 minCN=66Runoff=0.40 cfs1,481 cf		
Subcatchment PD: Pond Driv	Runoff Area=122,569 sf 50.22% Impervious Runoff Depth>1.87" Flow Length=1,773' Tc=16.0 min CN=88 Runoff=4.84 cfs 19,053 cf		
Reach TCR: Total Flow to Charles RiverInflow=37.81 cfs197,814 cfOutflow=37.81 cfs197,814 cf			
Pond B1: BASIN 1	Peak Elev=177.25' Storage=5,126 cf Inflow=2.60 cfs 10,724 cf Discarded=0.27 cfs 8,579 cf Primary=0.00 cfs 0 cf Outflow=0.27 cfs 8,579 cf		
Pond B3: BASIN 3	Peak Elev=176.36' Storage=10,863 cf Inflow=4.84 cfs 19,053 cf Discarded=0.32 cfs 10,610 cf Primary=0.00 cfs 0 cf Outflow=0.32 cfs 10,610 cf		
Pond T18A: TRENCH 18A	Peak Elev=172.26' Storage=17,191 cf Inflow=8.55 cfs 30,208 cf Discarded=0.48 cfs 16,033 cf Primary=0.00 cfs 4 cf Outflow=0.48 cfs 16,037 cf		
Total Runoff Area =	2.695.512 sf Runoff Volume = 259.277 cf Average Runoff Depth = 1.15"		

81.30% Pervious = 2,191,537 sf 18.70% Impervious = 503,975 sf

Summary for Subcatchment AR: Abutter Runoff

Runoff = 11.54 cfs @ 12.46 hrs, Volume= 60,819 cf, Depth> 1.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

A	rea (sf)	CN D	Description		
	1,629	70 1	/2 acre lots	s, 25% imp	, HSG B
4	47,952	85 1	/2 acre lots	<u>s, 25% imp</u>	, HSG D
449,581		85 V	Veighted A	verage	
337,186		7	'5.00% Per	vious Area	
112,395		2	5.00% Imp	pervious Are	ea
Та	المربع ورالم	Clana	Valasity	Conositu	Description
IC (mim)	Length	Siope		Capacity	Description
(min)	(feet)	(ft/ft)	(II/SEC)	(CIS)	
9.3	50	0.0400	0.09		Sheet Flow, Sheet AB
					Woods: Light underbrush n= 0.400 P2= 3.20"
1.5	253	0.0320	2.88		Shallow Concentrated Flow, Wooded BC
					Unpaved Kv= 16.1 fps
0.1	40	0.0050	4.97	8.78	Pipe Channel, Pipe CD
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
					n= 0.011 Concrete pipe, straight & clean
21.6	1,862	0.0080	1.44		Shallow Concentrated Flow, Wetland/Strea/Pond DE
					Unpaved Kv= 16.1 fps
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River EF
					Unpaved Kv= 16.1 fps
32.7	2,249	Total			



Subcatchment AR: Abutter Runoff

Summary for Subcatchment CR: Charles River

Runoff = 26.27 cfs @ 12.45 hrs, Volume= 136,991 cf, Depth> 0.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

_	A	rea (sf)	CN	Description					
		10,067	30	Woods, Go	od, HSG A				
		5,689	39	>75% Gras	s cover, Go	ood, HSG A			
*		3,253 78 Wetland, HSG A							
*		205	72	Path, HSG	A				
	2	03,113	55	Woods, Go	od, HSG B				
	2	11,820	61	>75% Gras	s cover, Go	ood, HSG B			
*	1	03,465	78	Wetlands, HSG B					
*		10,318	82	Path, HSG B					
*		2,704	80	Path in Res	ource, HSC	G B			
4,112 98 Water Surface, HSG B									
33,426 70 Woods, Go					od, HSG C				
758 74 >75% Grass cover, Good, HSG C						ood, HSG C			
*	1	41,675	78	Wetlands, HSG C					
*		3,310	87	Path, HSG C					
*		6,129	80	Path in Resource, HSG C					
10,807 98 Water Surface, HSG C									
	4	58,293	77	Woods, Go	od, HSG D				
		65,768	80	>75% Gras	s cover, Go	ood, HSG D			
*	2	27,701	78	Wetlands, HSG D					
*		27,658	89	Path, HSG D					
*		9,556	80	Path in Res	ource, HSC	G D			
		45,917	98	Water Surfa	ace, HSG D				
		20,004	70	1/2 acre lot	s, 25% imp	, HSG B			
		54,729	80	1/2 acre lot	s, 25% imp	, HSG C			
		60,917	85	1/2 acre lot	s, 25% imp	, HSG D			
*		34,660	98	impervious					
	1,7	56,054	74	Weighted A	verage				
	1,626,646		92.63% Pervious Area						
	1	29,409	·	7.37% Impe	ervious Are	a			
	т.	1	01.000		O a s a site s	Description			
	(min)	(foot)	Siope		Capacity	Description			
					(05)				
	7.9	50	0.0600	0.10		Sneet Flow, Sneet A-B			
	2.4	200	0 04 00	4.70		Woods: Light underbrush n= 0.400 P2= 3.20°			
	3.1	329	0.0120	1.76		Shallow Concentrated Flow, wetland B-C			
	10 E	1 500	0 0000			Unpaved Kv= 16.1 lps Shellow Concentrated Flow Wetland/Streem/Band C F			
	10.5	1,599	0.0080	1.44		Shahow Concentrated Flow, Wetland/Stream/Pond C-L			
	0.2	11	0 0000	0 100		Shallow Concentrated Flow, Bond to Biver D.F.			
	0.2	44	0.0900	4.03		Unpayed Ky 16.1 fps			
_	20.7	2 0 0 0	Total						
	29.7	2,022	rotal						


Subcatchment CR: Charles River

Summary for Subcatchment IR: Intermediate Roadway

Runoff = 2.60 cfs @ 12.25 hrs, Volume= 10,724 cf, Depth> 1.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

A	rea (sf)	CN E	Description		
	17,093	61 >	75% Gras	s cover, Go	ood, HSG B
	1,704	80 >	75% Gras	s cover, Go	od, HSG D
	28,466	98 F	Paved road	s w/curbs 8	k sewers, HSG B
	8,209	98 F	Paved road	s w/curbs &	& sewers, HSG D
*	13,560	<u>98</u> C	Cottages		
	69,032	88 V	Veighted A	verage	
	18,797	2	27.23% Per	vious Area	
	50,235	7	' 2.77% Imp	pervious Are	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
5.6	50	0.0200	0.15		Sheet Flow, Sheet A-B
					Grass: Short n= 0.150 P2= 3.20"
0.1	9	0.0200	2.28		Shallow Concentrated Flow, Grass B-C
	47		0.07		Unpaved Kv= 16.1 fps
0.3	47	0.0200	2.87		Shallow Concentrated Flow, Paved C-D
0.4	500	0.0050	0.04	0.50	Paved Kv= 20.3 fps
3.1	593	0.0050	3.21	2.52	Pipe Channel, Pipe D-E
					12.0 Round Alea= 0.0 Si Penini= 5.1 I= 0.25
03	153		8.02		Lake or Reservoir Basin E-E
0.5	100		0.02		Mean Denth- $2.00'$
0.5	46	0 0050	1 54	0.13	Pine Channel Pine F-F
0.0	10	0.0000	1.01	0.10	4.0" Round Area= 0.1 sf Perim= 1.0' $r= 0.08'$
					n=0.013 Corrugated PE, smooth interior
1.4	149	0.0130	1.84		Shallow Concentrated Flow, Unpaved
					Unpaved Kv= 16.1 fps
2.4	333	0.0200	2.28		Shallow Concentrated Flow, Unpaved
					Unpaved Kv= 16.1 fps
4.2	410	0.0100	1.61		Shallow Concentrated Flow, Unpaved
					Unpaved Kv= 16.1 fps

17.9 1,790 Total



Subcatchment IR: Intermediate Roadway

Summary for Subcatchment MC: Main Campus

Runoff = 8.55 cfs @ 12.17 hrs, Volume= 30,208 cf, Depth> 1.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

Α	rea (sf)	CN D	escription					
	22,404	39 >	39 >75% Grass cover, Good, HSG A					
	82,752	61 >	75% Gras	s cover, Go	od, HSG B			
	11,890	80 >	75% Gras	s cover, Go	od, HSG D			
	30,503	98 P	aved road	s w/curbs &	k sewers, HSG A			
	96,592	98 P	aved road	s w/curbs &	k sewers, HSG B			
	23,107	<u>98 P</u>	aved road	S W/CUIDS &	sewers, HSG D			
2	67,248	81 V	eighted A	verage				
1	17,046	4.	3.80% Per	vious Area				
I	50,202	C	0.20% imp	bervious Are	đa			
Тс	l enath	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Decemption			
5.0	43	0.0200	0.14	(0.0)	Sheet Flow, Sheet Grass A-B			
0.0		0.0200	••••		Grass: Short n= 0.150 P2= 3.20"			
0.1	7	0.0200	0.81		Sheet Flow, Sheet-Pave B-C			
					Smooth surfaces n= 0.011 P2= 3.20"			
1.3	217	0.0200	2.87		Shallow Concentrated Flow, Paved C-D			
					Paved Kv= 20.3 fps			
1.1	211	0.0050	3.21	2.52	Pipe Channel, Pipe D-E			
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'			
					n= 0.013 Corrugated PE, smooth interior			
1.6	397	0.0050	4.20	7.43	Pipe Channel, Pipe E-F			
					18.0° Round Area= 1.8 st Perim= 4.7° r= 0.38°			
1.0	400	0.0050	E 00	10.00	n= 0.013 Corrugated PE, smooth Interior			
1.0	490	0.0050	5.09	16.00	Pipe Channel, Pipe F-G 24.0° Round Aroa- 3.1 of Porim- 6.3' r- 0.50'			
					24.0 Round Alea 3.1 Si Penine 0.3 $1 = 0.50$			
0.0	24		8 97		Lake or Reservoir Lake G-H			
0.0	27		0.07		Mean Depth= $2.50'$			
0.5	42	0.0050	1.54	0.13	Pipe Channel, Pipe F-G			
					4.0" Round Area= 0.1 sf Perim= 1.0' r= 0.08'			
					n= 0.013 Corrugated PE, smooth interior			
0.8	146	0.0400	3.22		Shallow Concentrated Flow, Unpaved I-J			
					Unpaved Kv= 16.1 fps			

12.0 1,577 Total



Subcatchment MC: Main Campus

Summary for Subcatchment OSW: Off Site West

Runoff = 0.40 cfs @ 12.14 hrs, Volume= 1,481 cf, Depth> 0.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

	A	<u>rea (sf)</u>	CN	Description		
		2,983	55	Woods, Go	od, HSG B	
		15,112	61	>75% Gras	s cover, Go	ood, HSG B
*		1,048	80	Path(cover	unknown)	
		185	98	Unconnect	ed pavemer	nt, HSG B
		8,058	80	>75% Gras	s cover, Go	ood, HSG D
*		3,642	60	Permeable	Parking Are	ea
		31,028	66	Weighted A	Average	
		30,843		99.40% Pe	rvious Area	
		185		0.60% Imp	ervious Area	a
		185		100.00% U	nconnected	1
	Тс	Length	Slop	e Velocity	Capacity	Description
	(min)	(feet)	(ft/ft	t) (ft/sec)	(cfs)	
	7.1	50	0.080	0 0.12		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.20"
	0.6	128	0.054	0 3.74		Shallow Concentrated Flow, Wooded/Path/Wooded B-C

7.7 178 Total

Subcatchment OSW: Off Site West



Summary for Subcatchment PD: Pond Drive

Runoff = 4.84 cfs @ 12.22 hrs, Volume= 19,053 cf, Depth> 1.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

A	Area (sf)	CN D	escription					
	1,964	61 >	75% Grass	s cover, Go	od, HSG B			
	5,597	98 P	aved road	s w/curbs &	k sewers, HSG B			
	25,437	77 V	77 Woods, Good, HSG D					
	33,576	80 >	75% Grass	s cover, Go	od, HSG D			
×	43	89 P	ath, HSG	D				
	55,952	<u>98 P</u>	aved road	s w/curbs &	k sewers, HSG D			
	122,569	88 V	/eighted A	verage				
	61,020	4	9.78% Per	vious Area				
	61,549	5	0.22% Imp	ervious Are	28			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
7.9	50	0.0600	0.10		Sheet Flow, Sheet A-B			
					Woods: Light underbrush n= 0.400 P2= 3.20"			
0.3	55	0.0400	3.22		Shallow Concentrated Flow, Grass B-C			
					Unpaved Kv= 16.1 fps			
0.8	136	0.0200	2.87		Shallow Concentrated Flow, Paved C-D			
					Paved Kv= 20.3 fps			
4.0	1,006	0.0050	4.20	7.43	Pipe Channel, Pipe D-E			
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'			
					n= 0.013 Corrugated PE, smooth interior			
0.6	197	0.0050	5.09	16.00	Pipe Channel, Pipe E-F			
					24.0" Round Area= 3.1 st Perim= 6.3" r= 0.50"			
0.0			0.00		n= 0.013 Corrugated PE, smooth interior			
0.2	11		8.02		Lake or Reservoir, Basin F-G			
0.5	60	0.0050	2.02	0.40	Niean Depin= 2.00 Ding Channel, Ding C H			
0.5	02	0.0050	2.02	0.40	Fipe Champer, Fipe G-fi 6.0" Pound Aroo- 0.2 of Porim- 1.6' r - 0.13'			
					n = 0.013 Corrugated PE smooth interior			
07	89	0 0200	2 28		Shallow Concentrated Flow Unnaved H-I			
0.7	00	0.0200	2.20		Unpaved Ky= 16 1 fps			
0.8	57	0.0050	1.14		Shallow Concentrated Flow, Unpaved I-J			
210					Unpaved Kv= 16.1 fps			
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Upaved J-K			
		-	-		Unpaved Kv= 16.1 fps			

16.0 1,773 Total



Subcatchment PD: Pond Drive

Summary for Reach TCR: Total Flow to Charles River

Inflow /	Area =	=	2,664,484 sf,	18.91% Ir	npervious,	Inflow Depth >	0.89"	for 2-1	lear event
Inflow	=		37.81 cfs @	12.45 hrs,	Volume=	197,814 c	f		
Outflov	v =		37.81 cfs @	12.45 hrs,	Volume=	197,814 c	f, Atter	n= 0%,	Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach TCR: Total Flow to Charles River

Summary for Pond B1: BASIN 1

Inflow Area	a =	69,032 sf,	72.77% Impe	ervious, li	nflow Depth >	1.86"	for 2-Ye	ear event	
Inflow	=	2.60 cfs @	12.25 hrs, Vo	olume=	10,724 cf	:			
Outflow	=	0.27 cfs @	13.71 hrs, Vo	olume=	8,579 cf	, Atten	= 89%,	Lag= 87.7 mir	n
Discarded	=	0.27 cfs @	13.71 hrs, Vo	olume=	8,579 cf	:		-	
Primary	=	0.00 cfs @	5.00 hrs, Vo	olume=	0 cf	:			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.25' @ 13.71 hrs Surf.Area= 4,915 sf Storage= 5,126 cf

Plug-Flow detention time= 173.9 min calculated for 8,579 cf (80% of inflow) Center-of-Mass det. time= 121.8 min (912.8 - 790.9)

Volume	Inver	t Avail.Stor	rage Storage	Description	
#1	176.00	' 33,72	22 cf Custon	n Stage Data (Pr	ismatic)Listed below (Recalc)
Flowetic		Surf Area	In a Otara	Curro Chara	
Elevatio	ກ ຣ	Surr.Area	Inc.Store	Cum.Store	
(tee	et)	(SQ-II)	(CUDIC-TEET)	(CUDIC-TEET)	
176.0	00	3,342	0	0	
177.0	00	4,577	3,960	3,960	
178.0)0	5,952	5,265	9,224	
179.0	00	7,387	6,670	15,894	
180.0	00	8,885	8,136	24,030	
181.0	00	10,500	9,693	33,722	
Device	Routing	Invert	Outlet Device	S	
#1	Primary	174.00'	4.0" Round	Culvert	
			L= 36.0' CP	P, mitered to cor	form to fill, Ke= 0.700
			Inlet / Outlet	Invert= 174.00' /	173.50' S= 0.0139 '/' Cc= 0.900
			n= 0.010 PV	C, smooth interio	or, Flow Area= 0.09 sf
#2	Device 1	179.00'	6.0" Vert. Or	ifice/Grate C=	0.600
#3	Device 1	179.25'	1.0" Vert. Or	ifice/Grate C=	0.600
#4	Device 1	179.50'	24.0" x 24.0"	Horiz. Orifice/C	Grate C= 0.600
			Limited to we	ir flow at low hea	ads
#5	Primary	179.90'	20.0' long x	5.0' breadth Bro	oad-Crested Rectangular Weir
	-		Head (feet) (0.20 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.	50 4.00 4.50 5	.00 5.50
			Coef. (Englis	h) 2.34 2.50 2.	70 2.68 2.68 2.66 2.65 2.65 2.65
			2.65 2.67 2.	66 2.68 2.70 2	.74 2.79 2.88
#6	Discarded	176.00'	2.410 in/hr E	xfiltration over	Surface area

Discarded OutFlow Max=0.27 cfs @ 13.71 hrs HW=177.25' (Free Discharge) **G=Exfiltration** (Exfiltration Controls 0.27 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=176.00' (Free Discharge)

1=Culvert (Passes 0.00 cfs of 0.48 cfs potential flow)

2=Orifice/Grate (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

4=Orifice/Grate (Controls 0.00 cfs)

-5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B1: BASIN 1

Summary for Pond B3: BASIN 3

Inflow Area	a =	122,569 sf,	50.22% In	npervious,	Inflow Depth >	1.87"	for 2-Y	ear event	
Inflow	=	4.84 cfs @	12.22 hrs,	Volume=	19,053 ct	f			
Outflow	=	0.32 cfs @	15.02 hrs,	Volume=	10,610 ct	f, Atten	= 93%,	Lag= 168.1 m	nin
Discarded	=	0.32 cfs @	15.02 hrs,	Volume=	10,610 ct	f			
Primary	=	0.00 cfs @	5.00 hrs,	Volume=	0 c	f			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 176.36' @ 15.02 hrs Surf.Area= 5,603 sf Storage= 10,863 cf

Plug-Flow detention time= 196.2 min calculated for 10,610 cf (56% of inflow) Center-of-Mass det. time= 118.6 min (908.1 - 789.4)

Volume	Invert	Avail.Stor	rage Storage [Description		
#1	174.00'	38,01	0 cf Custom	Stage Data (Coni	c) Listed below (Red	calc)
Elevatio (fee	on S et)	urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
174.0 175.0 176.0 177.0 177.0 178.0 179.0	20 20 20 20 20 20 20 20	3,673 4,455 5,293 6,187 7,138 8,146 10,000	0 4,058 4,868 5,734 6,657 7,636 9,057	0 4,058 8,926 14,660 21,317 28,953 38,010	3,673 4,487 5,361 6,294 7,288 8,343 10,227	
Device	Routing	Invert	9,057 Outlet Devices	36,010	10,227	
#1	Primary	168.00'	6.0" Round C L= 53.0' CPP Inlet / Outlet In n= 0.010 PVC	ulvert , mitered to confor vert= 168.00' / 166 , smooth interior,	m to fill, Ke= 0.700 5.94' S= 0.0200 '/' Flow Area= 0.20 sf	Cc= 0.900
#2 #3	Device 1 Device 1	177.00' 178.50'	3.0" Vert. Orifi 24.0" x 48.0" H Limited to weir	ice/Grate C= 0.6 Horiz. Orifice/Gra flow at low heads	00 te C= 0.600	
#4	Primary	178.90'	20.0' long x 5 Head (feet) 0.250 3.00 3.50 Coef. (English) 2.65 2.67 2.60	.0' breadth Broad 20 0.40 0.60 0.8 0 4.00 4.50 5.00 0 2.34 2.50 2.70 6 2.68 2.70 2.74	I-Crested Rectang 0 1.00 1.20 1.40 5.50 2.68 2.68 2.66 2. 2.79 2.88	ular Weir 1.60 1.80 2.00 65 2.65 2.65
#5	Discarded	174.00'	2.410 in/hr Ex	filtration over We	tted area	

Discarded OutFlow Max=0.32 cfs @ 15.02 hrs HW=176.36' (Free Discharge) **5=Exfiltration** (Exfiltration Controls 0.32 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=174.00' (Free Discharge)

-1=Culvert (Passes 0.00 cfs of 1.97 cfs potential flow)

-2=Orifice/Grate (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

-4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B3: BASIN 3

Summary for Pond T18A: TRENCH 18A

Inflow Area = 267,248 sf, 56.20% Impervious, Inflow Depth > 1.36" for 2-Year event Inflow 8.55 cfs @ 12.17 hrs. Volume= 30.208 cf = 0.48 cfs @ 15.59 hrs, Volume= 16,037 cf, Atten= 94%, Lag= 205.4 min Outflow = 0.48 cfs @ 11.50 hrs, Volume= 16,033 cf Discarded = Primary = 0.00 cfs @ 15.59 hrs, Volume= 4 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 172.26' @ 15.59 hrs Surf.Area= 8,648 sf Storage= 17,191 cf

Plug-Flow detention time= 199.6 min calculated for 16,037 cf (53% of inflow) Center-of-Mass det. time= 117.5 min (923.4 - 805.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	169.50'	11,805 cf	44.75'W x 193.25'L x 5.75'H Field A
			49,726 cf Overall - 20,213 cf Embedded = 29,513 cf x 40.0% Voids
#2A	170.25'	20,213 cf	Cultec R-900HD x 162 Inside #1
			Effective Size= 72.7"W x 48.0"H => 17.61 sf x 7.00'L = 123.3 cf
			Overall Size= 78.0"W x 48.0"H x 9.25'L with 2.25' Overlap
_			Row Length Adjustment= +2.25' x 17.61 sf x 6 rows
		22.019 of	Total Available Storage

32,018 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1 #2	Primary Discarded	172.25' 169.50'	24.0" Round Culvert L= 25.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 172.25' / 163.50' S= 0.3500 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf 2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.48 cfs @ 11.50 hrs HW=169.56' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.48 cfs)

Primary OutFlow Max=0.00 cfs @ 15.59 hrs HW=172.26' (Free Discharge) ←1=Culvert (Inlet Controls 0.00 cfs @ 0.35 fps)

Pond T18A: TRENCH 18A - Chamber Wizard Field A

Chamber Model = Cultec R-900HD

Effective Size= 72.7"W x 48.0"H => 17.61 sf x 7.00'L = 123.3 cf Overall Size= 78.0"W x 48.0"H x 9.25'L with 2.25' Overlap Row Length Adjustment= +2.25' x 17.61 sf x 6 rows

78.0" Wide + 9.0" Spacing = 87.0" C-C Row Spacing

27 Chambers/Row x 7.00' Long +2.25' Row Adjustment = 191.25' Row Length +12.0" End Stone x 2 = 193.25' Base Length 6 Rows x 78.0" Wide + 9.0" Spacing x 5 + 12.0" Side Stone x 2 = 44.75' Base Width 9.0" Base + 48.0" Chamber Height + 12.0" Cover = 5.75' Field Height

162 Chambers x 123.3 cf +2.25' Row Adjustment x 17.61 sf x 6 Rows = 20,212.9 cf Chamber Storage

49,725.6 cf Field - 20,212.9 cf Chambers = 29,512.7 cf Stone x 40.0% Voids = 11,805.1 cf Stone Storage

Chamber Storage + Stone Storage = 32,018.0 cf = 0.735 af Overall Storage Efficiency = 64.4%

162 Chambers 1,841.7 cy Field 1,093.1 cy Stone

Image: selection of the selection





Pond T18A: TRENCH 18A

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment AR: Abutter Runoff	Runoff Area=449,581 sf 25.00% Impervious Runoff Depth>2.88" Flow Length=2,249' Tc=32.7 min CN=85 Runoff=20.21 cfs 107,883 cf
Subcatchment CR: Charles River	Runoff Area=1,756,054 sf 7.37% Impervious Runoff Depth>1.95" Flow Length=2,022' Tc=29.7 min CN=74 Runoff=56.40 cfs 285,319 cf
Subcatchment IR: Intermediate Roa	dway Runoff Area=69,032 sf 72.77% Impervious Runoff Depth>3.18" Flow Length=1,790' Tc=17.9 min CN=88 Runoff=4.35 cfs 18,291 cf
Subcatchment MC: Main Campus	Runoff Area=267,248 sf 56.20% Impervious Runoff Depth>2.54" Flow Length=1,577' Tc=12.0 min CN=81 Runoff=15.99 cfs 56,516 cf
Subcatchment OSW: Off Site West	Runoff Area=31,028 sf 0.60% Impervious Runoff Depth>1.39" Flow Length=178' Tc=7.7 min CN=66 Runoff=1.12 cfs 3,598 cf
Subcatchment PD: Pond Drive	Runoff Area=122,569 sf 50.22% Impervious Runoff Depth>3.18" Flow Length=1,773' Tc=16.0 min CN=88 Runoff=8.09 cfs 32,494 cf
Reach TCR: Total Flow to Charles R	Inflow=80.62 cfs 418,121 cf Outflow=80.62 cfs 418,121 cf
Pond B1: BASIN 1 Discarde	Peak Elev=178.11' Storage=9,905 cf Inflow=4.35 cfs 18,291 cf ed=0.34 cfs 11,508 cf Primary=0.00 cfs 0 cf Outflow=0.34 cfs 11,508 cf
Pond B3: BASIN 3 Discarded=0	Peak Elev=177.70' Storage=19,251 cf Inflow=8.09 cfs 32,494 cf .39 cfs 13,706 cf Primary=0.18 cfs 3,603 cf Outflow=0.57 cfs 17,309 cf
Pond T18A: TRENCH 18A Discarded=0.4	Peak Elev=173.27' Storage=23,671 cf Inflow=15.99 cfs 56,516 cf 48 cfs 18,288 cf Primary=4.89 cfs 21,315 cf Outflow=5.37 cfs 39,603 cf
Total Dunoff Area 2 605 f	12 of Bunoff Volume - 504 101 of Average Bunoff Denth 2.24

Total Runoff Area = 2,695,512 sf Runoff Volume = 504,101 cf Average Runoff Depth = 2.24" 81.30% Pervious = 2,191,537 sf 18.70% Impervious = 503,975 sf

Summary for Subcatchment AR: Abutter Runoff

Runoff = 20.21 cfs @ 12.45 hrs, Volume= 107,883 cf, Depth> 2.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN E	Description		
	1,629	70 1	/2 acre lots	s, 25% imp	, HSG B
4	47,952	85 1	/2 acre lots	<u>s, 25% imp</u>	, HSG D
4	49,581	85 V	Veighted A	verage	
3	37,186	7	'5.00% Per	vious Area	
1	12,395	2	5.00% Imp	pervious Are	ea
Т	المربع مرالم	01	\/_l!+	0	Description
IC (mim)	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(π/π)	(ft/sec)	(CTS)	
9.3	50	0.0400	0.09		Sheet Flow, Sheet AB
					Woods: Light underbrush n= 0.400 P2= 3.20"
1.5	253	0.0320	2.88		Shallow Concentrated Flow, Wooded BC
					Unpaved Kv= 16.1 fps
0.1	40	0.0050	4.97	8.78	Pipe Channel, Pipe CD
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
					n= 0.011 Concrete pipe, straight & clean
21.6	1,862	0.0080	1.44		Shallow Concentrated Flow, Wetland/Strea/Pond DE
					Unpaved Kv= 16.1 fps
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River EF
					Unpaved Kv= 16.1 fps
32.7	2,249	Total			



Subcatchment AR: Abutter Runoff

Summary for Subcatchment CR: Charles River

Runoff = 56.40 cfs @ 12.43 hrs, Volume= 285,319 cf, Depth> 1.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

	A	rea (sf)	CN	Description		
		10,067	30	Woods, Go	od, HSG A	
		5,689	39	>75% Gras	s cover, Go	ood, HSG A
*		3,253	78	Wetland, H	SG A	
*		205	72	Path, HSG	A	
	2	03,113	55	Woods, Go	od, HSG B	
	2	11,820	61	>75% Gras	s cover, Go	ood, HSG B
*	1	03,465	78	Wetlands, H	ISG B	
*		10,318	82	Path, HSG	В	
*		2,704	80	Path in Res	source, HSC	G B
		4,112	98	Water Surfa	ace, HSG B	
		33,426	70	Woods, Go	od, HSG C	
		758	74	>75% Gras	s cover, Go	ood, HSG C
*	1	41,675	78	Wetlands, H	HSG C	
*		3,310	87	Path, HSG	С	
*		6,129	80	Path in Res	source, HSC	GC
		10,807	98	Water Surfa	ace, HSG C	
	4	58,293	77	Woods, Go	od, HSG D	
		65,768	80	>75% Gras	s cover, Go	ood, HSG D
*	2	27,701	78	Wetlands, H	HSG D	
*		27,658	89	Path, HSG	D	
*		9,556	80	Path in Res	source, HSC	G D
		45,917	98	Water Surfa	ace, HSG D	
		20,004	70	1/2 acre lot	s, 25% imp	, HSG B
		54,729	80	1/2 acre lot	s, 25% imp	, HSG C
		60,917	85	1/2 acre lot	s, 25% imp	, HSG D
*		34,660	98	impervious		
	1,7	56,054	74	Weighted A	verage	
	1,6	26,646		92.63% Per	rvious Area	
	1	29,409		7.37% Impe	ervious Area	a
	_		<u>.</u>		a	- · · · ·
	, IC	Length	Slope	e Velocity	Capacity	Description
	(min)	(feet)	(ft/ft) (ft/sec)	(CfS)	
	7.9	50	0.0600	0.10		Sheet Flow, Sheet A-B
						Woods: Light underbrush n= 0.400 P2= 3.20"
	3.1	329	0.0120) 1.76		Shallow Concentrated Flow, Wetland B-C
						Unpaved Kv= 16.1 fps
	18.5	1,599	0.0080) 1.44		Shallow Concentrated Flow, Wetland/Stream/Pond C-D
			0.000			Unpaved Kv= 16.1 tps
	0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River D-E
						Unpaved Kv= 16.1 tps
	29.7	2,022	Total			



Subcatchment CR: Charles River

Summary for Subcatchment IR: Intermediate Roadway

Runoff = 4.35 cfs @ 12.24 hrs, Volume= 18,291 cf, Depth> 3.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN E	Description					
	17,093	61 >	61 >75% Grass cover, Good, HSG B					
	1,704	80 >	80 >75% Grass cover, Good, HSG D					
	28,466	98 F	98 Paved roads w/curbs & sewers, HSG B					
	8,209	98 F	Paved road	s w/curbs &	& sewers, HSG D			
*	13,560	<u>98</u> C	Cottages					
	69,032	88 V	Veighted A	verage				
	18,797	2	27.23% Per	vious Area				
	50,235	7	' 2.77% Imp	pervious Are	ea			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
5.6	50	0.0200	0.15		Sheet Flow, Sheet A-B			
					Grass: Short n= 0.150 P2= 3.20"			
0.1	9	0.0200	2.28		Shallow Concentrated Flow, Grass B-C			
	47		0.07		Unpaved Kv= 16.1 fps			
0.3	47	0.0200	2.87		Shallow Concentrated Flow, Paved C-D			
0.4	500	0.0050	0.04	0.50	Paved Kv= 20.3 fps			
3.1	593	0.0050	3.21	2.52	Pipe Channel, Pipe D-E			
					12.0 Round Alea= 0.0 Si Penini= 5.1 I= 0.25			
03	153		8.02		Lake or Reservoir Basin E-E			
0.5	100		0.02		Mean Denth- $2.00'$			
0.5	46	0 0050	1 54	0.13	Pine Channel Pine F-F			
0.0	10	0.0000	1.01	0.10	4.0" Round Area= 0.1 sf Perim= 1.0' $r= 0.08'$			
					n=0.013 Corrugated PE, smooth interior			
1.4	149	0.0130	1.84		Shallow Concentrated Flow, Unpaved			
					Unpaved Kv= 16.1 fps			
2.4	333	0.0200	2.28		Shallow Concentrated Flow, Unpaved			
					Unpaved Kv= 16.1 fps			
4.2	410	0.0100	1.61		Shallow Concentrated Flow, Unpaved			
					Unpaved Kv= 16.1 fps			

17.9 1,790 Total



Subcatchment IR: Intermediate Roadway

Summary for Subcatchment MC: Main Campus

Runoff = 15.99 cfs @ 12.17 hrs, Volume= 56,516 cf, Depth> 2.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN D	escription						
	22,404	39 >	39 >75% Grass cover, Good, HSG A						
	82,752	61 >	61 >75% Grass cover, Good, HSG B						
	11,890	80 >	75% Gras	s cover, Go	bod, HSG D				
	30,503	98 P	aved road	s w/curbs &	k sewers, HSG A				
	96,592	98 P	aved road	s w/curbs &	k sewers, HSG B				
	23,107	<u>98 P</u>	aved road	S W/CUIDS &	x sewers, HSG D				
	17.046	81 V	/eignted A						
1	17,040 50.202	4	3.80% Pei 6.20% Imr	vious Area	22				
I	50,202	5	0.20% 111	Del vious An	ed a state of the				
Тс	Lenath	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
5.0	43	0.0200	0.14		Sheet Flow, Sheet Grass A-B				
					Grass: Short n= 0.150 P2= 3.20"				
0.1	7	0.0200	0.81		Sheet Flow, Sheet-Pave B-C				
					Smooth surfaces n= 0.011 P2= 3.20"				
1.3	217	0.0200	2.87		Shallow Concentrated Flow, Paved C-D				
	- · · ·				Paved Kv= 20.3 fps				
1.1	211	0.0050	3.21	2.52	Pipe Channel, Pipe D-E				
					12.0° Round Area= 0.8 st Perim= 3.1° r= 0.25°				
16	207	0.0050	1 20	7 4 2	Pipe Channel Pipe E E				
1.0	291	0.0030	4.20	7.43	18.0" Round Area 1.8 of Perim 4.7 r -0.38				
					n=0.013 Corrugated PE smooth interior				
1.6	490	0.0050	5.09	16.00	Pipe Channel. Pipe F-G				
		0.0000	0.00		24.0" Round Area= 3.1 sf Perim= $6.3'$ r= $0.50'$				
					n= 0.013 Corrugated PE, smooth interior				
0.0	24		8.97		Lake or Reservoir, Lake G-H				
					Mean Depth= 2.50				
0.5	42	0.0050	1.54	0.13	Pipe Channel, Pipe F-G				
					4.0" Round Area= 0.1 sf Perim= 1.0' r= 0.08'				
					n= 0.013 Corrugated PE, smooth interior				
0.8	146	0.0400	3.22		Shallow Concentrated Flow, Unpaved I-J				
					Unpaved Kv= 16.1 tps				

12.0 1,577 Total



Subcatchment MC: Main Campus

Summary for Subcatchment OSW: Off Site West

Runoff = 1.12 cfs @ 12.12 hrs, Volume= 3,598 cf, Depth> 1.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

	A	rea (sf)	CN	Description	1	
		2,983	55	Woods, Go	od, HSG B	
		15,112	61	>75% Gras	s cover, Go	ood, HSG B
*		1,048	80	Path(cover	unknown)	
		185	98	Unconnect	ed pavemer	nt, HSG B
		8,058	80	>75% Gras	s cover, Go	ood, HSG D
*		3,642	60	Permeable	Parking Are	ea
		31,028	66	Weighted A	Verage	
	30.843 99.40% Pervious Area				rvious Area	
		185		0.60% Imp	ervious Area	a
		185		100.00% Ü	nconnected	1
	Тс	Length	Slop	e Velocity	Capacity	Description
(n	nin)	(feet)	(ft/f	t) (ft/sec)	(cfs)	
	7.1	50	0.080	0 0.12		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.20"
	0.6	128	0.054	0 3.74		Shallow Concentrated Flow, Wooded/Path/Wooded B-C
						Unpaved Kv= 16.1 fps
	7.7	178	Total			

Subcatchment OSW: Off Site West



Summary for Subcatchment PD: Pond Drive

Runoff = 8.09 cfs @ 12.22 hrs, Volume= 32,494 cf, Depth> 3.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN D	escription				
	1,964	61 >	75% Gras	s cover, Go	od, HSG B		
	5,597	98 Paved roads w/curbs & sewers, HSG B					
	25,437	77 V	/oods, Go	od, HSG D			
	33,576	80 >	75% Gras	s cover, Go	od, HSG D		
*	43	89 P	ath, HSG	D a.u./a.urba G			
	55,952	<u>98 P</u>	aved road	S W/CUIDS &	sewers, HSG D		
1	22,569	88 V	/eighted A	verage			
	61,020	4	9.78% Per	vious Area			
	61,549	5	0.22% imp	ervious Are	38		
Тс	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·		
7.9	50	0.0600	0.10		Sheet Flow, Sheet A-B		
					Woods: Light underbrush n= 0.400 P2= 3.20"		
0.3	55	0.0400	3.22		Shallow Concentrated Flow, Grass B-C		
					Unpaved Kv= 16.1 fps		
0.8	136	0.0200	2.87		Shallow Concentrated Flow, Paved C-D		
				= 10	Paved Kv= 20.3 fps		
4.0	1,006	0.0050	4.20	7.43	Pipe Channel, Pipe D-E		
					18.0° Round Area= 1.8 st Perim= 4.7° r= 0.38°		
0.6	107	0.0050	E 00	16.00	n= 0.013 Corrugated PE, smooth Interior		
0.0	197	0.0050	5.09	10.00	Pipe Champel, Fipe E-F $24.0^{"}$ Pound Aroa- 3.1 sf Porim- 6.3' r- 0.50'		
					n = 0.013 Corrugated PE smooth interior		
02	77		8 02		Lake or Reservoir Basin F-G		
0.2			0.02		Mean Depth= 2.00'		
0.5	62	0.0050	2.02	0.40	Pipe Channel, Pipe G-H		
					6.0" Round Area= 0.2 sf Perim= 1.6' r= 0.13'		
					n= 0.013 Corrugated PE, smooth interior		
0.7	89	0.0200	2.28		Shallow Concentrated Flow, Unpaved H-I		
					Unpaved Kv= 16.1 fps		
0.8	57	0.0050	1.14		Shallow Concentrated Flow, Unpaved I-J		
					Unpaved Kv= 16.1 fps		
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Upaved J-K		
					Unpaved Kv= 16.1 tps		

16.0 1,773 Total



Subcatchment PD: Pond Drive

Summary for Reach TCR: Total Flow to Charles River

Inflow A	Area =	2,664,484 sf, 18.91% Impervious,	Inflow Depth > 1.88"	for 10-Year event
Inflow	=	80.62 cfs @ 12.45 hrs, Volume=	418,121 cf	
Outflow	/ =	80.62 cfs @ 12.45 hrs, Volume=	418,121 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach TCR: Total Flow to Charles River

Summary for Pond B1: BASIN 1

Inflow Area	=	69,032 sf,	72.77% In	npervious,	Inflow Depth > 3	8.18" fo	or 10-`	Year event	
Inflow	=	4.35 cfs @	12.24 hrs,	Volume=	18,291 cf				
Outflow	=	0.34 cfs @	14.30 hrs,	Volume=	11,508 cf,	Atten=	92%,	Lag= 123.7	' min
Discarded	=	0.34 cfs @	14.30 hrs,	Volume=	11,508 cf			•	
Primary	=	0.00 cfs @	5.00 hrs,	Volume=	0 cf				

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.11' @ 14.30 hrs Surf.Area= 6,114 sf Storage= 9,905 cf

Plug-Flow detention time= 188.0 min calculated for 11,508 cf (63% of inflow) Center-of-Mass det. time= 116.2 min (894.5 - 778.3)

Volume	Inver	t Avail.Sto	rage Storage	e Description	
#1	176.00	' 33,72	22 cf Custon	n Stage Data (Pr	ismatic)Listed below (Recalc)
_		<i>.</i> .			
Elevatio	on S	urf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
176.0	00	3,342	0	0	
177.0	00	4,577	3,960	3,960	
178.0	00	5,952	5,265	9,224	
179.0	00	7,387	6,670	15,894	
180.0	00	8,885	8,136	24,030	
181.0	00	10,500	9,693	33,722	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	174.00'	4.0" Round	Culvert	
	-		L= 36.0' CP	P, mitered to cor	form to fill, Ke= 0.700
			Inlet / Outlet	Invert= 174.00' /	173.50' S= 0.0139 '/' Cc= 0.900
			n= 0.010 PV	C, smooth interio	or, Flow Area= 0.09 sf
#2	Device 1	179.00'	6.0" Vert. Or	ifice/Grate C=	0.600
#3	Device 1	179.25'	1.0" Vert. Or	ifice/Grate C=	0.600
#4	Device 1	179.50'	24.0" x 24.0"	' Horiz. Orifice/G	Grate C= 0.600
			Limited to we	ir flow at low hea	ads
#5	Primary	179.90'	20.0' long x	5.0' breadth Bro	oad-Crested Rectangular Weir
	-		Head (feet) (0.20 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.	50 4.00 4.50 5	.00 5.50
			Coef. (Englis	h) 2.34 2.50 2. ⁻	70 2.68 2.68 2.66 2.65 2.65 2.65
			2.65 2.67 2.	66 2.68 2.70 2	.74 2.79 2.88
#6	Discarded	176.00'	2.410 in/hr E	xfiltration over	Surface area

Discarded OutFlow Max=0.34 cfs @ 14.30 hrs HW=178.11' (Free Discharge) **G=Exfiltration** (Exfiltration Controls 0.34 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=176.00' (Free Discharge)

1=Culvert (Passes 0.00 cfs of 0.48 cfs potential flow)

2=Orifice/Grate (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

4=Orifice/Grate (Controls 0.00 cfs)

-5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B1: BASIN 1

Summary for Pond B3: BASIN 3

Inflow Area	ι =	122,569 sf,	50.22% In	npervious,	Inflow Depth > 3	3.18"	for 10-	Year event	
Inflow	=	8.09 cfs @	12.22 hrs,	Volume=	32,494 cf				
Outflow	=	0.57 cfs @	14.49 hrs,	Volume=	17,309 cf,	Atten	= 93%,	Lag= 136.7 r	min
Discarded	=	0.39 cfs @	14.49 hrs,	Volume=	13,706 cf			•	
Primary	=	0.18 cfs @	14.49 hrs,	Volume=	3,603 cf				

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.70' @ 14.49 hrs Surf.Area= 6,850 sf Storage= 19,251 cf

Plug-Flow detention time= 199.4 min calculated for 17,309 cf (53% of inflow) Center-of-Mass det. time= 118.9 min (895.7 - 776.8)

Volume	Invert	Avail.Sto	rage Storage I	Description		
#1	174.00	38,01	0 cf Custom	Stage Data (Coni	c) Listed below (Re	calc)
Elevatio (fee	on S et)	urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
174.0 175.0 176.0 177.0 177.0 178.0 179.0	00 00 00 00 00 00 00	3,673 4,455 5,293 6,187 7,138 8,146	0 4,058 4,868 5,734 6,657 7,636 0,057	0 4,058 8,926 14,660 21,317 28,953 38,010	3,673 4,487 5,361 6,294 7,288 8,343	
Device	Routing	Invert	9,057 Outlet Devices	38,010	10,227	
#1	Primary	168.00'	6.0" Round C L= 53.0' CPP Inlet / Outlet In n= 0.010 PVC	ulvert , mitered to confor vert= 168.00' / 166 , smooth interior,	m to fill, Ke= 0.700 5.94' S= 0.0200 '/' Flow Area= 0.20 sf) Cc= 0.900
#2 #3	Device 1 Device 1	177.00' 178.50'	3.0" Vert. Orif 24.0" x 48.0" I Limited to weir	ice/Grate C= 0.6 Horiz. Orifice/Gra flow at low heads	00 te C= 0.600	
#4	Primary	178.90'	20.0' long x 5 Head (feet) 0. 2.50 3.00 3.5 Coef. (English) 2.65 2.67 2.6	.0' breadth Broad 20 0.40 0.60 0.8 0 4.00 4.50 5.00) 2.34 2.50 2.70 6 2.68 2.70 2.74	I-Crested Rectang 0 1.00 1.20 1.40 5.50 2.68 2.68 2.66 2 2.79 2.88	ular Weir 1.60 1.80 2.00 .65 2.65 2.65
#5	Discarded	174.00'	2.410 in/hr Ex	filtration over We	etted area	

Discarded OutFlow Max=0.39 cfs @ 14.49 hrs HW=177.70' (Free Discharge) **5=Exfiltration** (Exfiltration Controls 0.39 cfs)

Primary OutFlow Max=0.18 cfs @ 14.49 hrs HW=177.70' (Free Discharge)

1=Culvert (Passes 0.18 cfs of 2.47 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.18 cfs @ 3.67 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

-4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B3: BASIN 3

Summary for Pond T18A: TRENCH 18A

Inflow Area = 267,248 sf, 56.20% Impervious, Inflow Depth > 2.54" for 10-Year event Inflow 15.99 cfs @ 12.17 hrs. Volume= 56.516 cf = 5.37 cfs @ 12.56 hrs, Volume= Outflow 39,603 cf, Atten= 66%, Lag= 23.5 min = 0.48 cfs @ 10.55 hrs, Volume= Discarded = 18,288 cf 4.89 cfs @ 12.56 hrs, Volume= Primary = 21,315 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 173.27' @ 12.56 hrs Surf.Area= 8,648 sf Storage= 23,671 cf

Plug-Flow detention time= 124.0 min calculated for 39,603 cf (70% of inflow) Center-of-Mass det. time= 57.7 min (849.4 - 791.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	169.50'	11,805 cf	44.75'W x 193.25'L x 5.75'H Field A
			49,726 cf Overall - 20,213 cf Embedded = 29,513 cf x 40.0% Voids
#2A	170.25'	20,213 cf	Cultec R-900HD x 162 Inside #1
			Effective Size= 72.7"W x 48.0"H => 17.61 sf x 7.00'L = 123.3 cf
			Overall Size= 78.0"W x 48.0"H x 9.25'L with 2.25' Overlap
_			Row Length Adjustment= +2.25' x 17.61 sf x 6 rows
		22.019 of	Total Available Storage

32,018 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	172.25'	24.0" Round Culvert L= 25.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= $172.25' / 163.50'$ S= 0.3500 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf 2.410 in/br Exfiltration over Surface area
	Biobalada	100100	

Discarded OutFlow Max=0.48 cfs @ 10.55 hrs HW=169.56' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.48 cfs)

Primary OutFlow Max=4.87 cfs @ 12.56 hrs HW=173.27' (Free Discharge) ←1=Culvert (Inlet Controls 4.87 cfs @ 3.03 fps)

Pond T18A: TRENCH 18A - Chamber Wizard Field A

Chamber Model = Cultec R-900HD

Effective Size= 72.7"W x 48.0"H => 17.61 sf x 7.00'L = 123.3 cf Overall Size= 78.0"W x 48.0"H x 9.25'L with 2.25' Overlap Row Length Adjustment= +2.25' x 17.61 sf x 6 rows

78.0" Wide + 9.0" Spacing = 87.0" C-C Row Spacing

27 Chambers/Row x 7.00' Long +2.25' Row Adjustment = 191.25' Row Length +12.0" End Stone x 2 = 193.25' Base Length 6 Rows x 78.0" Wide + 9.0" Spacing x 5 + 12.0" Side Stone x 2 = 44.75' Base Width 9.0" Base + 48.0" Chamber Height + 12.0" Cover = 5.75' Field Height

162 Chambers x 123.3 cf +2.25' Row Adjustment x 17.61 sf x 6 Rows = 20,212.9 cf Chamber Storage

49,725.6 cf Field - 20,212.9 cf Chambers = 29,512.7 cf Stone x 40.0% Voids = 11,805.1 cf Stone Storage

Chamber Storage + Stone Storage = 32,018.0 cf = 0.735 af Overall Storage Efficiency = 64.4%

162 Chambers 1,841.7 cy Field 1,093.1 cy Stone



 $\square \square \square \square \square \square \square \square$



Pond T18A: TRENCH 18A
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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment AR: Abutter Runoff	Runoff Area=449,581 sf 25.00% Impervious Runoff Depth>3.58" Flow Length=2,249' Tc=32.7 min CN=85 Runoff=24.92 cfs 134,100 cf
Subcatchment CR: Charles River	Runoff Area=1,756,054 sf 7.37% Impervious Runoff Depth>2.55" Flow Length=2,022' Tc=29.7 min CN=74 Runoff=73.98 cfs 373,200 cf
SubcatchmentIR: Intermediate Roa	dway Runoff Area=69,032 sf 72.77% Impervious Runoff Depth>3.90" Flow Length=1,790' Tc=17.9 min CN=88 Runoff=5.29 cfs 22,447 cf
Subcatchment MC: Main Campus	Runoff Area=267,248 sf 56.20% Impervious Runoff Depth>3.21" Flow Length=1,577' Tc=12.0 min CN=81 Runoff=20.11 cfs 71,465 cf
SubcatchmentOSW: Off Site West	Runoff Area=31,028 sf 0.60% Impervious Runoff Depth>1.90" Flow Length=178' Tc=7.7 min CN=66 Runoff=1.57 cfs 4,925 cf
Subcatchment PD: Pond Drive	Runoff Area=122,569 sf 50.22% Impervious Runoff Depth>3.90" Flow Length=1,773' Tc=16.0 min CN=88 Runoff=9.83 cfs 39,876 cf
Reach TCR: Total Flow to Charles R	Inflow=108.27 cfs 548,294 cf Outflow=108.27 cfs 548,294 cf
Pond B1: BASIN 1 Discarde	Peak Elev=178.55' Storage=12,700 cf Inflow=5.29 cfs 22,447 cf ed=0.38 cfs 12,960 cf Primary=0.00 cfs 0 cf Outflow=0.38 cfs 12,960 cf
Pond B3: BASIN 3 Discarded=0	Peak Elev=178.36' Storage=23,942 cf Inflow=9.83 cfs 39,876 cf .43 cfs 15,221 cf Primary=0.26 cfs 6,321 cf Outflow=0.69 cfs 21,542 cf
Pond T18A: TRENCH 18A Discarded=0.4	Peak Elev=173.75' Storage=26,371 cf Inflow=20.11 cfs 71,465 cf 48 cfs 19,325 cf Primary=9.34 cfs 34,673 cf Outflow=9.82 cfs 53,998 cf
	10 of Dun off Values - 040 044 of Augusta Dun off Danth - 0.00

Total Runoff Area = 2,695,512 sf Runoff Volume = 646,014 cf Average Runoff Depth = 2.88" 81.30% Pervious = 2,191,537 sf 18.70% Impervious = 503,975 sf

Summary for Subcatchment AR: Abutter Runoff

Runoff = 24.92 cfs @ 12.44 hrs, Volume= 134,100 cf, Depth> 3.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

A	rea (sf)	CN E	Description		
	1,629	70 1	/2 acre lots	s, 25% imp	, HSG B
4	47,952	85 1	/2 acre lots	<u>s, 25% imp</u>	, HSG D
4	49,581	85 V	Veighted A	verage	
3	37,186	7	'5.00% Per	vious Area	
1	12,395	2	5.00% Imp	pervious Are	ea
Т	المربع مرالم	01	\/_l!+	0	Description
IC (mim)	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(π/π)	(ft/sec)	(CTS)	
9.3	50	0.0400	0.09		Sheet Flow, Sheet AB
					Woods: Light underbrush n= 0.400 P2= 3.20"
1.5	253	0.0320	2.88		Shallow Concentrated Flow, Wooded BC
					Unpaved Kv= 16.1 fps
0.1	40	0.0050	4.97	8.78	Pipe Channel, Pipe CD
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
					n= 0.011 Concrete pipe, straight & clean
21.6	1,862	0.0080	1.44		Shallow Concentrated Flow, Wetland/Strea/Pond DE
					Unpaved Kv= 16.1 fps
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River EF
					Unpaved Kv= 16.1 fps
32.7	2,249	Total			



Subcatchment AR: Abutter Runoff

Summary for Subcatchment CR: Charles River

Runoff = 73.98 cfs @ 12.42 hrs, Volume= 373,200 cf, Depth> 2.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

_	A	rea (sf)	CN	Description		
		10,067	30	Woods, Go	od, HSG A	
		5,689	39	>75% Gras	s cover, Go	ood, HSG A
*		3,253	78	Wetland, H	SG A	
*		205	72	Path, HSG	A	
	2	03,113	55	Woods, Go	od, HSG B	
	2	11,820	61	>75% Gras	s cover, Go	ood, HSG B
*	1	03,465	78	Wetlands, H	ISG B	
*		10,318	82	Path, HSG	В	
*		2,704	80	Path in Res	ource, HSC	G B
		4,112	98	Water Surfa	ace, HSG B	
		33,426	70	Woods, Go	od, HSG C	
		758	74	>75% Gras	s cover, Go	ood, HSG C
*	1	41,675	78	Wetlands, H	ISG C	
*		3,310	87	Path, HSG	С	
*		6,129	80	Path in Res	ource, HSC	GC
		10,807	98	Water Surfa	ace, HSG C	
	4	58,293	77	Woods, Go	od, HSG D	
		65,768	80	>75% Gras	s cover, Go	ood, HSG D
*	2	27,701	78	Wetlands, H	ISG D	
*		27,658	89	Path, HSG	D	
*		9,556	80	Path in Res	ource, HSC	G D
		45,917	98	Water Surfa	ace, HSG D	
		20,004	70	1/2 acre lot	s, 25% imp	, HSG B
		54,729	80	1/2 acre lot	s, 25% imp	, HSG C
		60,917	85	1/2 acre lot	s, 25% imp	, HSG D
*		34,660	98	impervious		
	1,7	56,054	74	Weighted A	verage	
	1,6	26,646		92.63% Pei	vious Area	
	1	29,409		7.37% Impe	ervious Area	a
	Т	1	01.000		O an a aite	Description
	(min)	(foot)	Siope		Capacity	Description
_					(05)	Chast Flow, Chast A.D.
	7.9	50	0.0600	0.10		Sheet Flow, Sheet A-B
	2.1	220	0.0120	1 76		Shallow Concentrated Elew Watland P.C.
	5.1	329	0.0120	1.70		Uppoved Ky 16.1 fpc
	195	1 500	0 0080	1 1 1		Shallow Concentrated Flow Wetland/Stream/Bond C-F
	10.5	1,099	0.0000	, 1.44		Unnaved Ky-161 frs
	02	ΛΛ	0 0000) / 83		Shallow Concentrated Flow Pond to River D-F
	0.2		0.0300	, 4.00		Unpaved Ky= 16.1 fps
	29.7	2 022	Total			
	20.1	2,022	i otai			



Subcatchment CR: Charles River

Summary for Subcatchment IR: Intermediate Roadway

Runoff = 5.29 cfs @ 12.24 hrs, Volume= 22,447 cf, Depth> 3.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

A	rea (sf)	CN D	Description		
	17,093	61 >	75% Gras	s cover, Go	ood, HSG B
	1,704	80 >	75% Gras	s cover, Go	od, HSG D
	28,466	98 F	aved road	s w/curbs 8	k sewers, HSG B
	8,209	98 F	aved road	s w/curbs &	& sewers, HSG D
*	13,560	98 C	Cottages		
	69,032	88 V	Veighted A	verage	
	18,797	2	7.23% Per	vious Area	
	50,235	7	2.77% Imp	pervious Are	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
5.6	50	0.0200	0.15		Sheet Flow, Sheet A-B
					Grass: Short n= 0.150 P2= 3.20"
0.1	9	0.0200	2.28		Shallow Concentrated Flow, Grass B-C
					Unpaved Kv= 16.1 fps
0.3	47	0.0200	2.87		Shallow Concentrated Flow, Paved C-D
0.4	500	0.0050	0.04	0.50	Paved Kv= 20.3 fps
3.1	593	0.0050	3.21	2.52	Pipe Channel, Pipe D-E
					12.0 Round Area= 0.8 SI Perim= 3.1 T= 0.25
0.2	150		0 00		leko er Beservoir, Besin E E
0.5	155		0.02		Lake of Reservoir, Dasin E-F
05	46	0 0050	1 54	0 13	Dine Channel Dine E-E
0.0	-0	0.0000	1.04	0.10	4.0" Round Area= 0.1 sf Perim= 1.0' r= 0.08'
					n=0.013 Corrugated PE smooth interior
1.4	149	0.0130	1.84		Shallow Concentrated Flow, Unpaved
		0.0.00			Unpaved Kv= 16.1 fps
2.4	333	0.0200	2.28		Shallow Concentrated Flow, Unpaved
-					Unpaved Kv= 16.1 fps
4.2	410	0.0100	1.61		Shallow Concentrated Flow, Unpaved
					Unpaved Kv= 16.1 fps
4 - 0	4 700	-			

17.9 1,790 Total



Subcatchment IR: Intermediate Roadway

Summary for Subcatchment MC: Main Campus

Runoff = 20.11 cfs @ 12.17 hrs, Volume= 71,465 cf, Depth> 3.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

A	rea (sf)	CN D	escription						
	22,404	39 >	39 >75% Grass cover, Good, HSG A						
	82,752	61 >	75% Gras	s cover, Go	ood, HSG B				
	11,890	80 >	75% Gras	s cover, Go	bod, HSG D				
	30,503	98 P	aved road	s w/curbs &	k sewers, HSG A				
	96,592	98 P	aved road	S W/CURDS &	k sewers, HSG B				
	23,107	90 F	Aveu IUau						
ے 1	.07,240 17.046		2 80% Por	verage vious Area					
1	50 202	5	5.00 % l ei 6 20% lmr	vious Area	ea				
•	00,202	Ŭ	0120701111						
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
5.0	43	0.0200	0.14		Sheet Flow, Sheet Grass A-B				
					Grass: Short n= 0.150 P2= 3.20"				
0.1	7	0.0200	0.81		Sheet Flow, Sheet-Pave B-C				
					Smooth surfaces $n=0.011$ P2= 3.20"				
1.3	217	0.0200	2.87		Shallow Concentrated Flow, Paved C-D				
1 1	211	0.0050	2 21	2 5 2	Paved KV= 20.3 Ips				
1.1	211	0.0050	3.21	2.52	12.0" Round Area -0.8 sf Perim -3.1 ' r -0.25 '				
					n = 0.013 Corrugated PE smooth interior				
1.6	397	0.0050	4 20	7 43	Pipe Channel, Pipe E-F				
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'				
					n= 0.013 Corrugated PE, smooth interior				
1.6	490	0.0050	5.09	16.00	Pipe Channel, Pipe F-G				
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'				
					n= 0.013 Corrugated PE, smooth interior				
0.0	24		8.97		Lake or Reservoir, Lake G-H				
					Mean Depth= 2.50'				
0.5	42	0.0050	1.54	0.13	Pipe Channel, Pipe F-G				
					4.0" Round Area= 0.1 st Perim= 1.0' r= 0.08'				
0.0	110	0.0400	2 22		n= 0.013 Confugated PE, smooth Interior				
0.8	140	0.0400	3.22		Shahow Concentrated Flow, Unpaved I-J				
					Unpaveu IV-10.1 lps				

12.0 1,577 Total



Subcatchment MC: Main Campus

Summary for Subcatchment OSW: Off Site West

Runoff = 1.57 cfs @ 12.12 hrs, Volume= 4,925 cf, Depth> 1.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

	A	rea (sf)	CN	Description		
		2,983	55	Woods, Go	od, HSG B	
		15,112	61	>75% Gras	s cover, Go	ood, HSG B
*		1,048	80	Path(cover	unknown)	
		185	98	Unconnect	ed pavemer	nt, HSG B
		8,058	80	>75% Gras	s cover, Go	ood, HSG D
*		3,642	60	Permeable	Parking Are	ea
		31,028	66	Weighted A	Verage	
		30,843		99.40% Pe	rvious Area	
		185		0.60% Imp	ervious Area	a
		185		100.00% Ü	nconnected	1
	Тс	Length	Slop	e Velocity	Capacity	Description
(n	nin)	(feet)	(ft/f	t) (ft/sec)	(cfs)	·
	7.1	50	0.080	0 0.12		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.20"
	0.6	128	0.054	0 3.74		Shallow Concentrated Flow, Wooded/Path/Wooded B-C
						Unpaved Kv= 16.1 fps
	7.7	178	Total			

Subcatchment OSW: Off Site West



Summary for Subcatchment PD: Pond Drive

Runoff = 9.83 cfs @ 12.21 hrs, Volume= 39,876 cf, Depth> 3.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

A	rea (sf)	CN D	escription						
	1,964	61 >	61 >75% Grass cover, Good, HSG B						
	5,597	98 P	aved road	s w/curbs &	k sewers, HSG B				
	25,437	77 V	/oods, Go	od, HSG D					
	33,576	80 >	75% Gras	s cover, Go	od, HSG D				
×	43	89 P	ath, HSG	D a.u./a.urba G					
	<u>55,952</u>	<u>98 P</u>	aved road	S W/CUIDS &	sewers, HSG D				
1	22,569	88 V	/eighted A	verage					
	61,020	4	9.78% Per	vious Area					
	61,549	5	0.22% imp	ervious Are	38				
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·				
7.9	50	0.0600	0.10		Sheet Flow, Sheet A-B				
					Woods: Light underbrush n= 0.400 P2= 3.20"				
0.3	55	0.0400	3.22		Shallow Concentrated Flow, Grass B-C				
					Unpaved Kv= 16.1 fps				
0.8	136	0.0200	2.87		Shallow Concentrated Flow, Paved C-D				
				= 10	Paved Kv= 20.3 fps				
4.0	1,006	0.0050	4.20	7.43	Pipe Channel, Pipe D-E				
					18.0° Round Area= 1.8 st Perim= 4.7° r= 0.38°				
0.6	107	0.0050	E 00	16.00	n= 0.013 Corrugated PE, smooth Interior				
0.0	197	0.0050	5.09	10.00	Pipe Champel, Fipe E-F $24.0^{"}$ Pound Aroa- 3.1 sf Porim- 6.3' r- 0.50'				
					n = 0.013 Corrugated PE smooth interior				
02	77		8 02		Lake or Reservoir Basin F-G				
0.2			0.02		Mean Depth= $2.00'$				
0.5	62	0.0050	2.02	0.40	Pipe Channel, Pipe G-H				
					6.0" Round Area= 0.2 sf Perim= 1.6' r= 0.13'				
					n= 0.013 Corrugated PE, smooth interior				
0.7	89	0.0200	2.28		Shallow Concentrated Flow, Unpaved H-I				
					Unpaved Kv= 16.1 fps				
0.8	57	0.0050	1.14		Shallow Concentrated Flow, Unpaved I-J				
					Unpaved Kv= 16.1 fps				
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Upaved J-K				
					Unpaved Kv= 16.1 tps				

16.0 1,773 Total

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Subcatchment PD: Pond Drive

Summary for Reach TCR: Total Flow to Charles River

Inflow /	Area =	2,664,484 sf,	18.91% Impervious,	Inflow Depth > 2.47	7" for 25-Year event
Inflow	=	108.27 cfs @	12.43 hrs, Volume=	548,294 cf	
Outflow	v =	108.27 cfs @	12.43 hrs, Volume=	548,294 cf, At	ten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach TCR: Total Flow to Charles River

Summary for Pond B1: BASIN 1

Inflow Area	ι =	69,032 sf,	72.77% In	npervious,	Inflow Depth >	3.90"	for 25-	Year event	
Inflow	=	5.29 cfs @	12.24 hrs,	Volume=	22,447 c	f			
Outflow	=	0.38 cfs @	14.59 hrs,	Volume=	12,960 c	f, Atten	= 93%,	Lag= 141.0 m	າin
Discarded	=	0.38 cfs @	14.59 hrs,	Volume=	12,960 c	f		-	
Primary	=	0.00 cfs @	5.00 hrs,	Volume=	0 C	f			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.55' @ 14.59 hrs Surf.Area= 6,738 sf Storage= 12,700 cf

Plug-Flow detention time= 190.4 min calculated for 12,916 cf (58% of inflow) Center-of-Mass det. time= 114.2 min (887.7 - 773.5)

Volume	Inver	t Avail.Sto	rage Storage	e Description	
#1	176.00	' 33,72	22 cf Custor	n Stage Data (Pr	rismatic)Listed below (Recalc)
E 1				0	
Elevatio	on S	Surf.Area	Inc.Store	Cum.Store	
(tee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
176.0	00	3,342	0	0	
177.0	00	4,577	3,960	3,960	
178.0	00	5,952	5,265	9,224	
179.0	00	7,387	6,670	15,894	
180.0	00	8,885	8,136	24,030	
181.0	00	10,500	9,693	33,722	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	174.00'	4.0" Round	Culvert	
	-		L= 36.0' CP	P, mitered to cor	nform to fill, Ke= 0.700
			Inlet / Outlet	Invert= 174.00' /	173.50' S= 0.0139 '/' Cc= 0.900
			n= 0.010 PV	C, smooth interio	or, Flow Area= 0.09 sf
#2	Device 1	179.00'	6.0" Vert. Or	rifice/Grate C=	0.600
#3	Device 1	179.25'	1.0" Vert. Or	rifice/Grate C=	0.600
#4	Device 1	179.50'	24.0" x 24.0'	" Horiz. Orifice/0	Grate C= 0.600
			Limited to we	eir flow at low hea	ads
#5	Primary	179.90'	20.0' long x	5.0' breadth Bro	oad-Crested Rectangular Weir
	2		Head (feet)	0.20 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3	.50 4.00 4.50 5	.00 5.50
			Coef. (Englis	h) 2.34 2.50 2.	70 2.68 2.68 2.66 2.65 2.65 2.65
			2.65 2.67 2	.66 2.68 2.70 2	.74 2.79 2.88
#6	Discarded	176.00'	2.410 in/hr E	Exfiltration over	Surface area
			-		

Discarded OutFlow Max=0.38 cfs @ 14.59 hrs HW=178.55' (Free Discharge) **G=Exfiltration** (Exfiltration Controls 0.38 cfs)

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=176.00' (Free Discharge)

-1=Culvert (Passes 0.00 cfs of 0.48 cfs potential flow)

2=Orifice/Grate (Controls 0.00 cfs)

-3=Orifice/Grate (Controls 0.00 cfs)

4=Orifice/Grate (Controls 0.00 cfs)

-5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B1: BASIN 1

Summary for Pond B3: BASIN 3

Inflow Area	I =	122,569 sf,	50.22% In	npervious,	Inflow Depth >	3.90"	for 25-	Year event	
Inflow	=	9.83 cfs @	12.21 hrs,	Volume=	39,876 c	f			
Outflow	=	0.69 cfs @	14.43 hrs,	Volume=	21,542 c	f, Atten	= 93%,	Lag= 133.0 m	in
Discarded	=	0.43 cfs @	14.43 hrs,	Volume=	15,221 c	f		-	
Primary	=	0.26 cfs @	14.43 hrs,	Volume=	6,321 c	f			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.36' @ 14.43 hrs Surf.Area= 7,492 sf Storage= 23,942 cf

Plug-Flow detention time= 207.5 min calculated for 21,470 cf (54% of inflow) Center-of-Mass det. time= 127.7 min (899.6 - 771.9)

Volume	Inver	t Avail.Sto	rage Storage E	Description		
#1	174.00	' 38,01	0 cf Custom	Stage Data (Coni	c)Listed below (Re	calc)
Elevatio (fee	on S et)	urf.Area (sɑ-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sg-ft)	
174.0 175.0 176.0 177.0 178.0 178.0	20 20 20 20 20 20 20	3,673 4,455 5,293 6,187 7,138 8,146	0 4,058 4,868 5,734 6,657 7,636 0,057	0 4,058 8,926 14,660 21,317 28,953 28,010	3,673 4,487 5,361 6,294 7,288 8,343	
Device	Routing	Invert	9,057 Outlet Devices	38,010	10,227	
#1	Primary	168.00'	6.0" Round C L= 53.0' CPP, Inlet / Outlet In n= 0.010 PVC	ulvert , mitered to confor vert= 168.00' / 160 , smooth interior,	rm to fill, Ke= 0.70 6.94' S= 0.0200 '/' Flow Area= 0.20 s) Cc= 0.900 f
#2 #3	Device 1 Device 1	177.00' 178.50'	3.0" Vert. Orifi 24.0" x 48.0" H Limited to weir	ce/Grate C= 0.6 loriz. Orifice/Gra	te C= 0.600	
#4	Primary	178.90'	20.0' long x 5 Head (feet) 0.2 2.50 3.00 3.50 Coef. (English) 2.65 2.67 2.66	O' breadth Broad 20 0.40 0.60 0.8 0 4.00 4.50 5.00 2.34 2.50 2.70 6 2.68 2.70 2.74	d-Crested Rectang 0 1.00 1.20 1.40 0 5.50 2.68 2.68 2.66 2 2.79 2.88	Jular Weir 1.60 1.80 2.00 .65 2.65 2.65
#5	Discarded	174.00'	2.410 in/hr Ext	filtration over We	etted area	

Discarded OutFlow Max=0.43 cfs @ 14.43 hrs HW=178.36' (Free Discharge) **5=Exfiltration** (Exfiltration Controls 0.43 cfs)

Primary OutFlow Max=0.26 cfs @ 14.43 hrs HW=178.36' (Free Discharge)

1=Culvert (Passes 0.26 cfs of 2.55 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.26 cfs @ 5.35 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

-4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B3: BASIN 3

Summary for Pond T18A: TRENCH 18A

Inflow Area = 267,248 sf, 56.20% Impervious, Inflow Depth > 3.21" for 25-Year event Inflow 20.11 cfs @ 12.17 hrs. Volume= 71.465 cf = 9.82 cfs @ 12.43 hrs, Volume= Outflow 53,998 cf, Atten= 51%, Lag= 16.1 min = 0.48 cfs @ 10.00 hrs, Volume= Discarded = 19.325 cf Primary = 9.34 cfs @ 12.43 hrs, Volume= 34,673 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 173.75' @ 12.43 hrs Surf.Area= 8,648 sf Storage= 26,371 cf

Plug-Flow detention time= 103.1 min calculated for 53,819 cf (75% of inflow) Center-of-Mass det. time= 44.7 min (831.0 - 786.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	169.50'	11,805 cf	44.75'W x 193.25'L x 5.75'H Field A
			49,726 cf Overall - 20,213 cf Embedded = 29,513 cf x 40.0% Voids
#2A	170.25'	20,213 cf	Cultec R-900HD x 162 Inside #1
			Effective Size= 72.7"W x 48.0"H => 17.61 sf x 7.00'L = 123.3 cf
			Overall Size= 78.0"W x 48.0"H x 9.25'L with 2.25' Overlap
_			Row Length Adjustment= +2.25' x 17.61 sf x 6 rows
		22.019 of	Total Available Storage

32,018 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	172.25'	24.0" Round Culvert L= 25.0' CPP, mitered to conform to fill, Ke= 0.700
#2	Discarded	169.50'	Inlet / Outlet Invert= 172.25' / 163.50' S= 0.3500 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf 2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.48 cfs @ 10.00 hrs HW=169.56' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.48 cfs)

Primary OutFlow Max=9.30 cfs @ 12.43 hrs HW=173.75' (Free Discharge) ↓ 1=Culvert (Inlet Controls 9.30 cfs @ 3.68 fps)

Pond T18A: TRENCH 18A - Chamber Wizard Field A

Chamber Model = Cultec R-900HD

Effective Size= 72.7"W x 48.0"H => 17.61 sf x 7.00'L = 123.3 cf Overall Size= 78.0"W x 48.0"H x 9.25'L with 2.25' Overlap Row Length Adjustment= +2.25' x 17.61 sf x 6 rows

78.0" Wide + 9.0" Spacing = 87.0" C-C Row Spacing

27 Chambers/Row x 7.00' Long +2.25' Row Adjustment = 191.25' Row Length +12.0" End Stone x 2 = 193.25' Base Length 6 Rows x 78.0" Wide + 9.0" Spacing x 5 + 12.0" Side Stone x 2 = 44.75' Base Width 9.0" Base + 48.0" Chamber Height + 12.0" Cover = 5.75' Field Height

162 Chambers x 123.3 cf +2.25' Row Adjustment x 17.61 sf x 6 Rows = 20,212.9 cf Chamber Storage

49,725.6 cf Field - 20,212.9 cf Chambers = 29,512.7 cf Stone x 40.0% Voids = 11,805.1 cf Stone Storage

Chamber Storage + Stone Storage = 32,018.0 cf = 0.735 af Overall Storage Efficiency = 64.4%

162 Chambers 1,841.7 cy Field 1,093.1 cy Stone



 $\square \square \square \square \square \square \square \square$



Pond T18A: TRENCH 18A

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment AR: Abutter Runoff	Runoff Area=449,581 sf 25.00% Impervious Runoff Depth>4.65" Flow Length=2,249' Tc=32.7 min CN=85 Runoff=31.99 cfs 174,258 cf
Subcatchment CR: Charles River	Runoff Area=1,756,054 sf 7.37% Impervious Runoff Depth>3.50" Flow Length=2,022' Tc=29.7 min CN=74 Runoff=101.35 cfs 512,314 cf
Subcatchment IR: Intermediate Roa	dway Runoff Area=69,032 sf 72.77% Impervious Runoff Depth>5.00" Flow Length=1,790' Tc=17.9 min CN=88 Runoff=6.69 cfs 28,748 cf
Subcatchment MC: Main Campus	Runoff Area=267,248 sf 56.20% Impervious Runoff Depth>4.25" Flow Length=1,577' Tc=12.0 min CN=81 Runoff=26.36 cfs 94,604 cf
SubcatchmentOSW: Off Site West	Runoff Area=31,028 sf 0.60% Impervious Runoff Depth>2.74" Flow Length=178' Tc=7.7 min CN=66 Runoff=2.29 cfs 7,093 cf
Subcatchment PD: Pond Drive	Runoff Area=122,569 sf 50.22% Impervious Runoff Depth>5.00" Flow Length=1,773' Tc=16.0 min CN=88 Runoff=12.42 cfs 51,067 cf
Reach TCR: Total Flow to Charles R	Inflow=149.08 cfs 757,504 cf Outflow=149.08 cfs 757,504 cf
Pond B1: BASIN 1 Discarded=	Peak Elev=179.13' Storage=16,904 cf Inflow=6.69 cfs 28,748 cf =0.42 cfs 14,887 cf Primary=0.05 cfs 434 cf Outflow=0.48 cfs 15,322 cf
Pond B3: BASIN 3 Discarded=0.4	Peak Elev=178.72' Storage=26,745 cf Inflow=12.42 cfs 51,067 cf 45 cfs 16,404 cf Primary=2.59 cfs 14,522 cf Outflow=3.04 cfs 30,926 cf
Pond T18A: TRENCH 18A Discarded=0.48	Peak Elev=174.74' Storage=30,266 cf Inflow=26.36 cfs 94,604 cf cfs 20,647 cf Primary=16.31 cfs 55,975 cf Outflow=16.79 cfs 76,622 cf
Total Runoff Area - 2 695 4	512 sf Runoff Volume - 868 085 cf Average Runoff Denth - 3.86

Total Runoff Area = 2,695,512 sf Runoff Volume = 868,085 cf Average Runoff Depth = 3.86" 81.30% Pervious = 2,191,537 sf 18.70% Impervious = 503,975 sf

Summary for Subcatchment AR: Abutter Runoff

Runoff = 31.99 cfs @ 12.44 hrs, Volume= 174,258 cf, Depth> 4.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

A	rea (sf)	CN E	Description		
	1,629	70 1	/2 acre lots	s, 25% imp	, HSG B
4	47,952	85 1	/2 acre lots	<u>s, 25% imp</u>	, HSG D
4	49,581	85 V	Veighted A	verage	
3	37,186	7	'5.00% Per	vious Area	
1	12,395	2	5.00% Imp	pervious Are	ea
Т	المربع مرالم	01	\/_l!+	0	Description
IC (mim)	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(π/π)	(ft/sec)	(CTS)	
9.3	50	0.0400	0.09		Sheet Flow, Sheet AB
					Woods: Light underbrush n= 0.400 P2= 3.20"
1.5	253	0.0320	2.88		Shallow Concentrated Flow, Wooded BC
					Unpaved Kv= 16.1 fps
0.1	40	0.0050	4.97	8.78	Pipe Channel, Pipe CD
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'
					n= 0.011 Concrete pipe, straight & clean
21.6	1,862	0.0080	1.44		Shallow Concentrated Flow, Wetland/Strea/Pond DE
					Unpaved Kv= 16.1 fps
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Pond to River EF
					Unpaved Kv= 16.1 fps
32.7	2,249	Total			



Subcatchment AR: Abutter Runoff

Summary for Subcatchment CR: Charles River

Runoff = 101.35 cfs @ 12.41 hrs, Volume= 512,314 cf, Depth> 3.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

	A	rea (sf)	CN	Description		
		10,067	30	Woods, Go	od, HSG A	
		5,689	39	>75% Gras	s cover, Go	ood, HSG A
*		3,253	78	Wetland, H	SG A	
*		205	72	Path, HSG	A	
	2	03,113	55	Woods, Go	od, HSG B	
	2	11,820	61	>75% Gras	s cover, Go	ood, HSG B
*	1	03,465	78	Wetlands, H	ISG B	
*		10,318	82	Path, HSG	В	
*		2,704	80	Path in Res	ource, HSC	G B
		4,112	98	Water Surfa	ace, HSG B	
		33,426	70	Woods, Go	od, HSG C	
		758	74	>75% Gras	s cover, Go	ood, HSG C
*	1	41,675	78	Wetlands, H	ISG C	
*		3,310	87	Path, HSG	С	
*		6,129	80	Path in Res	ource, HSC	G C
		10,807	98	Water Surfa	ace, HSG C	
	4	58,293	77	Woods, Go	od, HSG D	
		65,768	80	>75% Gras	s cover, Go	ood, HSG D
*	2	27,701	78	Wetlands, H	ISG D	
*		27,658	89	Path, HSG	D	
*		9,556	80	Path in Res	ource, HSC	G D
		45,917	98	Water Surfa	ace, HSG D	
		20,004	70	1/2 acre lot	s, 25% imp	, HSG B
		54,729	80	1/2 acre lot	s, 25% imp	, HSG C
		60,917	85	1/2 acre lot	s, 25% imp	, HSG D
*		34,660	98	impervious		
	1,7	56,054	74	Weighted A	verage	
	1,6	26,646		92.63% Per	vious Area	
	1	29,409		7.37% Impe	ervious Are	a
	_		•		a	- · · · ·
		Length	Slope	e Velocity	Capacity	Description
_	(min)	(teet)	(ft/ft) (Tt/SeC)	(CIS)	
	7.9	50	0.0600) 0.10		Sheet Flow, Sheet A-B
	0.4	000	0.0400	4 70		Woods: Light underbrush n= 0.400 P2= 3.20"
	3.1	329	0.0120) 1.76		Shallow Concentrated Flow, Wetland B-C
	40.5	4 500	0 0000			Unpaved KV= 16.1 fps
	18.5	1,599	0.0080) 1.44		Snallow Concentrated Flow, Wetland/Stream/Pond C-L
	0.0	A A	0.0000	1 00		Unpaved KV= 10.1 Ips
	0.2	44	0.0900	4.83		Snallow Concentrated Flow, Pond to River D-E
		0.000	-			Unpaved KV= 16.1 Ips
	29.7	2,022	Iotal			



Subcatchment CR: Charles River

Summary for Subcatchment IR: Intermediate Roadway

Runoff = 6.69 cfs @ 12.24 hrs, Volume= 28,748 cf, Depth> 5.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

A	rea (sf)	CN D	Description								
	17,093	61 >	61 >75% Grass cover, Good, HSG B								
	1,704	80 >	80 >75% Grass cover, Good, HSG D								
	28,466	98 F	aved road	s w/curbs 8	k sewers, HSG B						
	8,209	98 F	aved road	s w/curbs &	& sewers, HSG D						
*	13,560	98 C	Cottages								
	69,032	88 V	Veighted A	verage							
	18,797	2	7.23% Per	vious Area							
	50,235	7	2.77% Imp	pervious Are	ea						
Tc	Length	Slope	Velocity	Capacity	Description						
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
5.6	50	0.0200	0.15		Sheet Flow, Sheet A-B						
					Grass: Short n= 0.150 P2= 3.20"						
0.1	9	0.0200	2.28		Shallow Concentrated Flow, Grass B-C						
	47		0.07		Unpaved Kv= 16.1 fps						
0.3	47	0.0200	2.87		Shallow Concentrated Flow, Paved C-D						
0.4	500	0.0050	2.24	0.50	Paved KV= 20.3 fps						
3.1	593	0.0050	3.21	2.52	12.0" Bound Area 0.8 of Darim 2.1' r 0.25'						
					12.0 Round Alea= 0.0 Si Pellin= 3.1 1= 0.25						
03	153		8 02		Lake or Reservoir Basin F-F						
0.5	100		0.02		Mean Denth- $2.00'$						
0.5	46	0 0050	1 54	0.13	Pine Channel Pine F-F						
0.0	10	0.0000	1.01	0.10	4.0" Round Area= 0.1 sf Perim= 1.0' r= 0.08'						
					n=0.013 Corrugated PE, smooth interior						
1.4	149	0.0130	1.84		Shallow Concentrated Flow, Unpaved						
					Unpaved Kv= 16.1 fps						
2.4	333	0.0200	2.28		Shallow Concentrated Flow, Unpaved						
					Unpaved Kv= 16.1 fps						
4.2	410	0.0100	1.61		Shallow Concentrated Flow, Unpaved						
					Unpaved Kv= 16.1 fps						

17.9 1,790 Total



Subcatchment IR: Intermediate Roadway

Summary for Subcatchment MC: Main Campus

Runoff = 26.36 cfs @ 12.16 hrs, Volume= 94,604 cf, Depth> 4.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

A	rea (sf)	CN D	escription							
	22,404	39 >	39 >75% Grass cover, Good, HSG A							
	82,752	61 >	75% Gras	s cover, Go	ood, HSG B					
	11,890	80 >	75% Gras	s cover, Go	bod, HSG D					
	30,503	98 P	aved road	s w/curbs &	k sewers, HSG A					
	96,592	98 P	aved road	S W/CURDS &	k sewers, HSG B					
	23,107	90 F	Aveu IUau							
ے 1	.07,240 17.046		2 80% Por	verage vious Area						
1	50 202	5	5.00 % l ei 6 20% lmr	vious Area	ea					
•	00,202	Ŭ	0120701111							
Тс	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
5.0	43	0.0200	0.14		Sheet Flow, Sheet Grass A-B					
					Grass: Short n= 0.150 P2= 3.20"					
0.1	7	0.0200	0.81		Sheet Flow, Sheet-Pave B-C					
					Smooth surfaces $n=0.011$ P2= 3.20"					
1.3	217	0.0200	2.87		Shallow Concentrated Flow, Paved C-D					
1 1	211	0.0050	2 21	2 5 2	Paved KV= 20.3 Ips					
1.1	211	0.0050	3.21	2.52	12.0" Round Area -0.8 sf Perim -3.1 ' r -0.25 '					
					n = 0.013 Corrugated PE smooth interior					
1.6	397	0.0050	4 20	7 43	Pipe Channel, Pipe E-F					
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'					
					n= 0.013 Corrugated PE, smooth interior					
1.6	490	0.0050	5.09	16.00	Pipe Channel, Pipe F-G					
					24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50'					
					n= 0.013 Corrugated PE, smooth interior					
0.0	24		8.97		Lake or Reservoir, Lake G-H					
					Mean Depth= 2.50'					
0.5	42	0.0050	1.54	0.13	Pipe Channel, Pipe F-G					
					4.0" Round Area= 0.1 st Perim= 1.0' r= 0.08'					
0.0	110	0.0400	2 22		n= 0.013 Confugated PE, smooth Interior					
0.8	140	0.0400	3.22		Shahow Concentrated Flow, Unpaved I-J					
					Unpaveu IV-10.1 lps					

12.0 1,577 Total



Subcatchment MC: Main Campus

Summary for Subcatchment OSW: Off Site West

Runoff = 2.29 cfs @ 12.12 hrs, Volume= 7,093 cf, Depth> 2.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

	Ar	rea (sf)	CN	Descriptior	n	
		2,983	55	Woods, Go	od, HSG B	
		15,112	61	>75% Gras	s cover, Go	ood, HSG B
*		1,048	80	Path(cover	unknown)	
		185	98	Unconnect	ed pavemer	nt, HSG B
		8,058	80	>75% Gras	s cover, Go	ood, HSG D
*		3,642	60	Permeable	Parking Are	ea
		31,028	66	Weighted A	Average	
		30,843		99.40% Pe	rvious Area	
		185		0.60% Imp	ervious Area	a
		185		100.00% Ü	Inconnected	1
	Тс	Length	Slop	e Velocity	Capacity	Description
(m	nin)	(feet)	(ft/f	t) (ft/sec)	(cfs)	
	7.1	50	0.080	0 0.12		Sheet Flow, A-B
						Woods: Light underbrush n= 0.400 P2= 3.20"
	0.6	128	0.054	0 3.74		Shallow Concentrated Flow, Wooded/Path/Wooded B-C
						Unpaved Kv= 16.1 fps
	7.7	178	Total			

Subcatchment OSW: Off Site West



Summary for Subcatchment PD: Pond Drive

Runoff = 12.42 cfs @ 12.21 hrs, Volume= 51,067 cf, Depth> 5.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"

A	rea (sf)	CN D	escription						
	1,964	61 >	61 >75% Grass cover, Good, HSG B						
	5,597	98 P	aved road	s w/curbs &	& sewers, HSG B				
	25,437	77 V	loods, Goo	od, HSG D					
	33,576	80 >	75% Grass	s cover, Go	ood, HSG D				
×	43	89 P	ath, HSG	D					
	55,952	<u>98 P</u>	aved road	s w/curbs &	k sewers, HSG D				
1	22,569	88 W	/eighted A	verage					
	61,020	4	9.78% Per	vious Area					
	61,549	5	0.22% Imp	ervious Are	ea				
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
7.9	50	0.0600	0.10		Sheet Flow, Sheet A-B				
					Woods: Light underbrush n= 0.400 P2= 3.20"				
0.3	55	0.0400	3.22		Shallow Concentrated Flow, Grass B-C				
					Unpaved Kv= 16.1 fps				
0.8	136	0.0200	2.87		Shallow Concentrated Flow, Paved C-D				
					Paved Kv= 20.3 fps				
4.0	1,006	0.0050	4.20	7.43	Pipe Channel, Pipe D-E				
					18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38'				
					n= 0.013 Corrugated PE, smooth interior				
0.6	197	0.0050	5.09	16.00	Pipe Channel, Pipe E-F				
					24.0" Round Area= 3.1 st Perim= 6.3' r= 0.50'				
0.0			0.00		n= 0.013 Corrugated PE, smooth interior				
0.2	11		8.02		Lake or Reservoir, Basin F-G				
0.5	60	0.0050	2.02	0.40	Mean Depth= 2.00 Dine Chennel, Dine C, H				
0.5	02	0.0050	2.02	0.40	Fipe Channel, Fipe G- Π				
					0.0 Round Alea 0.2 Si Feinn 1.0 $1 = 0.13$				
07	80	0 0200	2 28		Shallow Concentrated Flow Unnaved H-I				
0.7	03	0.0200	2.20		Unnaved Ky-161 fns				
0.8	57	0.0050	1.14		Shallow Concentrated Flow, Unpaved I-J				
0.0	01	210000			Unpaved Kv= 16.1 fps				
0.2	44	0.0900	4.83		Shallow Concentrated Flow, Upaved J-K				
	-				Unpaved Kv= 16.1 fps				

16.0 1,773 Total



Subcatchment PD: Pond Drive

Summary for Reach TCR: Total Flow to Charles River

Inflow /	Area =	2,664,484 sf,	18.91% Impervious,	Inflow Depth >	3.41"	for 100-Year event
Inflow	=	149.08 cfs @	12.41 hrs, Volume=	757,504 cf		
Outflov	v =	149.08 cfs @	12.41 hrs, Volume=	757,504 cf	, Atten	= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach TCR: Total Flow to Charles River

Summary for Pond B1: BASIN 1

Inflow Area	=	69,032 sf,	72.77% In	npervious,	Inflow Depth >	5.00"	for 100	-Year e	vent
Inflow	=	6.69 cfs @	12.24 hrs,	Volume=	28,748 c	f			
Outflow	=	0.48 cfs @	14.49 hrs,	Volume=	15,322 c	f, Atten	= 93%,	Lag= 13	35.0 min
Discarded	=	0.42 cfs @	14.49 hrs,	Volume=	14,887 c	f		-	
Primary	=	0.05 cfs @	14.49 hrs,	Volume=	434 c	f			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.13' @ 14.49 hrs Surf.Area= 7,589 sf Storage= 16,904 cf

Plug-Flow detention time= 194.6 min calculated for 15,320 cf (53% of inflow) Center-of-Mass det. time= 111.9 min (879.9 - 767.9)

Volume	Inver	t Avail.Sto	rage Storage	e Description	
#1	176.00)' 33,72	22 cf Custor	n Stage Data (Pi	rismatic)Listed below (Recalc)
Elevatio	on S	Surf.Area	Inc.Store	Cum.Store	
(tee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
176.0	00	3,342	0	0	
177.(00	4,577	3,960	3,960	
178.0	00	5,952	5,265	9,224	
179.0	00	7,387	6,670	15,894	
180.0	00	8,885	8,136	24,030	
181.(00	10,500	9,693	33,722	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	174.00'	4.0" Round	Culvert	
			L= 36.0' CP	P, mitered to cor	nform to fill, Ke= 0.700
			Inlet / Outlet	Invert= 174.00' /	173.50' S= 0.0139 '/' Cc= 0.900
			n= 0.010 PV	C, smooth interio	or, Flow Area= 0.09 sf
#2	Device 1	179.00'	6.0" Vert. Or	rifice/Grate C=	0.600
#3	Device 1	179.25'	1.0" Vert. Or	rifice/Grate C=	0.600
#4	Device 1	179.50'	24.0" x 24.0	" Horiz. Orifice/0	Grate C= 0.600
			Limited to we	eir flow at low hea	ads
#5	Primary	179.90'	20.0' long x	5.0' breadth Bro	oad-Crested Rectangular Weir
	,		Head (feet)	0.20 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3	.50 4.00 4.50 5	.00 5.50
			Coef (Englis	h) 234 250 2	70 2 68 2 68 2 66 2 65 2 65 2 65
			2 65 2 67 2	66 2 68 2 70 2	74 2 79 2 88
#6	Discarded	176 00'	2 410 in/hr F	xfiltration over	Surface area
	2.0001000		2		

Discarded OutFlow Max=0.42 cfs @ 14.49 hrs HW=179.13' (Free Discharge) **G=Exfiltration** (Exfiltration Controls 0.42 cfs)

Primary OutFlow Max=0.05 cfs @ 14.49 hrs HW=179.13' (Free Discharge)

-1=Culvert (Passes 0.05 cfs of 0.75 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.05 cfs @ 1.25 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

4=Orifice/Grate (Controls 0.00 cfs)

-5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B1: BASIN 1

Summary for Pond B3: BASIN 3

Inflow Area =		122,569 sf,	, 50.22% Impervious,	Inflow Depth > 5.00)" for 100-Year event
Inflow	=	12.42 cfs @	12.21 hrs, Volume=	51,067 cf	
Outflow	=	3.04 cfs @	12.72 hrs, Volume=	30,926 cf, At	ten= 76%, Lag= 30.6 min
Discarded	=	0.45 cfs @	12.72 hrs, Volume=	16,404 cf	-
Primary	=	2.59 cfs @	12.72 hrs, Volume=	14,522 cf	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.72' @ 12.72 hrs Surf.Area= 7,861 sf Storage= 26,745 cf

Plug-Flow detention time= 173.5 min calculated for 30,821 cf (60% of inflow) Center-of-Mass det. time= 99.3 min (865.7 - 766.4)

Volume	Invert	Avail.Sto	rage Storage I	Description				
#1	174.00	38,01	0 cf Custom	Stage Data (Coni	c) Listed below (Re	calc)		
Elevatio (fee	on S et)	urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)			
174.0 175.0 176.0 177.0 177.0 178.0 179.0	00 00 00 00 00 00 00	3,673 4,455 5,293 6,187 7,138 8,146	0 4,058 4,868 5,734 6,657 7,636 0,057	0 4,058 8,926 14,660 21,317 28,953 38,010	3,673 4,487 5,361 6,294 7,288 8,343			
Device	Routing	Invert	9,057 Outlet Devices	38,010	10,227			
#1	Primary	168.00'	6.0" Round Culvert L= 53.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 168.00' / 166.94' S= 0.0200 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.20 sf					
#2 #3	Device 1 Device 1	177.00' 178.50'	3.0" Vert. Orifice/Grate C= 0.600 24.0" x 48.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads					
#4	Primary	178.90'	20.0' long x 5.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.34 2.50 2.70 2.68 2.68 2.66 2.65 2.65 2.65 2.65 2.67 2.66 2.68 2.70 2.74 2.79 2.88					
#5	Discarded	174.00'	2.410 in/hr Exfiltration over Wetted area					

Discarded OutFlow Max=0.45 cfs @ 12.72 hrs HW=178.72' (Free Discharge) **5=Exfiltration** (Exfiltration Controls 0.45 cfs)

Primary OutFlow Max=2.59 cfs @ 12.72 hrs HW=178.72' (Free Discharge)

-1=Culvert (Barrel Controls 2.59 cfs @ 13.18 fps)

-2=Orifice/Grate (Passes < 0.30 cfs potential flow)

3=Orifice/Grate (Passes < 4.12 cfs potential flow)

-4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)
8548.0 - Salmon Senior Community - Medway - PropType III 24-hr100-Year Rainfall=6.70"Prepared by MicrosoftPrinted 10/9/2015HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLCPage 82



Pond B3: BASIN 3

Summary for Pond T18A: TRENCH 18A

Inflow Area = 267,248 sf, 56.20% Impervious, Inflow Depth > 4.25" for 100-Year event Inflow 26.36 cfs @ 12.16 hrs. Volume= 94.604 cf = 16.79 cfs @ 12.34 hrs, Volume= Outflow 76,622 cf, Atten= 36%, Lag= 10.2 min = 9.25 hrs, Volume= 20,647 cf Discarded = 0.48 cfs @ Primary = 16.31 cfs @ 12.34 hrs, Volume= 55,975 cf

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 174.74' @ 12.34 hrs Surf.Area= 8,648 sf Storage= 30,266 cf

Plug-Flow detention time= 86.1 min calculated for 76,367 cf (81% of inflow) Center-of-Mass det. time= 35.9 min (815.6 - 779.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	169.50'	11,805 cf	44.75'W x 193.25'L x 5.75'H Field A
			49,726 cf Overall - 20,213 cf Embedded = 29,513 cf x 40.0% Voids
#2A	170.25'	20,213 cf	Cultec R-900HD x 162 Inside #1
			Effective Size= 72.7"W x 48.0"H => 17.61 sf x 7.00'L = 123.3 cf
			Overall Size= 78.0"W x 48.0"H x 9.25'L with 2.25' Overlap
_			Row Length Adjustment= +2.25' x 17.61 sf x 6 rows
		22.019 of	Total Available Storage

32,018 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	172.25'	24.0" Round Culvert L= 25.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 172.25' / 163.50' S= 0.3500 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
#2	Discarded	169.50'	2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.48 cfs @ 9.25 hrs HW=169.56' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.48 cfs)

Primary OutFlow Max=16.25 cfs @ 12.34 hrs HW=174.73' (Free Discharge) **1=Culvert** (Inlet Controls 16.25 cfs @ 5.17 fps)

Pond T18A: TRENCH 18A - Chamber Wizard Field A

Chamber Model = Cultec R-900HD

Effective Size= 72.7"W x 48.0"H => 17.61 sf x 7.00'L = 123.3 cf Overall Size= 78.0"W x 48.0"H x 9.25'L with 2.25' Overlap Row Length Adjustment= +2.25' x 17.61 sf x 6 rows

78.0" Wide + 9.0" Spacing = 87.0" C-C Row Spacing

27 Chambers/Row x 7.00' Long +2.25' Row Adjustment = 191.25' Row Length +12.0" End Stone x 2 = 193.25' Base Length 6 Rows x 78.0" Wide + 9.0" Spacing x 5 + 12.0" Side Stone x 2 = 44.75' Base Width 9.0" Base + 48.0" Chamber Height + 12.0" Cover = 5.75' Field Height

162 Chambers x 123.3 cf +2.25' Row Adjustment x 17.61 sf x 6 Rows = 20,212.9 cf Chamber Storage

49,725.6 cf Field - 20,212.9 cf Chambers = 29,512.7 cf Stone x 40.0% Voids = 11,805.1 cf Stone Storage

Chamber Storage + Stone Storage = 32,018.0 cf = 0.735 af Overall Storage Efficiency = 64.4%

162 Chambers 1,841.7 cy Field 1,093.1 cy Stone



 $\square \square \square \square \square \square \square \square$



Pond T18A: TRENCH 18A

APPENDIX C

STORMWATER MANAGEMENT SYSTEM CLOSED DRAINAGE SYSTEM/PIPE SIZING CALCULATIONS DRAINAGE SYSTEM CALCULATIONS



Project Number: Project Name: Project Address: Client: Location: 8548.0 Salmon Health ARCPUD Village Street, Medway, MA Continuing Care Management Medway, MA Date:October 8, 2015Calculations by:JENCalculations date:October 8, 2015Checked by:TLDChecked Date:October 9, 2015

STORMWATER MANAGEMENT STANDARD 2 - PEAK RATE OF RUNOFF

Offsite West

DESIGN STORM (YEAR)	EXISTING PEAK RUNOFF (CFS)	PROPOSEDPEAK RUNOFF (CFS)	REDUCTION IN PEAK RUNOFF
2	0.46	0.40	13.0%
10	1.51	1.12	25.8%
20	2.18	1.57	28.0%
100	3.29	2.29	30.4%
	EXISTING TOTAL VOLUME (CF)	PROPOSED TOTAL RUNOFF (CF)	REDUCTION IN TOTAL RUNOFF
2	2,291	1,808	21.1%
2 10	2,291 6,000	1,808 4,203	21.1% 30.0%
2 10 20	2,291 6,000 8,389	1,808 4,203 5,682	21.1% 30.0% 32.3%

Charles River

	EXISTING PEAK RUNOFF	PROPOSED PEAK	REDUCTION IN PEAK
DESIGN STORM (YEAR)	(CFS)	RUNOFF (CFS)	RUNOFF
2	39.16	37.81	3.4%
10	86.05	80.62	6.3%
25	113.68	108.27	4.8%
100	157.2	149.08	5.2%
DESIGN STORM (YEAR)	EXISTING TOTAL VOLUME (CF)	PROPOSED TOTAL RUNOFF (CF)	REDUCTION IN TOTAL RUNOFF
2	211,274	197,814	6.4%
10	444,528	418,121	5.9%
25	584,111	548,294	6.1%
100	806,433	757,504	6.1%



Project Number: Project Name: Project Address: Client: Location: 8548 Salmon Health ARCPUD Village Street, Medway, MA Continuing Care Management Medway, MA
 Date:
 October 8, 2015

 Calculations by:
 JEN

 Calculations date:
 October 8, 2015

 Checked by:
 TLD

 Checked Date:
 October 9, 2015

STORMWATER MANAGEMENT STANDARD 3 - RECHARGE VOLUME

	HYDROLOGIC SOIL GROUP				TOTAL
	А	В	С	D	TOTAL
IMPERVIOUS AREA (S.F.)	57,688	301,626	50,370	114,789	524,473
INCHES OF RUNOFF TO BE RECHARGED	0.60	0.35	0.25	0.10	
REQUIRED RECHARGE VOLUME (FT ³)	2,884	8,797	1,049	957	13,688

CAPTURE AREA ADJUSTMENT - ADJUSTED MINIMUM REQUIRED RECHARGE VOLUME

MINIMUM OF 65% OF IMPERVIOUS AREA MUST BE DIRECTED TO THE RECHARGE BMP; 65 % IS =	340,907	SF	
IMPERVIOUS SITE AREA DRAINING TO BMP =	495,468	SF	94.5% PERCENTAGE OF IMPERVIOUS AREA DIVERTED TO INFILTRATION FACILITY
RATIO OF TOTAL IMPERVIOUS AREA TO IMPERVIOUS AREA DRAINING TO RECHARGE BMP =	1.06		=
ADJUSTED REQUIRED RECHARGE VOLUME=	14,489	CF	= RATIO OF IMPERVIOUS AREA x REQUIRED RECHARGE VOLUME
PROPOSED RECHARGE VOLUME	121,661	CF	TOTAL AVAILABLE RECHARGE VOLUME



Project Number: Project Name: Project Address: Client: Location:

8548.0	Date:	October 8, 2015
Salmon Health ARCPUD	Calculations by:	JEN
Village Street, Medway, MA	Calculations date:	October 8, 2015
Continuing Care Management	Checked by:	TLD
Medway, MA	Checked Date:	October 9, 2015

STORMWATER MANAGEMENT STANDARD 4 - WATER QUALITY VOLUME

	DEPTH TO TREAT (IN.)	IMPERVIOUS AREA (SF)	WATER VOLUME (CF)
WATER QUALITY VOLUME	0.5	524,473	21,853
NET WATER QUALITY VOLUME			21,853



Project Number:8548.0Project Name:Salmon HeProject Address:Village StrClient:ContinuingLocation:Medway, H

8548.0 Salmon Health ARCPUD Village Street Continuing Care Managent Medway, MA Date: Calculations by: Calculations date: Checked by: Checked Date: October 5, 2015 Jonathan E. Novak October 5, 2015 TLD October 9, 2015

CONVERSION OF WATER QUALITY VOLUME TO A DISCHARGE RATE FOR PROPRIETAY STORMWATER TREATMENT PRACTICES

Q = (qu)(A)(WQV)

Q= FLOW RATE qu = UNIT PEAK DISCHARGE (csm/in) A = IMPERVIOUS SURFACE DRAINAGE AREA (sq mi) WQV = WATER QUALITY VOLUME

STC-1

Tc =	5	min
qu =	795	
A =	0.810	Acre
WQV =	1	inch
Q =	1.01	CFS

STC-2

Tc =	5	min
qu =	795	
A =	1.270	Acre
WQV =	1	inch
Q =	1.58	CFS

STC-3

Tc =	5	min
qu =	795	
A =	6.140	Acre
WQV =	1	inch
Q =	7.63	CFS

STC-4

Tc =	5	min
qu =	795	
A =	2.810	Acre
WQV =	1	inch
Q =	3.49	CFS



Project Number:8548.0Project Name:Salmon Health ARCPUDProject Address:Village StreetClient:Continuing Care ManagentLocation:Medway, MA

Date: Calculations by: Calculations date: Checked by: Checked Date:

October 13, 2015 Damien Dmitruk October 5, 2015 Jonathan E. Novak October 8, 2015

PROPOSED DRAWDOWN FOR RECHARGE STRUCTURES

BASIN 1

	A = AREA OF	PROPOSED LEA	CHING STRUCT	URE	2,970	SQ. FT.
	Rv	= REQUIRED REG	CHARGE VOLUM	4E =	16,904	CU. FT.
K= SATURA	FED HYDRAULI	C CONDUCTIVIT	ΓY (RAWLS RAT	E) =	2.41	NICHES/HOLID
	VALUE IS BAS	SED ON A HYDR.	AULIC SOIL GRO	OUP	2.41	INCILES/HOUK
T = ALLO	OWABLE DRAW	DOWN DURING	PEAK (USE 2 HR	(S) =	72	HRS
WDOWN TIME T	= Rv	=		28.3 HOUI	RS TO EMPTY THE	E RECHARGE BMP
	K x A			<72 H	IOURS, SO DRAWI	DOWN IS OK

BASIN 3

А	= AREA OF PROP	POSED LEACHING S	STRUCTURE	3,673	SQ. FT.
	$\mathbf{R}\mathbf{v} = \mathbf{R}\mathbf{E}\mathbf{Q}$	UIRED RECHARGE	VOLUME =	26,745	CU. FT.
K= SATURATED	HYDRAULIC CO	NDUCTIVITY (RAW	LS RATE) =	2.41	INCHES/HOUR
V	ALUE IS BASED O	ON A HYDRAULIC S	OIL GROUP	2	
T = ALLOWA	ABLE DRAWDOW	N DURING PEAK (U	JSE 2 HRS) =	72	HRS
WDOWN TIME T=	Rv	=	36.3 H	IOURS TO EMPTY THE	RECHARGE BMP
	K x A		<	72 HOURS, SO DRAWD	OWN IS OK



Project Number: 8548.0 Date: October 13, 2015 **Project Name:** Salmon Health ARCPUD Calculations by: Damien Dmitruk **Project Address:** Calculations date: October 5, 2015 Village Street **Client:** Continuing Care Managent Checked by: Jonathan E. Novak Location: Medway, MA **Checked Date:** October 8, 2015

PROPOSED DRAWDOWN FOR RECHARGE STRUCTURES

A = AREA OF PROPOSED LEACHING STRUCTURE	858	SQ. FT.
Rv = REQUIRED RECHARGE VOLUME =	2,026	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41	INCHES/HOUR
VALUE IS BASED ON AHYDRAULIC SOIL GROUP	2	interinder into ent
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72	HRS
WDOWN TIME T- P_V - 118 I	HOURS TO EMPTY THE REC	HARGE BMP
	Z72 HOURS SO DRAWDOW	N IS OK
	<72 HOOKS, 50 DRAWDOW	
INFILTRATION T	RENCH 9	
A = AREA OF PROPOSED LEACHING STRUCTURE	280	SO. FT.
Rv = REQUIRED RECHARGE VOLUME =	605	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	0.41	NCUER/HOUD
VALUE IS BASED ON A HYDRAULIC SOIL GROUP	2.41	INCHES/HOUR
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72	HRS
WDOWN TIME $T = Rv = 10.8$	HOURS TO EMPTY THE REC	CHARGE BMP
K x A	<72 HOURS, SO DRAWDOW	N IS OK
INITIT OD A OTANI OT	DENICII 10	
INFILIRATION II	<u>KENCH IU</u>	
	524	00 FT
$A = AREA OF PROPOSED LEACHING STRUCTURE P_{V} = PEOLUPED PECHAPCE VOLUME =$	530 1 261	SQ. FT.
K – SATURATED HYDRAUI IC CONDUCTIVITY (RAWI S RATE) –	1,201	CU. F1.
VALUE IS BASED ON A HYDRAULIC SOIL GROUP	2.41	INCHES/HOUR
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72	HRS
WDOWN TIME $T = Rv = 11.7$	HOURS TO EMPTY THE REC	CHARGE BMP
K x A	<72 HOURS, SO DRAWDOW	N IS OK
INFILTRATION T	RENCH 11	
A = AREA OF PROPOSED LEACHING STRUCTURE	1,207	SQ. FT.
Rv = REQUIRED RECHARGE VOLUME =	2,875	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41	NCHES/HOUD
VALUE REDARES ON A LIVED ARE COULD OF	2.41	INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP	2.41	INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72	HRS
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T= Rv = 11.9 I	72 HOURS TO EMPTY THE REC	HRS CHARGE BMP
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T= $\frac{Rv}{K \times A}$ = 11.9 I	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW	HRS CHARGE BMP N IS OK
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T= \underline{Rv} = 11.9 I \underline{KxA}	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW	HRS CHARGE BMP N IS OK
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = $\frac{Rv}{K \times A}$ = 11.9 I INFILTRATION TR	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW EENCH 11A	HRS CHARGE BMP N IS OK
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = $\frac{R_V}{K \times A}$ = 11.9 I <u>INFILTRATION TR</u>	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 11A	HRS HRS CHARGE BMP N IS OK
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = $\frac{R_V}{K \times A}$ = 11.9 I <u>INFILTRATION TR</u> A = AREA OF PROPOSED LEACHING STRUCTURE	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW EENCH 11A 280	HRS CHARGE BMP N IS OK SQ. FT.
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME $T = Rv = 11.9$ I $K \ge A$ $K \ge A$ K	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW EENCH 11A 280 661	HRS CHARGE BMP N IS OK SQ. FT. CU. FT.
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME $T = Rv = 11.9$ I $K \times A$ INFILTRATION TR A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW EENCH 11A 280 661 2.41	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME $T = Rv = 11.9$ I $K \ge A$ = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW SENCH 11A 280 661 2.41	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME $T = Rv = 11.9$ I $K \times A$ INFILTRATION TR A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW EENCH 11A 280 661 2.41 72	HRS HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = Rv Rv = INFILTRATION TR A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW EENCH 11A 280 661 2.41 72 HOURS TO EMPTY THE DEC	HRS HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = $\frac{Rv}{K \times A}$ = 11.9 I $\frac{INFILTRATION TR}{K \times A}$ A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = $\frac{Rv}{K \times A}$ = 11.8 I	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW EENCH 11A 280 661 2.41 72 HOURS TO EMPTY THE REC <72 HOURS SO DRAWDOW	INCHES/HOUK HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS CHARGE BMP N IS OK



Project Number: 8548.0 Date: October 13, 2015 Project Name: Salmon Health ARCPUD Calculations by: Damien Dmitruk **Project Address:** Calculations date: October 5, 2015 Village Street **Client:** Continuing Care Managent Checked by: Jonathan E. Novak Location: Medway, MA **Checked Date:** October 8, 2015

PROPOSED DRAWDOWN FOR RECHARGE STRUCTURES

A = AREA OF PROPOSED LEACHING STRUCTURE	613	SQ. FT.
KV = REQUIRED RECHARGE VOLUME = K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	1,442	CU. FI.
VALUE IS BASED ON A HYDRAULIC SOIL GROUP	2.41	INCHES/HOUR
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72	HRS
WDOWN TIME $T = Rv = 11.7 H$	HOURS TO EMPTY THE REC	CHARGE BMP
K x A	<72 HOURS, SO DRAWDOW	N IS OK
INFILTRATION TI	RENCH 13	
A = AREA OF PROPOSED LEACHING STRUCTURE	531	SQ. FT.
Rv = REQUIRED RECHARGE VOLUME =	1,247	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41	INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWARDER DRAWDOWN DURING REAK (USE 2 URS) =	70	LIDC
I = ALLOWABLE DRAWDOWN DURING FEAR (USE 2 HRS) =	12	пкэ
WDOWN TIME T= $\frac{Rv}{K \times A}$ = 11.7 H	HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW	CHARGE BMP N IS OK
ΙΝΕΠ ΤΡΑΤΙΟΝ ΤΙ	DENCH 14	
	KEIVCH 14	
A = AREA OF PROPOSED LEACHING STRUCTURE	531	SQ. FT.
Rv = REQUIRED RECHARGE VOLUME =	1,247	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41	INCHES/HOUR
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72	HRS
WDOWN TIME $T = \frac{Rv}{KxA} = 11.7 H$	HOURS TO EMPTY THE REC	CHARGE BMP
n A A		
INFILTRATION TI	RENCH 15	
A = AREA OF PROPOSED LEACHING STRUCTURE	613	SO. FT.
Rv = REQUIRED RECHARGE VOLUME =	1,442	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41	INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP	70	
I = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	12	HKS
WDOWN TIME $T = Rv = 11.7 H$	HOURS TO EMPTY THE REC	CHARGE BMP
K x A	<72 HOURS, SO DRAWDOW	N IS OK
INFILTRATION TI	RENCH 16	
A = AREA OF PROPOSED LEACHING STRUCTURE	1,840	SQ. FT.
Rv = REQUIRED RECHARGE VOLUME =	4,416	CU. FT.
VALUE IS BASED ON A HYDRAULIC SOIL GROUP	2.41	INCHES/HOUR
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72	HRS
WDOWN TIME T_ D 1101	IOUDS TO EMPTY THE PEC	
$\frac{11.9}{KxA}$	<pre><72 HOURS. SO DRAWDOW]</pre>	N IS OK



 Project Number:
 8548.0

 Project Name:
 Salmon Health ARCPUD

 Project Address:
 Village Street

 Client:
 Continuing Care Managent

 Location:
 Medway, MA

 Date:
 October 13, 2015

 Calculations by:
 Damien Dmitruk

 Calculations date:
 October 5, 2015

 Checked by:
 Jonathan E. Novak

 Checked Date:
 October 8, 2015

PROPOSED DRAWDOWN FOR RECHARGE STRUCTURES

A = AREA OF PROPOSED LEACHING STRUCTURE	1,040	SQ. FT.
Rv = REQUIRED RECHARGE VOLUME =	2,472	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41	INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP	70	UDC
I = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	12	HRS
WDOWN TIME $T = Rv = 11.8$	HOURS TO EMPTY THE REC	CHARGE BMP
K x A	<72 HOURS, SO DRAWDOW	N IS OK
INFILTRATION T	RENCH 18	
A = AREA OF PROPOSED LEACHING STRUCTURE	1,910	SQ. FT.
Rv = REQUIRED RECHARGE VOLUME =	5,052	CU. FT.
K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP	2.41	INCHES/HOUR
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72	HRS
(*********************************		
WDOWN TIME $T = Rv = 13.2$	HOURS TO EMPTY THE REC	CHARGE BMP
K x A	<72 HOURS, SO DRAWDOW	N IS OK
	ENGLI 10 A	
INFILTRATION TR	<u>ENCH 18A</u>	
	9 619	SO ET
$R_{v} = REOURED RECHARGE VOLUME =$	32.018	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41	DICHERMICHE
	/41	INCHEN/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP	2.71	interills/nook
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72	HRS
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72	HRS
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = $\frac{R_V}{K \times A}$ = 18.4 1	72 HOURS TO EMPTY THE REC	HRS CHARGE BMP
VALUE IS BASED ON A HYDRAULIC SOIL GROUPT = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =WDOWN TIMET=Rv=K x A-	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW	HRS CHARGE BMP N IS OK
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T= Rv = 18.4 $K \times A$ INFILTRATION T	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19	HRS CHARGE BMP N IS OK
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T= $K \times A$ INFILTRATION T	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19	HRS CHARGE BMP N IS OK
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = R_V = 18.4 	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964	HRS CHARGE BMP N IS OK SQ. FT.
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T= \mathbf{Rv} = INFILTRATION T A = AREA OF PROPOSED LEACHING STRUCTURE \mathbf{Rv} = REQUIRED RECHARGE VOLUME =	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717	HRS CHARGE BMP N IS OK SQ. FT. CU. FT.
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME $T = \underline{Rv} = 18.4$ $\underline{K \times A}$ INFILTRATION T A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME $T = \underline{Rv} = 18.4$ $\overline{K \times A}$ INFILTRATION T A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = AULOWAPL E DRAWDOWN DURING REAK (USE 2 HPS) =	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = WDOWN TIME $T = \underline{Rv} = 18.4$ $\overline{K \times A}$ INFILTRATION T A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = WDOWN TIME $T = Rv = 18.4$ $K \times A$ INFILTRATION T A = AREA OF PROPOSED LEACHING STRUCTURE $Rv = REQUIRED RECHARGE VOLUME =K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =VALUE IS BASED ON A HYDRAULIC SOIL GROUPT = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =WDOWN TIME T = Rv = 12.0$	72 HOURS TO EMPTY THE REC 72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72 HOURS TO EMPTY THE REC	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS CHARGE BMP
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T= Rv = INFILTRATION A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T= Rv = .WDOWN TIME T=	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS CHARGE BMP N IS OK
VALUE IS BASED ON A HYDRAULIC SOIL GROUPT = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =.WDOWN TIMET = Rv = 18.4.WDOWN TIMET = Rv = 18.4	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS CHARGE BMP N IS OK
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = Rv = 18.4 MDOWN TIME T = Rv = 18.4 A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 20	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS CHARGE BMP N IS OK
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T= Rv = INFILTRATION A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T= Rv = INFILTRATION TI	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 20	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS CHARGE BMP N IS OK
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = Rv = A = Rv The second	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 20 3,993 9.653	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS CHARGE BMP N IS OK SQ. FT. CU. FT.
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = Rv $K \ge A$ INFILTRATION TI A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = .WDOWN TIME T = Rv Rv = INFILTRATION TI A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = A = AREA OF PROPOSED LEACHING STRUCTURE A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 20 3,993 9,653	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS CHARGE BMP N IS OK SQ. FT. CU. FT.
VALUE IS BASED ON A HYDRAULIC SOIL GROUPT = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =WDOWN TIME T = \underline{Rv} = 18.4K x AINFILTRATION TIA = AREA OF PROPOSED LEACHING STRUCTURERv = REQUIRED RECHARGE VOLUME =K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =VALUE IS BASED ON A HYDRAULIC SOIL GROUPT = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =WDOWN TIME T = \underline{Rv} = 12.0MUDOWN TIME T = \underline{Rv} = 12.0K x AA = AREA OF PROPOSED LEACHING STRUCTURERv = REQUIRED RECHARGE VOLUME =K x AK x AUNDOWN TIME T = \underline{Rv} = 12.0K x ALINFILTRATION TIA = AREA OF PROPOSED LEACHING STRUCTURERv = REQUIRED RECHARGE VOLUME =K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =VALUE IS BASED ON A HYDRAULIC SOIL GROUP	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 20 3,993 9,653 2.41	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUPT = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =WDOWN TIME T = Rv = 18.4K x AINFILTRATION TA = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME =K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =WDOWN TIME T = Rv = 12.0K x AINFILTRATION TA = AREA OF PROPOSED LEACHING STRUCTURE RV = REQUIRED RECHARGE VOLUME =K x AINFILTRATION TA = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME =K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 20 3,993 9,653 2.41 72	HRS HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS SQ. FT. CU. FT. INCHES/HOUR HRS
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = WDOWN TIME T = Rv = 18.4 K x A INFILTRATION T A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) = WDOWN TIME T = Rv = 12.0 K x A INFILTRATION T A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K x A INFILTRATION T A = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 20 3,993 9,653 2.41 72	HRS HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS SQ. FT. CU. FT. INCHES/HOUR HRS
VALUE IS BASED ON A HYDRAULIC SOIL GROUPT = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =WDOWN TIMET = Rv =Rv=INFILTRATION TIA = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME =K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =WDOWN TIMET = Rv =Rv = REQUIRED RECHING STRUCTURE Rv = REQUIRED REAK (USE 2 HRS) =WDOWN TIMET = Rv =Rv = REQUIRED REAK (USE 2 HRS) =WDOWN TIME T = Rv =L = Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =WDOWN TIME T = Rv =L = AREA OF PROPOSED LEACHING STRUCTURE Rv = REQUIRED RECHARGE VOLUME = K = SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) = VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS) =WDOWN TIMET = Rv =L = Rv =12.0	72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 19 1,964 4,717 2.41 72 HOURS TO EMPTY THE REC <72 HOURS, SO DRAWDOW RENCH 20 3,993 9,653 2.41 72 HOURS TO EMPTY THE REC (72 HOURS TO EMPTY THE REC	HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS CHARGE BMP N IS OK SQ. FT. CU. FT. INCHES/HOUR HRS CHARGE BMP N IS OK



Project Number: 8548.0 **Project Name:** Salmon Health ARCPUD Project Address: Village Street **Client:** Continuing Care Managent Location: Medway, MA

Date: October 13, 2015 Calculations by: Calculations date: Checked by: **Checked Date:**

Damien Dmitruk October 5, 2015 Jonathan E. Novak October 8, 2015

PROPOSED DRAWDOWN FOR RECHARGE STRUCTURES

A = AREA OF PROPOSED LEACHING STRUCTU	RE	1,065	SQ. FT.												
Rv = REQUIRED RECHARGE VOLUM	E = 2	2,538	CU. FT.												
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41	INCHES/HOUR												
VALUE IS BASED ON A HYDRAULIC SOIL GRO T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HR)	UP S) =	72	HRS												
	<i>y</i>) –	12	IIKS												
WDOWN TIME T= Rv = 1	1.9 HOURS TO	EMPTY THE REC	CHARGE BMP												
K x A	<72 HOURS	SO DRAWDOW	N IS OK												
<u>INFILTRATION</u>	TRENCH 22														
$\Delta = \Delta RE \Delta OE PROPOSED I E A CHING STRUCTU$	RE	860	SO FT												
$R_{v} = REQUIRED RECHARGE VOLUMI$	RE 3 =	2 043	CU FT												
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2,015													
VALUE IS BASED ON A HYDRAULIC SOIL GRO	UP	2.41	INCHES/HOUR												
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HR	5) =	72	HRS												
WDOWN TIME $T = \frac{Rv}{V} = 1$	L8 HOURS TO	EMPTY THE REC	HARGE BMP												
K X A	2 HOURS</td <td>SODRAWDOW</td> <td>N IS OK</td>	SODRAWDOW	N IS OK												
INFILTRATION	TRENCH 22	4													
	A = AREA OF PROPOSED LEACHING STRUCTURE 288 SQ. FT. Rv = REQUIRED RECHARGE VOLUME = 603 CU. FT. STURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =														
A = AREA OF PROPOSED LEACHING STRUCTU	RE	288	SO. FT.												
Rv = REQUIRED RECHARGE VOLUM	Ξ =	603	CU. FT.												
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41	INCUES/HOUD												
VALUE IS BASED ON A HYDRAULIC SOIL GRO	UP	2.41	INCHES/HOUK												
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS	5) =	72	HRS												
$\frac{1}{K_{XA}} = 1$	72 HOURS TO		N IS OK												
	<72 HOOKS	SO DRAWDOW	NIS OK												
INFILTRATION	TRENCH 23	<u>}</u>													
A = AREA OF PROPOSED LEACHING STRUCTU	RE :	3,550	SQ. FT.												
KV = REQUIRED RECHARGE VOLUM K- SATURATED HVDRAUU IC CONDUCTIVITY (RAWI S RATE	5 = 5) -	3,567	CU. FI.												
VALUE IS BASED ON A HYDRAULIC SOIL GRO) – []P	2.41	INCHES/HOUR												
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS	5) =	72	HRS												
WDOWN TIME $T = Rv = 12$	2.0 HOURS TO	EMPTY THE REC	CHARGE BMP												
K x A	<72 HOURS	SO DRAWDOW	N IS OK												
ΙΝΕΠ ΤΡΑΤΙΟΝ	TRENCH 24	1													
	I KENCII 24	<u>.</u>													
A = AREA OF PROPOSED LEACHING STRUCTU	RE	352	SQ. FT.												
Rv = REQUIRED RECHARGE VOLUM	Ξ =	762	CU. FT.												
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2 41	INCHES/HOUR												
VALUE IS BASED ON A HYDRAULIC SOIL GRO	UP	2.11	LI CHLO/HOUK												
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS	5) =	72	HRS												
WDOWNTIME T- Py - 10	B HOURS TO	εмрту тне dec	HARGE BMD												
K x A	/		N 1.3 V/N												



Project Number:8548.0Date:Project Name:Salmon Health ARCPUDCalculations by:Project Address:Village StreetCalculations date:Client:Continuing Care ManagentChecked by:Location:Medway, MAChecked Date:

PROPOSED DRAWDOWN FOR RECHARGE STRUCTURES

October 13, 2015

Damien Dmitruk

October 5, 2015

October 8, 2015

Jonathan E. Novak

A = AREA OF PROPOSED LEACHING STRUCTURE	E 531	SQ. FT.
RV = REQUIRED RECHARGE VOLUME =	= 1,247	CU. FT.
VALUE IS BASED ON A HYDRAULIC SOIL GROUP	2.41	INCHES/HOUR
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS)	= 72	HRS
WDOWN TIME T= Rv = 11.7	HOURS TO EMPTY THE RE	CHARGE BMP
K x A	<72 HOURS, SO DRAWDOW	WN IS OK
INFILTRATION 7	<u> [RENCH 26</u>	
A = AREA OF PROPOSED LEACHING STRUCTURE	E 774	SQ. FT.
Rv = REQUIRED RECHARGE VOLUME =	= 1,834	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	- 241	INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP	2.41	interies/nook
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS)	= 72	HRS
WDOWN TIME $T = \frac{Rv}{K x A} = 11.8$	HOURS TO EMPTY THE RE <72 HOURS, SO DRAWDOW	ECHARGE BMP VN IS OK
INFILTRATION 7	TRENCH 29	
A = AREA OF PROPOSED LEACHING STRUCTURE	E 1,131	SQ. FT.
RV = REQUIRED RECHARGE VOLUME =	= 2,693	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41	INCHES/HOUR
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS)	= 72	HRS
$\frac{11.9}{K \times A}$	<pre><72 HOURS, SO DRAWDOW</pre>	WN IS OK
INFILTRATION 7	FRENCH 30	
A = AREA OF PROPOSED LEACHING STRUCTURE	E 655	SQ. FT.
Rv = REQUIRED RECHARGE VOLUME =	= 1,548	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	2.41	INCHES/HOUR
VALUE IS BASED ON A HYDRAULIC SOIL GROUP T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS)	= 72	HRS
	- 12	IIII
WDOWN TIME $T = Rv = 11.8$	HOURS TO EMPTY THE RE	ECHARGE BMP
K x A	<72 HOURS, SO DRAWDOW	WN IS OK
INFILTRATION 1	TRENCH 31	
A = AREA OF PROPOSED LEACHING STRUCTURF	E 1,131	SQ. FT.
Rv = REQUIRED RECHARGE VOLUME =	= 2,693	CU. FT.
K= SATURATED HYDRAULIC CONDUCTIVITY (RAWLS RATE) =	- 2.41	INCHES/HOUP
VALUE IS BASED ON A HYDRAULIC SOIL GROUP	2.41	INCITES/HOUK
T = ALLOWABLE DRAWDOWN DURING PEAK (USE 2 HRS)	= 72	HRS
WDOWN TIME T= Rv - 110	ΗΟURS ΤΟ ΕΜΡΤΥ ΤΗΕ ΡΕ	CHARGE RMP
	<72 HOURS, SO DRAWDOW	WN IS OK



		WAT	ERSHED CH	ARACTI	ERISTICS										PIPE CH	ARACTERIS	STICS					FL(OW CHARA	CTERISTIC	cs
	LOCATION		-	AND U	SE	FLC	OW TIME		FL	ow					R = hy	draulic radi	us = area/v	vetted perim	eter						Тс
Description	ion Cover Increm. 1 (ACRE) (A		A C	CA	Total CA	To Inlet	In Pipe	Тс	1	Q	Structure	Invert	Pipe	Size	Length	Area	R	Slope	n	Qf	Vf	Q/Qf	V/Vf	V	L/V
		(ACRE) (ACRE)			(MIN)	(MIN)	(MIN)	(IPH)	(CFS)				(IN)	(FT)	(SF)	(FT)			(CFS)	(FT/S)			(FT/S)	(MIN)
WS CB-1	LANDSCAPED	0.096	0.400							Fr	om: CB-1	Out:													
	IMPERVIOUS	0.123 0.2	0.850 19 0.653	0.143		5.00	NONE	5.00	6.57	0.94 To	o: DMH-1	In:	HDPE	12	20	0.79	0.250	0.005	0.013	2.52	3.21	0.37	0.79	2.52	0.13
WS CB-2	LANDSCAPED	0.100	0.400							Fr	om: CB-2	Out:													
	IMPERVIOUS	0.065 0.1	0.850 65 0.577	0.095		5.00	NONE	5.00	6.57	0.63 To	: DMH-1	In:	HDPE	12	23	0.79	0.250	0.005	0.013	2.52	3.21	0.25	0.70	2.24	0.17
DMH-1	TO DMH-3				0.238	5.00	0.17	5.17	6.54	1.56 Fr	om: DMH-1	Out:													
										Тс	b: DMH-3	In:	HDPE	12	93	0.79	0.250	0.002	0.013	1.59	2.03	0.98	1.04	2.11	0.73
WS CB-3	LANDSCAPED	0.037	0.400							Fr	om: CB-3	Out:													
	IMPERVIOUS	0.078	0.850	0 081		5.00	NONE	5.00	6 57	0 53 Tc). DMH-2	In:	HDPE	12	21	0.79	0.250	0.010	0.013	3.56	4.54	0.15	0.60	2.74	0.13
DMH-2	TO DMH-3	0.1	10 0.100	0.001	0 081	5.00	0.13	5.00	6 55	0.53 Fr	rom: DMH-2	Out [.]													
Dimit-2					0.001	0.00	0.15	0.10	0.00	0.0011		la:	HDPE	12	43	0.79	0.250	0.001	0.013	1.13	1.43	0.47	0.84	1.21	0.59
											DIVIEN-3	In:													
WS CB-4		0.005	0.400							Fr	om: CB-4	Out:		40	05	0.70	0.050	0.040	0.040			0.04	0.00	0.00	0.44
	IMPERVIOUS	0.129	0.850 34 0.833	0.112		5.00	NONE	5.00	6.57	0.73 To	: DMH-4	In:	HDPE	12	25	0.79	0.250	0.010	0.013	3.96	4.54	0.21	0.66	3.00	0.14
WS CB-5	LANDSCAPED	0.011	0.400							Fr	om: CB-5	Out:		10	05	0.70	0.050								
	IMPERVIOUS	0.074	0.850 0.792	0.067		5.00	NONE	5.00	6.57	0.44 To	: DMH-4	In:	HDPE	12	25	0.79	0.250	0.010	0.013	3.56	4.54	0.12	0.57	2.59	0.16
DMH-4	TO DMH3				0.179	5.00	0.16	5.16	6.54	1.17 Fr	om: DMH-4	Out:													
										To	DMH3	ln:	HDPE	18	4	1.77	0.375	0.001	0.013	3.32	1.88	0.35	0.77	1.45	0.05
DMH-3	TO STC-1				0.498	5.17	0.73	5.91	6.41	3.19 Fr	om: DMH-3	Out:													
	TO STC-1 0.498 5									Тс	o: STC-1	In:	HDPE	18	81	1.77	0.375	0.001	0.013	3.32	1.88	0.96	1.03	1.95	0.69



		WATE	RSHED CH	ARACTE	ERISTICS										PIPE CH	ARACTERIS	STICS					FL(OW CHARA	CTERISTIC	S
	LOCATION		1	LAND US	SE	FL	OW TIME		F!	LOW					R = hy	draulic radi	us = area/	wetted perin	neter		/ /				Тс
Description	Cover	Increm. Total_/ (ACRE) (ACRE	A C	CA	Total CA	To Inlet (MIN)	In Pipe (MIN)	Tc (MIN	I) (IPH	Q (CFS)	Structure	Invert	Pipe	Size (IN)	Length (FT)	Area (SF)	R (FT)	Slope	n	Qf (CFS)	Vf (FT/S)	Q/Qf	V/Vf	V (FT/S)	L/V (MIN)
WS CB-8	LANDSCAPED IMPERVIOUS	0.086 0.110 0.1	0.400 0.850 96 0.653	0.128	}	5.00	NONI	E 5.C	0 6.5	7 0.84	From: CB-8 To: DMH-11	Out: In:	HDPE	12	16	0.79	0.250	0.020	0.013	5.04	6.42	0.17	0.62	4.00	0.07
WS CB-9	LANDSCAPED IMPERVIOUS	0.069 0.153 0.2	0.400 0.850 22 0.710	0.158	3	5.00	NONI	E 5.C	0 6.5	7 1.04	From: CB-9 To: DMH-11	Out: In:	HDPE	12	19	0.79	0.250	0.020	0.013	5.04	6.42	0.21	0.66	4.25	0.07
DMH-11	TO DMH-10				0.286	5.00	0.07	7 5.0)7 6.56	6 1.87	['] From: DMH-11 To: DMH-10	Out: In:	HDPE	12	90	0.79	0.250	0.005	0.013	2.52	3.21	0.74	0.96	3.08	0.49
DMH-10	то DMH-9				0.286	5.07	0.4	9 5.5	56 6.4 [°]	7 1.85	From: DMH-10 To: DMH-9	Out: In:	HDPE	12	129	0.79	0.250	0.005	0.013	2.52	3.21	0.73	0.96	3.07	0.70
DMH-9	TO DMH-8				0.286	5.56	0.70	0 6.2	26 6.34	4 1.81	From: DMH-9 To: DMH-8	Out: In:	HDPE	12	78	0.79	0.25	0.005	0.013	2.52	3.21	0.72	0.95	3.05	0.43
DMH-8	TO DMH-5				0.286	6.26	0.43	3 6.6	39 6.2	7 1.79) From: DMH-8 To: DMH-5	Out: In:	HDPE	12	97	0.79	0.25	0.005	0.013	2.52	3.21	0.71	0.95	3.04	0.53



		WATE						PIPE CH	ARACTERI	STICS					FLO	OW CHARA	CTERISTIC	S							
	LOCATION				SE	FL	OW TIME		FL	.ow					R = hy	draulic radi	ius = area/	wetted perin	neter						Тс
Description	Cover	Increm. Total_/	A C	CA	Total CA	To Inlet	In Pipe	Tc	I	Q	Structure	Invert	Pipe	Size	Length	Area	R	Slope	n	Qf	Vf	Q/Qf	V/Vf	v	L/V
		(ACRE) (ACRE				(MIN)	(MIN)	(MIN) (IPH)	(CFS)				(IN)	(FT)	(SF)	(FT)			(CFS)	(FT/S)			(FT/S)	(MIN)
WS CB-6	LANDSCAPED	0.117 0.224	0.400)							From: CB-6	Out:	HDPF	12	13	0.79	0.250	0.020	0.013	5.04	6.42	0.31	0.75	4.78	0.05
		0.34	41 0.696	0.237	•	5.00	NONE	5.0	0 6.57	′ 1.5 0	To: DMH-5	In:		.=		0.1.0	0.200	0.020	0.0.0			0.01	0.1.0		0100
WS CB-7		0.162	0.400)							From: CB-7	Out:	HUDE	12	6	0 79	0 250	0 020	0.013	5 04	6.42	0.47	0.84	5 30	0.02
		0.540	0.000	, 0.359)	5.00	NONE	5.0	0 6.57	2.36	To: DMH-5	In:	HDI L	12	0	0.75	0.230	0.020	0.010	5.04	0.42	0.47	0.04	0.00	0.02
DMH-5	TO DMH-6				0.882	6.69	0.53	3 7.2	2 6.18	5.45	From: DMH-5	Out:	норе	18	66	1 77	0 375	0.005	0.013	7 /3	4 20	0 73	0.06	1 02	0 27
											To: DMH-6	In:	TIDE	10	00	1.77	0.375	0.003	0.013	7.45	4.20	0.75	0.90	4.02	0.27
DMH-6	TO DMH-7				0.882	7.22	0.27	7.4	9 6.13	3 5.41	From: DMH-6	Out:													
											To: DMH-7	In:	HDPE	18	27	1.77	0.375	0.005	0.013	7.43	4.20	0.73	0.95	4.01	0.11
DMH-7	TO STC-2				0.882	7 49	0.11	76	0 6 1 2	> 5 30	From: DMH-7	Out:													
Dimit 1	10 0102				0.002	1.40	0.1	1.0	0 0.12	. 0.00		le:	HDPE	18	42	1.77	0.375	0.005	0.013	7.43	4.20	0.73	0.95	4.01	0.17
											10. 310-2														
STC-2	TO FES-1				0.882	7.60	0.17	7.7	8 6.09	5.37	From: STC-2	Out:	עססק	10	47	1 77	0.975	0.005	0.012	7 40	4.00	0.70	0.05	4.04	0.07
											To: FES-1	In:	NUFE	18	17	1.77	0.375	0.005	0.013	7.43	4.20	0.72	0.95	4.01	0.07



									PIPE CH	ARACTERI	STICS					FL	OW CHARA	CTERISTIC	s								
	LOCATION	LOCATION LAND USE FLOW TIME															R = hyd	draulic rad	ius = area/\	vetted perim	neter						Тс
Description	Cover	Increm. (ACRE)	Total_A (ACRE)	С	CA	Total CA	To Inlet (MIN)	In Pipe (MIN)	To (MI	c I N) (IPH)	Q (CFS)		Structure	Invert	Pipe	Size (IN)	Length (FT)	Area (SF)	R (FT)	Slope	n	Qf (CFS)	Vf (FT/S)	Q/Qf	V/Vf	V (FT/S)	L/V (MIN)
WS CB-34	LANDSCAPED IMPERVIOUS	0.023 0.048	0.07	0.400 0.850 1 0.704) 0.050		5.00	NONE	E 5.	.00 6.57	7 0.33	Fror	m: CB-34 DMH-36	Out: In:	HDPE	12	15	0.79	0.250	0.020	0.013	5.04	6.42	0.07	0.47	3.04	0.08
WS CB-35	LANDSCAPED IMPERVIOUS	0.026 0.047	0.07	0.400 0.850 3 0.690))) 0.050		5.00	NONE	E 5.	.00 6.57	7 0.33	Fror To:	m: CB-35 DMH-36	Out: In:	HDPE	12	9	0.79	0.250	0.020	0.013	5.04	6.42	0.07	0.48	3.05	0.05
DMH-36	TO DMH-35					0.100	5.00	0.08	85.	.08 6.56	6 0.66	Fror To:	m: DMH-36 DMH-35	Out: In:	HDPE	12	84	0.79	0.250	0.005	0.013	2.52	3.21	0.26	0.71	2.28	0.62
WS CB-36	LANDSCAPED IMPERVIOUS	0.021 0.054	0.07	0.400 0.850 5 0.724)) - 0.054		5.00	NONE	E 5.	.00 6.57	7 0.36	Fror To:	m: CB-36 DMH-35	Out: In:	HDPE	12	15	0.79	0.250	0.020	0.013	5.04	6.42	0.07	0.49	3.12	0.08
WS CB-37	LANDSCAPED IMPERVIOUS	0.056 0.106	0.16	0.400 0.850 2 0.694) 0.113		5.00	NONE	E 5.	.00 6.57	7 0.74	Fror To:	m: CB-37 DMH-35	Out: In:	HDPE	12	9	0.79	0.250	0.020	0.013	5.04	6.42	0.15	0.60	3.85	0.04
DMH-35	TO DMH-34					0.267	5.08	0.62	25.	.70 6.44	1.72	Fror To:	m: DMH-35 DMH-34	Out: In:	HDPE	12	19	0.79	0.250	0.005	0.013	2.52	3.21	0.68	0.94	3.01	0.11
WS CB-33	LANDSCAPED IMPERVIOUS	0.014 0.021	0.03	0.400 0.850 5 0.670)) 0.023		5.00	NONE	E 5.	.00 6.57	⁷ 0.15	Fror To:	m: CB-33 DMH-34	Out: In:	HDPE	12	14	0.79	0.250	0.020	0.013	5.04	6.42	0.03	0.38	2.44	0.10
DMH-34	TO DMH-33					0.391	5.70	0.1	1 5.	.80 6.42	2 2.51	Fror To:	m: DMH-34 DMH-33	Out: In:	HDPE	12	101	0.79	0.250	0.005	0.013	2.52	3.21	1.00	1.05	3.36	0.50
WS CB-40	LANDSCAPED IMPERVIOUS	0.110 0.188	0.29	0.400 0.850 3 0.684) 0 0.204		5.00	NONE	E 5.	.00 6.57	7 1.34	Fror	m: CB-40 DMH-40	Out: In:	HDPE	12	24	0.79	0.250	0.020	0.013	5.04	6.42	0.27	0.71	4.57	0.09
WS CB-41	LANDSCAPED IMPERVIOUS	0.163 0.096	0.25	0.400 0.850 9 0.567)) 0.147		5.00	NONE	E 5.	.00 6.57	7 0.96	Fror To:	m: CB-41 DMH-40	Out: In:	HDPE	12	20	0.79	0.250	0.020	0.013	5.04	6.42	0.19	0.65	4.16	0.08
DMH-40	TO DMH-39					0.351	5.00	0.09	95.	.09 6.56	6 2.30	Fror To:	m: DMH-40 DMH-39	Out: In:	HDPE	12	100	0.79	0.250	0.005	0.013	2.52	3.21	0.91	1.02	3.27	0.51
DMH-39	TO DMH-38					0.351	5.09	0.5	1 5.	.60 6.46	6 2.27	' Fror To:	m: DMH-39 DMH-38	Out: In:	HDPE	12	82	0.79	0.250	0.005	0.013	2.52	3.21	0.90	1.02	3.26	0.42



			WATER	SHED CH	ARACTE	RISTICS										PIPE CH/	ARACTERIS	STICS					FLO	OW CHARA	CTERISTIC	s
	LOCATION			I		SE	FL	OW TIME		FL	_OW					R = hyd	draulic radi	us = area/\	wetted perim	neter						Тс
Description	Cover	Increm. (ACRE)	Total_A (ACRE)	С	CA	Total CA	To Inlet (MIN)	In Pipe (MIN)	Tc (MIN	l) (IPH)	Q (CFS)	Structu	re Invert	Pipe	Size (IN)	Length (FT)	Area (SF)	R (FT)	Slope	n	Qf (CFS)	Vf (FT/S)	Q/Qf	V/Vf	V (FT/S)	L/V (MIN)
WS CB-38	LANDSCAPED IMPERVIOUS	0.031 0.108	3 0.139	0.400 0.850 0.750	0.104		5.00	NONE	E 5.0	00 6.57	7 0.68	From: CB-38 To: DMH-3	Out: 38 In:	HDPE	12	18	0.79	0.250	0.020	0.013	5.04	6.42	0.14	0.59	3.77	0.08
WS CB-39	LANDSCAPED IMPERVIOUS	0.153 0.223	3 3 0.376	0.400 0.850 0.667	0.251		5.00	NONE	E 5.0	0 6.57	7 1.65	From: CB-39	Out: 38 In:	HDPE	12	14	0.79	0.250	0.020	0.013	5.04	6.42	0.33	0.76	4.86	0.05
DMH-38	TO DMH-37					0.706	5.60	0.42	2 6.0	02 6.39	9 4.51	From: DMH-3 To: DMH-3	38 Out: 37 In:	HDPE	18	85	1.77	0.375	0.005	0.013	7.43	4.20	0.61	0.91	3.81	0.37
DMH-37	TO DMH-33					0.706	6.02	0.37	7 6.3	39 6.32	2 4.46	From: DMH-: To: DMH-:	37 Out: 33 In:	HDPE	18	57	1.77	0.375	0.005	0.013	7.43	4.20	0.60	0.90	3.80	0.25
DMH-33	TO DMH-32					1.097	6.39	0.50	0 6.8	39 6.23	3 6.84	From: DMH-	33 Out: 32 In:	HDPE	18	53	1.77	0.375	0.005	0.013	7.43	4.20	0.92	1.02	4.30	0.21
DMH-32	TO DMH-31					1.097	6.89	0.21	1 7.1	10 6.20	6.80	From: DMH-: To: DMH-:	32 Out: 31 In:	HDPE	18	94	1.77	0.375	0.005	0.013	7.43	4.20	0.92	1.02	4.29	0.37
WS CB-31	LANDSCAPED IMPERVIOUS	0.059 0.057	0.116	0.400 0.850 0.621	0.072		5.00	NONE	E 5.0	0 6.57	7 0.47	From: CB-31 To: DMH-3	Out: 31 In:	HDPE	12	34	0.79	0.250	0.020	0.013	5.04	6.42	0.09	0.53	3.38	0.17
WS CB-32	LANDSCAPED IMPERVIOUS	0.106 0.121	6 0.227	0.400 0.850 0.640	0.145		5.00	NONE	E 5.0	0 6.57	7 0.95	From: CB-32	Out: 31 In:	HDPE	12	26	0.79	0.250	0.020	0.013	5.04	6.42	0.19	0.65	4.15	0.10
DMH-31	TO DMH-30					1.314	7.10	0.37	7 7.4	16 6.14	4 8.07	From: DMH-3	31 Out: 30 In:	HDPE	24	83	3.14	0.500	0.005	0.013	16.00	5.09	0.50	0.86	4.37	0.32
WS CB-29	LANDSCAPED IMPERVIOUS	0.086 0.152	0.238	0.400 0.850 0.687	0.164		5.00	NONE	E 5.0	00 6.57	7 1.08	From: CB-29	Out: 30 In:	HDPE	12	10	0.79	0.250	0.020	0.013	5.04	6.42	0.21	0.67	4.29	0.04
WS CB-30	LANDSCAPED IMPERVIOUS	0.017 0.113	, 3 0.130	0.400 0.850 0.791	0.103		5.00	NONE	E 5.0	0 6.57	7 0.68	From: CB-30	Out: 30 In:	HDPE	12	25	0.79	0.250	0.020	0.013	5.04	6.42	0.13	0.58	3.75	0.11
DMH-30	TO DMH-29					1.580	7.46	0.32	2 7.7	78 6.09	9.62	From: DMH-	30 Out: 29 In:	HDPE	24	119	3.14	0.500	0.005	0.013	16.00	5.09	0.60	0.90	4.60	0.43
DMH-29	TO DMH-28					1.580	7.78	0.43	3 8.2	21 6.02	2 9.51	From: DMH-2 To: DMH-2	29 Out: 28 In:	HDPE	24	74	3.14	0.500	0.005	0.013	16.00	5.09	0.59	0.90	4.59	0.27



			WATERS	HED CH/	ARACTE	RISTICS											PIPE CH/	ARACTERIS	STICS					FL	OW CHARA	CTERISTIC	;s
	LOCATION			L	AND US	E	FL	OW TIME		F	LOW						R = hyc	draulic radi	us = area/\	vetted perin	neter						Тс
Description	Cover	Increm. T (ACRE) (/	otal_A ACRE)	С	CA	Total CA	To Inlet (MIN)	In Pipe (MIN)	Tc (MIN)	I) (IPH	Q 1) (CFS))	Structure	Invert	Pipe	Size (IN)	Length (FT)	Area (SF)	R (FT)	Slope	n	Qf (CFS)	Vf (FT/S)	Q/Qf	V/Vf	V (FT/S)	L/V (MIN)
DMH-28	TO DMH-27					1.580	8.21	0.27	7 8.48	8 5.9	98 9.4 5	5 Fror To:	m: DMH-28 DMH-27	Out: In:	HDPE	24	58	3.14	0.500	0.005	0.013	16.00	5.09	0.59	0.90	4.58	0.21
WS CB-27	LANDSCAPED IMPERVIOUS	0.222 0.101	0.323	0.400 0.850 0.541	0.175		5.00	NONE	E 5.00	0 6.5	57 1.15	Fror 5 To:	m: CB-27 DMH-27	Out: In:	HDPE	12	14	0.79	0.250	0.020	0.013	5.04	6.42	0.23	0.68	4.37	0.05
WS CB-28	LANDSCAPED IMPERVIOUS	0.014 0.121	0.135	0.400 0.850 0.803	0.108		5.00	NONE	5.00	0 6.5	57 0.71	Fror	m: CB-28 DMH-27	Out: In:	HDPE	12	15	0.79	0.250	0.020	0.013	5.04	6.42	0.14	0.59	3.81	0.07
DMH-27	TO DMH-26					1.863	8.48	0.07	7 8.54	4 5.9	97 11.12	2 Fror To:	m: DMH-27 DMH-26	Out: In:	HDPE	24	95	3.14	0.500	0.005	0.013	16.00	5.09	0.70	0.94	4.80	0.33
DMH-26	TO STC-3					1.863	8.54	0.33	3 8.87	7 5.9	92 11.02	2 Fror To:	m: DMH-26 STC-3	Out: In:	HDPE	24	57	3.14	0.500	0.005	0.013	16.00	5.09	0.69	0.94	4.79	0.20
WS CB-10	LANDSCAPED IMPERVIOUS	0.150 0.175	0.325	0.400 0.850 0.642	0.209		5.00	NONE	E 5.00	0 6.5	57 1.37	Fror 7 To:	m: CB-10 DMH-12	Out: In:	HDPE	12	9	0.79	0.250	0.020	0.013	5.04	6.42	0.27	0.72	4.61	0.03
DMH-12	TO DMH-13					0.209	5.00	0.03	3 5.03	3 6.5	57 1.37	7 Fror To:	m: DMH-12 DMH-13	Out: In:	HDPE	12	194	0.79	0.250	0.005	0.013	2.52	3.21	0.54	0.88	2.81	1.15
WS CB-11	LANDSCAPED IMPERVIOUS	0.232 0.078	0.310	0.400 0.850 0.513	0.159		5.00	NONE	E 5.00	0 6.5	57 1.05	Fror 5 To:	m: CB-11 DMH-13	Out: In:	HDPE	12	10	0.79	0.250	0.020	0.013	5.04	6.42	0.21	0.66	4.26	0.04
WS CB-12	LANDSCAPED IMPERVIOUS	0.057 0.083	0.140	0.400 0.850 0.667	0.093		5.00	NONE	5.00	0 6.5	57 0.61	Fror I To:	m: CB-12 DMH-13	Out: In:	HDPE	12	13	0.79	0.250	0.020	0.013	5.04	6.42	0.12	0.57	3.65	0.06
DMH-13	TO DMH-14					0.461	5.03	1.15	5 6.18	8 6.3	36 2.9 3	B From To:	m: DMH-13 DMH-14	Out: In:	HDPE	18	58	1.77	0.375	0.005	0.013	7.43	4.20	0.39	0.80	3.36	0.29
DMH-14	TO DMH-18					0.461	6.18	0.29	9 6.47	7 6.3	31 2.91	I Fror To:	m: DMH-14 DMH-18	Out: In:	HDPE	18	97	1.77	0.375	0.005	0.013	7.43	4.20	0.39	0.80	3.35	0.48
DMH-18	TO DMH-19					0.461	6.47	0.48	3 6.95	5 6.2	22 2.87	7 Fror To:	m: DMH-18 DMH-19	Out: In:	HDPE	18	63	1.77	0.375	0.005	0.013	7.43	4.20	0.39	0.79	3.34	0.31



Description	LOCATION																									
Description				L	AND USE	Ξ	FLC	OW TIME		FLOW						R = hyd	draulic radi	us = area/\	wetted perim	neter						Тс
	Cover	Increm. (ACRE)	Total_A (ACRE)	С	CA	Total CA	To Inlet (MIN)	In Pipe (MIN)	Tc (MIN) (I	I Q IPH) (CF	ຊ ≂S)	Structure	Invert	Pipe	Size (IN)	Length (FT)	Area (SF)	R (FT)	Slope	n	Qf (CFS)	Vf (FT/S)	Q/Qf	V/Vf	V (FT/S)	L/V (MIN)
WS CB-13	LANDSCAPED IMPERVIOUS	0.015 0.042	0.057	0.400 0.850 0.732	0.042		5.00	NONE	5.00	6.57 0.	Frc .27 To:	om: CB-13 : DMH-15	Out: In:	HDPE	12	12	0.79	0.250	0.020	0.013	5.04	6.42	0.05	0.45	2.89	0.07
WS CB-14	LANDSCAPED IMPERVIOUS	0.089 0.122	0.211	0.400 0.850 0.660	0.139		5.00	NONE	5.00	6.57 0.	Frc .92 To:	om: CB-14 : DMH-15	Out: In:	HDPE	12	10	0.79	0.250	0.020	0.013	5.04	6.42	0.18	0.64	4.10	0.04
DMH-15	TO DMH-16					0.181	5.00	0.31	5.31	6.51 1.	. 18 Fro	om: DMH-15 : DMH-16	Out: In:	HDPE	12	52	0.79	0.250	0.005	0.013	2.52	3.21	0.47	0.84	2.69	0.32
WS CB-15	LANDSCAPED IMPERVIOUS	0.011 0.070	0.081	0.400 0.850 0.789	0.064		5.00	NONE	5.00	6.57 0.	Frc .42 To:	om: CB-15 : DMH-16	Out: In:	HDPE	12	47	0.79	0.250	0.020	0.013	5.04	6.42	0.08	0.51	3.27	0.24
WS CB-16	LANDSCAPED IMPERVIOUS	0.023 0.166	0.189	0.400 0.850 0.795	0.150		5.00	NONE	5.00	6.57 0.	Frc . 99 To:	om: CB-16 : DMH-16	Out: In:	HDPE	12	11	0.79	0.250	0.020	0.013	5.04	6.42	0.20	0.65	4.19	0.04
DMH-16	TO DMH-17					0.395	5.31	0.32	5.64	6.45 2.	. 55 Fro	om: DMH-16 : DMH-17	Out: In:	HDPE	18	101	1.77	0.375	0.005	0.013	7.43	4.20	0.34	0.77	3.23	0.52
WS CB-17	LANDSCAPED IMPERVIOUS	0.018 0.090	0.108	0.400 0.850 0.775	0.084		5.00	NONE	5.00	6.57 0.	Frc . 55 To:	om: CB-17 : DMH-17	Out: In:	HDPE	12	45	0.79	0.250	0.020	0.013	5.04	6.42	0.11	0.55	3.53	0.21
WS CB-18	LANDSCAPED IMPERVIOUS	0.000 0.072	0.072	0.400 0.850 0.850	0.061		5.00	NONE	5.00	6.57 0.	Frc . 40 To:	om: CB-18 : DMH-17	Out: In:	HDPE	12	9	0.79	0.250	0.020	0.013	5.04	6.42	0.08	0.50	3.23	0.05
DMH-17	TO DMH-19					0.540	6.95	0.52	7.47	6.14 3.	. 32 Fro	om: DMH-17 : DMH-19	Out: In:	HDPE	18	39	1.77	0.375	0.005	0.013	7.43	4.20	0.45	0.83	3.48	0.19
DMH-19	TO DMH-21					1.001	7.47	0.31	7.79	6.09 6.	. 09 Fro	om: DMH-19 : DMH-21	Out: In:	HDPE	18	61	1.77	0.375	0.005	0.013	7.43	4.20	0.82	0.99	4.16	0.24
WS CB-19	LANDSCAPED IMPERVIOUS	0.008 0.046	0.054	0.400 0.850 0.783	0.042		5.00	NONE	5.00	6.57 0.	Frc .28 To:	om: CB-19 : DMH-20	Out: In:	HDPE	12	11	0.79	0.250	0.020	0.013	5.04	6.42	0.06	0.45	2.90	0.06
WS CB-20	LANDSCAPED IMPERVIOUS	0.020 0.089	0.109	0.400 0.850 0.767	0.084		5.00	NONE	5.00	6.57 0.	Frc . 55 To:	om: CB-20 : DMH-20	Out: In:	HDPE	12	15	0.79	0.250	0.020	0.013	5.04	6.42	0.11	0.55	3.53	0.07
DMH-20	TO DMH-21					0.126	5.00	0.07	5.07	6.56 0.	. 83 Fro	om: DMH-20 : DMH-21	Out: In:	HDPE	12	28	0.79	0.250	0.005	0.013	2.52	3.21	0.33	0.76	2.43	0.19



			WATERS	HED CHA	ARACTE	RISTICS											PIPE CH	ARACTERI	STICS					FLO	OW CHARA	CTERISTIC	:S
	LOCATION			L	AND US	E	FLO	OW TIME		FL	.ow						R = hy	draulic radi	us = area/v	vetted perim	neter						Тс
Description	Cover	Increm. T (ACRE) (A	Total_A ACRE)	С	CA	Total CA	To Inlet (MIN)	In Pipe (MIN)	Tc (MIN	l) (IPH)	Q (CFS)		Structure	Invert	Pipe	Size (IN)	Length (FT)	Area (SF)	R (FT)	Slope	n	Qf (CFS)	Vf (FT/S)	Q/Qf	V/Vf	V (FT/S)	L/V (MIN)
DMH-21	TO DMH-22					1.127	7.79	0.24	4 8.0	03 6.05	5 6.82	Pron	n: DMH-21	Out:	норе	18	100	1 77	0 375	0.005	0.013	7 /3	4 20	0.92	1 02	1 29	0 30
												To:	DMH-22	In:	TIDI L	10	100	1.77	0.373	0.000	0.013	7.45	4.20	0.52	1.02	4.25	0.55
WS CB-21		0.140		0.400								Fron	n: CB-21	Out:		10	14	0.70	0.250	0.020	0.012	5.04	6 42	0.20	0.72	4 67	0.05
		0.192	0.332	0.660	0.219		5.00	NONE	E 5.0	0 6.57	' 1.44	To:	DMH-22	ln:	TIDEL	12	14	0.79	0.230	0.020	0.013	5.04	0.42	0.29	0.75	4.07	0.03
WS CB-22	LANDSCAPED IMPERVIOUS	0.012 0.084		0.400 0.850								Fron	n: CB-22	Out:	HDPE	12	19	0.79	0.250	0.020	0.013	5.04	6.42	0.10	0.54	3.44	0.09
DMU 00			0.096	0.794	0.076	1 100	5.00	NONE	E 5.0	0 6.57	0.50	To:	DMH-22	In:													
DMH-22	TO DMH-23					1.423	8.03	0.3	9 8.4	12 5.99	8.52	To.	DMH-22	Out:	HDPE	24	67	3.14	0.500	0.005	0.013	16.00	5.09	0.53	0.87	4.44	0.25
												10.	2111120														
DMH-23	TO DMH-24					1.423	8.42	0.25	5 8.6	67 5.95	5 8.46	Fron	n: DMH-23	Out:	HDPE	24	162	3.14	0.500	0.005	0.013	16.00	5.09	0.53	0.87	4.43	0.61
												10:	DMH-24	In:													
WS CB-23	LANDSCAPED IMPERVIOUS	0.235 0.081		0.400 0.850								Fron	n: CB-23	Out:	HDPE	12	10	0.79	0.250	0.020	0.013	5.04	6.42	0.21	0.67	4.29	0.04
			0.316	0.515	0.163		5.00	NONE	E 5.0	0 6.57	7 1.07	To:	DMH-24	ln:													
WS CB-24	LANDSCAPED IMPERVIOUS	0.010 0.108	0.118	0.400	0.006		5.00	NON		0 6 57		Fron	n: CB-24	Out:	HDPE	12	28	0.79	0.250	0.020	0.013	5.04	6.42	0.12	0.57	3.67	0.13
DMH-24	TO DMH-25		0.118	0.012	0.090	1.681	8.67	0.6	⊑ 5.0 1 9.2	28 5.86	5 9.84	Fron	n: DMH-24	Out:													
												To:	DMH-25	In:	HDPE	24	141	3.14	0.500	0.005	0.013	16.00	5.09	0.62	0.91	4.63	0.51
		0.000		0.400								From	or CB 25	Out													
W3 CB-23	IMPERVIOUS	0.081	0.319	0.400 0.850 0.514	0.164		5.00	NONE	E 5.0	0 6.57	⁷ 1.08		DMH-25	In:	HDPE	12	19	0.79	0.250	0.020	0.013	5.04	6.42	0.21	0.67	4.29	0.07
WS CB-26	LANDSCAPED	0.009		0.400								Fron	n: CB-26	Out:													
	IMPERVIOUS	0.112	0.121	0.850 0.817	0.099		5.00	NONE	E 5.0	0 6.57	0.65	To:	DMH-25	In:	HDPE	12	18	0.79	0.250	0.020	0.013	5.04	6.42	0.13	0.58	3.71	0.08
DMH-25	TO STC-3					1.944	9.28	0.5	1 9.7	79 5.78	3 11.24	Fron	n: DMH-25	Out:	HDPE	24	57	3.14	0.500	0.005	0.013	16.00	5.09	0.70	0.95	4.81	0.20
												To:	STC-3	ln:			-	-								-	
STC-3	TO FES-3				_	3.808	9.79	0.20	0 9.9	99 5.75	5 21.90	Fron	n: STC-3	Out:			47	4.04	0.005	0.005	0.010	20.00	E 0.1	0.70	0.07	E 70	
												To:	FES-3	In:	NUPE	30	47	4.91	0.625	0.005	0.013	29.00	5.91	0.76	0.97	5.70	0.14



WATERSIDE RUN - 25 YEAR STORM - CLOSED SYSTEM PIPE SIZING

			WATER	SHED CH	ARACTE	RISTICS										PIPE CH	ARACTERIS	STICS					FLO	OW CHARA	CTERIS
	LOCATION			L	AND US	E	FL	OW TIME		FL	wo					R = hy	draulic radi	us = area/v	vetted perim	neter					
Description	Cover	Increm.	Total_A	С	CA	Total CA	To Inlet	In Pipe	Tc	I	Q	Structure	Invert	Pipe	Size	Length	Area	R	Slope	n	Qf	Vf	Q/Qf	V/Vf	v
		(ACRE)	(ACRE)				(MIN)	(MIN)	(MIN)) (IPH)	(CFS				(IN)	(FT)	(SF)	(FT)			(CFS)	(FT/S)			(FT/S)
WS CB-42	LANDSCAPED	0.000)	0.400								From: CB-42	Out:												
	IMPERVIOUS	0.007	7 0.007	0.850 0.850	0.006		5.00	NONE	5.00	0 6.57	7 0.04	To: DMH-41	In:	HDPE	12	10	0.79	0.250	0.020	0.013	5.04	6.42	0.01	0.26	1.6
WS CB-43	LANDSCAPED	0.006	6	0.400								From: CB-43	Out:												
	IMPERVIOUS	0.029	9 0.035	0.850	0 027		5.00	NONE	5.00	0 6 57	7 0 1	To DMH-41	In [.]	HDPE	12	13	0.79	0.250	0.020	0.013	5.04	6.42	0.04	0.40	2.
DMU 44			0.000	0.170	0.027	0.022	5.00	0.10	. 0.00	0.07	- 0.0		0.4												
Divit 1-4 1	10 Divin-42					0.055	5.00	0.10	, 3.10	5 0.50	0.2			HDPE	12	147	0.79	0.250	0.020	0.013	5.04	6.42	0.04	0.42	2.
												To: DMH-42	In:												
DMH-42	TO DMH-43					0.033	5.10	0.91	6.01	1 6.39	9 0.2 [.]	From: DMH-42	Out:												
												To: DMH-43	In:	HDPE	12	74	0.79	0.250	0.020	0.013	5.04	6.42	0.04	0.42	2.0
DMH-43	TO DMH-44					0.033	6.01	0.46	6.47	7 6.31	1 0.2	From: DMH-43	Out:	HDPE	12	57	0 79	0.25	0 020	0.013	5 04	6 42	0.04	0 42	21
												To: DMH-44	In:			0.	0110	0.20	01020	0.010	0.01	0.12	0.01	0.12	2.0
WS CB-44		0.053	2	0.400								From: CB-44	Out												
WO 00-44	IMPERVIOUS	0.083	3	0.850	0.004		5.00	NONE					out.	HDPE	12	13	0.79	0.250	0.020	0.013	5.04	6.42	0.12	0.56	3.
			0.135	0.677	0.091		5.00	NONE	5.00	J 6.5 <i>1</i>	0.6	10: DMH-44	In:												
WS CB-45	LANDSCAPED IMPERVIOUS	0.010 0.055) 5	0.400 0.850								From: CB-45	Out:	HDPE	12	17	0.79	0.250	0.020	0.013	5.04	6.42	0.07	0.48	3.0
			0.065	0.781	0.051		5.00	NONE	5.00	0 6.57	7 0.33	To: DMH-44	In:												
DMH-44	TO DMH-45					0.175	6.47	0.36	6.83	3 6.25	5 1.0 9	From: DMH-44	Out:	HDPF	12	144	0 79	0 250	0 020	0.013	5.04	6.42	0.22	0.67	4.3
												To: DMH-45	In:												
DMH-45	TO DMH-46					0 175	6.83	0.56	5 7 39	8 6 1 F	5 1 0	From: DMH-45	Out												
Dim 43						0.175	0.00	0.00	/ 1.50	5 0.10	5 1.00		lei	HDPE	12	129	0.79	0.25	0.020	0.013	5.04	6.42	0.21	0.67	4.2
												TO. DIVIH-40													
WS CB-46	LANDSCAPED	0.058	3	0.400								From: CB-46	Out:												
	IMPERVIOUS	0.175	5 0.233	0.850 0.738	0.172		5.00	NONE	5.00	0 6.57	7 1.1:	To: DMH-46	In:	HDPE	12	12	0.79	0.250	0.020	0.013	5.04	6.42	0.22	0.68	4.3
WS CB-47	LANDSCAPED	0.140)	0.400								From: CB-47	Out:												
	IMPERVIOUS	0.161	1 0.301	0.850 0.641	0.193		5.00	NONE	5.00	0 6.57	7 1.2	To: DMH-46	In:	HDPE	12	16	0.79	0.250	0.020	0.013	5.04	6.42	0.25	0.70	4.
DMH-46	TO DMH-47					0 540	7 38	0.50	780	9 6 07	7 3 2	From: DMH-46	Out												
Dim 140						0.040	7.50	0.00	/ /.00	5 0.07	5.2		Gui.	HDPE	18	145	1.77	0.375	0.005	0.013	7.43	4.20	0.44	0.83	3.4
												10: DMH-47	In:												
DMH-47	TO DMH-48					0.540	7.89	0.70	8.58	8 5.96	6 3.2	From: DMH-47	Out:												
												To: DMH-48	In:	HDPE	18	37	1.77	0.375	0.005	0.013	7.43	4.20	0.43	0.82	3.4
DMH-48	TO DMH-49					0.540	8.58	0.18	8 8.76	6 5.93	3 3.20	From: DMH-48	Out:	HDPF	18	100	1 77	0.375	0.005	0.013	7 43	4 20	0.43	0.82	3.
												To: DMH-49	In:		10	100		0.070	0.000	0.010	1.40	4.20	0.40	0.02	0
L																									

Calculations by: DJD Calculations Date: 06/10/15 Checked By: JEN Checked Date: 06/10/15

RISTIC	s T
v	L/V
T/S)	(MIN)
1.64	0.10
2.55	0.09
2.70	0.91
2.68	0.46
2.67	0.36
3.62	0.06
3.06	0.09
4.31	0.56
4.29	0.50
4.35	0.05
4.50	0.06
3.47	0.70
3.45	0.18
3.45	0.48



WATERSIDE RUN - 25 YEAR STORM - CLOSED SYSTEM PIPE SIZING

			WATER	SHED CH	ARACTE	RISTICS											PIPE CH	ARACTERIS	TICS					FLO	OW CHARA	CTERIS
	LOCATION			L	AND US	E	FL	OW TIME		F	FLOW						R = hy	draulic radi	us = area/	wetted perim	eter					
Description	Cover	Increm. (ACRE)	Total_A (ACRE)	С	CA	Total CA	To Inlet (MIN)	In Pipe (MIN)	Tc (MIN)	I (IPH	Q H) (CFS)		Structure	Invert	Pipe	Size (IN)	Length (FT)	Area (SF)	R (FT)	Slope	n	Qf (CFS)	Vf (FT/S)	Q/Qf	V/Vf	V (FT/S
WS CB-48	LANDSCAPED IMPERVIOUS	0.261 0.137	0.398	0.400 0.850 0.555	0.221		5.00	NONE	5.00	0 6.5	57 1.45	From To:	n: CB-48 DMH-49	Out: In:	HDPE	12	8	0.79	0.250	0.02	0.013	5.04	6.42	0.29	0.73	4.
WS CB-49	LANDSCAPED IMPERVIOUS	0.070 0.137	0.207	0.400 0.850 0.698	0.144		5.00	NONE	5.00	0 6.5	57 0.95	From To:	n: CB-49 DMH-49	Out: In:	HDPE	12	14	0.79	0.250	0.02	0.013	5.04	6.42	0.19	0.65	4
DMH-49	TO DMH-50					0.905	8.76	0.48	9.24	4 5.8	86 5.31	From To:	n: DMH-49 DMH-50	Out: In:	HDPE	18	30	1.77	0.375	0.005	0.013	7.43	4.20	0.71	0.95	3
DMH-50	TO DMH-51					0.905	9.24	0.13	9.37	7 5.8	84 5.29	From To:	n: DMH-50 DMH-51	Out: In:	HDPE	18	176	1.77	0.375	0.005	0.013	7.43	4.20	0.71	0.95	3
DMH-51	TO DMH-52					0.905	9.37	0.74	10.10	0 5.7	74 5.19	From To:	n: DMH-51 DMH-52	Out: In:	HDPE	18	89	1.77	0.375	0.005	0.013	7.43	4.20	0.70	0.94	3
WS CB-50	LANDSCAPED IMPERVIOUS	0.008 0.066	3 5 0.074	0.400 0.850 0.801	0.059		5.00	NONE	5.00	0 6.5	57 0.3 9	From To:	n: CB-50 DMH-52	Out: In:	HDPE	12	9	0.79	0.250	0.02	0.013	5.04	6.42	0.08	0.50	3
WS CB-51	LANDSCAPED IMPERVIOUS	0.058 0.064	3 4 0.122	0.400 0.850 0.636	0.078		5.00	NONE	5.00	0 6.5	57 0.51	From To:	n: CB-51 DMH-52	Out: In:	HDPE	12	12	0.79	0.250	0.02	0.013	5.04	6.42	0.10	0.54	3
DMH-52	TO DMH-53					1.042	10.10	0.37	10.48	3 5.6	68 5.92	Prom To:	n: DMH-52 DMH-53	Out: In:	HDPE	18	32	1.77	0.375	0.005	0.013	7.43	4.20	0.80	0.98	4
DMH-53	TO DMH-54					1.042	10.48	0.13	3 10.61	1 5.6	66 5.90) From To:	n: DMH-53 DMH-54	Out: In:	HDPE	18	114	1.77	0.375	0.005	0.013	7.43	4.20	0.79	0.98	4
WS CB-52	LANDSCAPED IMPERVIOUS	0.045 0.091	0.136	0.400 0.850 0.701	0.095		5.00	NONE	5.00	0 6.5	57 0.63	From To:	n: CB-52 DMH-54	Out: In:	HDPE	12	14	0.79	0.250	0.02	0.013	5.04	6.42	0.12	0.57	3
WS CB-53	LANDSCAPED IMPERVIOUS	0.073 0.120	3) 0.193	0.400 0.850 0.680	0.131		5.00	NONE	5.00	0 6.5	57 0.86	From To:	n: CB-53 DMH-54	Out: In:	HDPE	12	18	0.79	0.250	0.02	0.013	5.04	6.42	0.17	0.63	4
DMH-54	TO DMH-55					1.269	10.61	0.46	5 11.07	7 5.6	60 7.10	From To:	n: DMH-54 DMH-55	Out: In:	HDPE	18	66	1.77	0.375	0.005	0.013	7.43	4.20	0.96	1.03	4

Calculations by: DJD Calculations Date: 06/10/15 Checked By: JEN Checked Date: 06/10/15

RISTICS	6
V T/S)	Tc L/V (MIN)
4.68	0.03
4.14	0.06
3.99	0.13
3.99	0.74
3.97	0.37
3.20	0.05
3.46	0.06
4.12	0.13
4.12	0.46
3.67	0.06
4.03	0.07
4.34	0.25



WATERSIDE RUN - 25 YEAR STORM - CLOSED SYSTEM PIPE SIZING

			WATER	SHED CH	ARACTE	RISTICS											PIPE CI	ARACTERIS	STICS					FLC	W CHARA	CTERIS
	LOCATION			I	AND US	SE .	FL	OW TIME		F	LOW						R = h	ydraulic radi	us = area/w	etted perim	neter					
Description	Cover	Increm. (ACRE)	Total_A (ACRE)	С	CA	Total CA	To Inlet (MIN)	In Pipe (MIN)	Tc (MIN)	I) (IPH	0 I) (CF	≀ S)	Structure	Invert	Pipe	Size (IN)	Length (FT)	Area (SF)	R (FT)	Slope	n	Qf (CFS)	Vf (FT/S)	Q/Qf	V/Vf	V (FT/S)
WS CB-54	LANDSCAPED IMPERVIOUS	0.008	3) 0.028	0.400 0.850 0.721	0.020		5.00	NONE	5.00	0 6.5	57 0.	Frc	m: CB-54 DMH-56	Out: In:	HDPE	12	9	0.79	0.250	0.02	0.013	5.04	6.42	0.03	0.36	2.3
WS CB-55	LANDSCAPED IMPERVIOUS	0.006 0.005	5 0.011	0.400 0.850 0.605	0.007		5.00	NONE	5.00	0 6.5	57 0.	Frc	om: CB-55 DMH-56	Out:	HDPE	12	16	0.79	0.250	0.02	0.013	5.04	6.42	0.01	0.26	1.7
DMH-56	TO DMH-55					0.027	5.00	0.16	5.16	6 6.5	4 0 .	18 Fro	om: DMH-56 DMH-55	Out: In:	HDPE	12	25	0.79	0.250	0.005	0.013	2.52	3.21	0.07	0.48	1.
DMH-55	TO DMH-57					1.296	11.07	0.25	5 11.32	2 5.5	77.	21 Fro To:	m: DMH-55 DMH-57	Out: In:	HDPE	18	71	1.77	0.375	0.005	0.013	7.43	4.20	0.97	1.04	4.:
WS CB-56	LANDSCAPED IMPERVIOUS	0.015 0.036	5 6 0.051	0.400 0.850 0.718	0.037		5.00	NONE	5.00	0 6.5	i7 0 .	Frc . 24 To:	om: CB-56 DMH-57	Out: In:	HDPE	12	49	0.79	0.250	0.020	0.013	5.04	6.42	0.05	0.43	2.7
DMH-57	TO DMH-58					1.332	11.32	0.27	11.59	9 5.5	i3 7 .	. 37 Fro To:	m: DMH-57 DMH-58	Out: In:	HDPE	18	91	1.77	0.375	0.005	0.013	7.43	4.20	0.99	1.04	4.
WS CB-57	LANDSCAPED IMPERVIOUS	0.038 0.103	3 3 0.141	0.400 0.850 0.729	0.103		5.00	NONE	5.00	0 6.5	57 0 .	Frc . 68 To:	om: CB-57 DMH-58	Out: In:	HDPE	12	27	0.79	0.250	0.020	0.013	5.04	6.42	0.13	0.58	3.
WS CB-58	LANDSCAPED IMPERVIOUS	0.004 0.028	4 3 0.032	0.400 0.850 0.794	0.025		5.00	NONE	5.00	0 6.5	57 0 .	Frc . 17 To:	om: CB-58 DMH-58	Out: In:	HDPE	12	10	0.79	0.250	0.020	0.013	5.04	6.42	0.03	0.39	2.
DMH-58	TO DMH-59					1.460	11.59	0.35	5 11.94	4 5.4	8 8 .	. 01 Fro	m: DMH-58 DMH-59	Out: In:	HDPE	24	42	3.14	0.500	0.005	0.013	16.00	5.09	0.50	0.86	4.:
DMH-59	TO STC-4					1.460	11.94	0.16	5 12.10	0 5.4	67.	.98 Fro To:	om: DMH-59 STC-4	Out: In:	HDPE	24	113	3.14	0.5	0.005	0.013	16.00	5.09	0.50	0.86	4.3
STC-4	TO FES-5					1.460	12.10	0.43	3 12.53	3 5.4	17.	.90 Fro To:	rm: STC-4 FES-5	Out: In:	HDPE	24	32	3.14	0.5	0.005	0.013	16.00	5.09	0.49	0.85	4.:

Calculations by: DJD Calculations Date: 06/10/15 Checked By: JEN Checked Date: 06/10/15

RISTICS	;
V T/S)	Tc L/V (MIN)
2.34	0.06
1.70	0.16
1.55	0.27
4.36	0.27
2.78	0.29
4.39	0.35
3.75	0.12
2.50	0.07
4.36	0.16
4.36	0.43
4.34	0.12



WATERSIDE RUN - 25 YEAR STORM - CLOSED SYSTEM PIPE SIZING

		WA	TERSHE	D CHAR	RACTER	RISTICS										PIPE CH/	ARACTERIS	STICS					FLC	W CHARA	CTERISTIC	s
	LOCATION			LA	ND USE	E	FL	OW TIME		FLC	ow					R = hyd	draulic radi	us = area/\	wetted perim	neter						Тс
Description	Cover	Increm. Tota	I_A (C	CA	Total CA	To Inlet	In Pipe	Tc	I	q	Structure	Invert	Pipe	Size	Length	Area	R	Slope	n	Qf	Vf	Q/Qf	V/Vf	v	L/V
		(ACRE) (ACF	RE)				(MIN)	(MIN)	(MIN	I) (IPH)	(CFS)				(IN)	(FT)	(SF)	(FT)			(CFS)	(FT/S)			(FT/S)	(MIN)
WS AD1	RESIDENTIAL	1.440	0	0.200								From: AD1	Out:	PCP	12	35	0.79	0.250	0.005	0.011	2.08	3 70	0.64	0.92	3 / 8	0.17
		1	.440 0	0.200	0.288		5.00	NON	∃ 5.0	0 6.57	1.89	To: FES	In:	NOP	12	55	0.79	0.230	0.005	0.011	2.90	5.75	0.04	0.92	5.40	0.17
WS DCB1	RESIDENTIAL	7.528	0).200								From: DCB1	Out:	RCP	24	117	3 14	0 500	0.005	0.011	18 90	6.02	0.52	0.87	5 22	0 37
		7	.528 0	0.200	1.506		5.00	NON	Ξ 5.0	0 6.57	9.89	To: FES	In:	NO	27		0.14	0.000	0.000	0.011	10.50	0.02	0.52	0.07	5.22	0.07

Calculations by: DJD Calculations Date: 10/08/15 Checked By: JEN Checked Date: 10/08/15



Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
495,468	98	Impervious (I)
495,468	98	TOTAL AREA

Soil Listing (all nodes)

Area	Soil	Subcatchment
(sq-ft)	Group	Numbers
0	HSG A	
0	HSG B	
0	HSG C	
0	HSG D	
495,468	Other	I
495,468		TOTAL AREA

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Crowned Covers (all nodes)						

HSG-A (sq-ft)	HSG-B (sq-ft)	HSG-C (sq-ft)	HSG-D (sq-ft)	Other (sq-ft)	Total (sq-ft)	Ground Cover	Subcatchment Numbers
0	0	0	0	495,468	495,468	Impervious	I
0	0	0	0	495,468	495,468	TOTAL	
						AREA	

Ground Covers (all nodes)

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Time span=11.00-13.00 hrs, dt=0.05 hrs, 41 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

SubcatchmentI: Impervious	Runoff Area=495,468 sf 100.00% Impervious Runoff Depth>0.35" Tc=0.0 min CN=98 Runoff=9.17 cfs 14,568 cf
Pond T18A: TRENCH 18A	Peak Elev=171.41' Storage=11,148 cf Inflow=9.17 cfs 14,568 cf Outflow=0.48 cfs 3,406 cf
Total Runoff Area = 495,46	38 sf Runoff Volume = 14,568 cf Average Runoff Depth = 0.35

otal Runoff Area = 495,468 sf Runoff Volume = 14,568 cf Average Runoff Depth = 0.35" 0.00% Pervious = 0 sf 100.00% Impervious = 495,468 sf

Summary for Subcatchment I: Impervious

[46] Hint: Tc=0 (Instant runoff peak depends on dt)

Runoff = 9.17 cfs @ 12.00 hrs, Volume= 14,568 cf, Depth> 0.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 11.00-13.00 hrs, dt= 0.05 hrs Type III 24-hr SDS Rainfall=0.82"

	Area (sf)	CN	Description
*	495,468	98	Impervious
	495,468		100.00% Impervious Area

Subcatchment I: Impervious



Summary for Pond T18A: TRENCH 18A

[82] Warning: Early inflow requires earlier time span

Inflow Area	=	495,468 sf,	100.00% Imp	ervious,	Inflow Depth >	0.35"	for SDS	event
Inflow	=	9.17 cfs @	12.00 hrs, V	′olume=	14,568 c	f		
Outflow	=	0.48 cfs @	11.25 hrs, V	′olume=	3,406 c	f, Atten	= 95%, L	_ag= 0.0 min
Discarded	=	0.48 cfs @	11.25 hrs, V	′olume=	3,406 c	f		

Routing by Stor-Ind method, Time Span= 11.00-13.00 hrs, dt= 0.05 hrs Peak Elev= 171.41' @ 13.00 hrs Surf.Area= 8,648 sf Storage= 11,148 cf

Plug-Flow detention time= 30.2 min calculated for 3,289 cf (23% of inflow) Center-of-Mass det. time= 1.0 min (722.6 - 721.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	169.50'	11,805 cf	44.75'W x 193.25'L x 5.75'H Field A
			49,726 cf Overall - 20,213 cf Embedded = 29,513 cf x 40.0% Voids
#2A	170.25'	20,213 cf	Cultec R-900HD x 162 Inside #1
			Effective Size= 72.7"W x 48.0"H => 17.61 sf x 7.00'L = 123.3 cf
			Overall Size= 78.0"W x 48.0"H x 9.25'L with 2.25' Overlap
			Row Length Adjustment= +2.25' x 17.61 sf x 6 rows
		32,018 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	169.50'	2.410 in/hr Exfiltration over Surface area	
Discard	led OutFlow	Max=0.48 cfs	@ 11.25 hrs HW=169.57' (Free Discharge)	

1=Exfiltration (Exfiltration Controls 0.48 cfs)

Pond T18A: TRENCH 18A - Chamber Wizard Field A

Chamber Model = Cultec R-900HD

Effective Size= 72.7"W x 48.0"H => 17.61 sf x 7.00'L = 123.3 cf Overall Size= 78.0"W x 48.0"H x 9.25'L with 2.25' Overlap Row Length Adjustment= +2.25' x 17.61 sf x 6 rows

78.0" Wide + 9.0" Spacing = 87.0" C-C Row Spacing

27 Chambers/Row x 7.00' Long +2.25' Row Adjustment = 191.25' Row Length +12.0" End Stone x 2 = 193.25' Base Length 6 Rows x 78.0" Wide + 9.0" Spacing x 5 + 12.0" Side Stone x 2 = 44.75' Base Width 9.0" Base + 48.0" Chamber Height + 12.0" Cover = 5.75' Field Height

162 Chambers x 123.3 cf +2.25' Row Adjustment x 17.61 sf x 6 Rows = 20,212.9 cf Chamber Storage

49,725.6 cf Field - 20,212.9 cf Chambers = 29,512.7 cf Stone x 40.0% Voids = 11,805.1 cf Stone Storage

Chamber Storage + Stone Storage = 32,018.0 cf = 0.735 af Overall Storage Efficiency = 64.4%

162 Chambers 1,841.7 cy Field 1,093.1 cy Stone

 Image: selection of the selection



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Pond T18A: TRENCH 18A
APPENDIX D

LONG TERM POLLUTION PREVENTION PLAN – REQUIRED BY STANDARDS 4-6

LONG TERM POLLUTION PREVENTION PLAN

To keep the Stormwater Management System (SMS) functioning properly and to ensure that the stormwater Total Suspended Solids (TSS) are reduced, a long term pollution prevention is required. Continuing Care Management, LLC, the owner/operator of the facility, is responsible for the adherence to this long term plan. The following is a guideline of the specific requirements of the plan to maintain the long term viability of the stormwater management system.

The Stormwater Pollution Prevention Plan for the site addresses many of the items in the Long Term Pollution Prevention Plan.

Good Housekeeping Practices

Employees shall be instructed in the importance of not spilling fluids and chemicals such as oil, antifreeze, etc. onto the bare ground. All areas exposed to the weather shall be kept clean

Maintenance of the Grounds

Maintenance of lawns, gardens and other landscaped areas is to be performed by appropriate maintenance staff, as approved by the Owner. All materials and equipment will be stored per the above-referenced requirements. Fertilizers shall not be used within 25 feet of the wetland resource areas. Excess fertilizers shall be swept up from all impervious surfaces and not allowed to run into the drainage system.

Provisions for Storing Materials and Waste Products Inside or Under Cover

Liquid waste products shall be captured when draining from vehicles, and stored in sealed containers under cover until they are disposed of. Waste products shall be disposed of in a legal manner, at a state licensed recycling center or landfill.

Vehicle washing controls;

Vehicles shall be washed on the concrete pad which is served by the proposed trench drain and oil/grit separator. Vehicles shall not be washed if there are known contaminants being washed into the trench drain.

Requirements for routine inspections and maintenance of stormwater BMPs;

BMPs shall be inspected on a monthly basis. BMPs shall be maintained per the operations and

Spill prevention and response plans;

First responders	Phone Numbers			
Medway Fire Department	911 if emergency or 508) 533-3213			
Medway Police Department	911 if emergency or (508) 533-3212			
 Mass Department of Environmental Protection 				
Emergency Response	1-888-304-1133			

Requirements for storage and use of fertilizers, herbicides, and pesticides;

Fertilizers shall not be used within 100 feet of the wetland resource areas. Excess fertilizers shall be swept up from all impervious surfaces and not allowed to run into the drainage system.

All fertilizer, herbicides, and pesticides shall be stored at least 100 feet away from the wetland line. If stored on site, these materials should be kept in a wrapped or sealed container, and kept under cover out of the rain and snow.

Pet waste receptacles will be placed in appropriate sites throughout the development. Residents will be responsible to remove pet waste from the facility.

Provisions for solid waste management;

Solid waste shall be collected at a minimum of once per week and disposed of in an appropriate dumpster or garbage truck. Waste shall be disposed of in a legal manner, at a state licensed recycling center or landfill.

Routine Inspections and Maintenance of SMS BMP's

Routine inspections and maintenance shall be performed in accordance with the Operations and Maintenance Plan

Spill Prevention, Control and Countermeasures

Continuing Care Management, LLC and its subsidiaries have in place a SPCC plan for all of their assets. The plan is updated periodically and/or when necessary due to changes to the existing facility. A copy is kept onsite at all times in the event of a spill.

Illicit Discharges

All non-allowable, non-stormwater discharges are prohibited from being directed to the drainage system. The following list of non-stormwater discharges are allowed to drain to the closed drainage system and has been taken from the "NATIONAL POLLUTANT DISCHARGE ELIMINATION SYSTEM (NPDES) GENERAL PERMIT FOR STORM WATER DISCHARGES FROM SMALL MUNICIPAL SEPARATE STORM SEWER SYSTEMS".

"Part I, Section F. Allowable Non-Storm Water Discharges

The following non-storm water discharges are authorized provided it has been determined by the permittee that they are not significant contributors of pollutants to the MS4. If these discharges are identified as significant contributors to the MS4, they must be addressed in the Illicit Discharge Detection and Elimination minimum control measure described in Parts II, III, IV and V.

- 1. Water line flushing,
- 2. Landscape irrigation,
- 3. Diverted stream flows,
- 4. Rising ground waters,
- 5. Uncontaminated ground water infiltration (as defined at 40 cfr 35.2005(20)),
- 6. Uncontaminated pumped ground water,
- 7. Discharge from potable water sources,
- 8. Foundation drains,
- 9. Air conditioning condensation,

10. Irrigation water, springs,

- 11. Water from crawl space pumps,
- 12. Footing drains,
- 13. Lawn watering,
- 14. Individual resident car washing,
- 15. Flows from riparian habitats and wetlands,
- 16. Dechlorinated swimming pool discharges,
- 17. Street wash water, and
- 18. Residential building wash waters, without detergents.

Discharges or flows from firefighting activities occur during emergency situations. The permittee is not expected to evaluate firefighting discharges with regard to pollutant contributions. Therefore, these discharges are authorized as allowable non-storm water discharges, unless identified, by EPA, as significant sources of pollutants to Waters of the U.S.."

APPENDIX E

CONSTRUCTION PERIOD POLLUTION PREVENTION AND EROSION AND SEDIMENTATION CONTROL PLAN - REQUIRED BY STANDARD 8

CONSTRUCTION PERIOD POLLUTION PREVENTION PLAN

& EROSION & SEDIMENTATION CONTROL PLAN

The proposed development at Village Street consists of the construction of an Adult Retirement Community Planned Residential District (ARCPUD) consisting of a four story main residence building which has 40 memory care, 60 assisted living and 54 independent living residential units and 15 attached cottages (two bedroom) as well as 48 two bedroom and 8 three bedroom detached cottages, a two story medical office building, and a pavilion.

The proposed Stormwater Management system consists of a series of deep sump catch basins, roof leaders, pipes, and manholes to collect stormwater; and a series of infiltration trenches, water quality units, vegetated detention basins, and outlet control structures which both treat and control the proposed flows. Each detention basin is sized to slow down the peak flow from the 100-year storm.

Soils, Slopes, Vegetation, and Current Drainage Patterns

The Soil Conservation Service map for the area indicates that the site is made of seven soil types which include 4 – Rippowam silt loam, 0 to 3 percent slopes (Hydrologic Soil Group D), 5 – Saco silt loam, 0 to 3 percent slopes (Hydrologic Soil Group D), 31A – Walpole sandy loam, 0 to 3 percent slopes (Hydrologic Soil Group D), 70A – Ridgebury fine sandy loam, 0 to 5 percent slopes (Hydrologic Soil Group D), 245B – Merrimac fine sandy loam, 3 to 8 percent slopes (Hydrologic Soil Group A), 260B – Sudbury fine sandy loam, 2 to 8 percent slopes (Hydrologic Soil Group B), and 310B – Udorthents, Woodbridge fine sandy loam, 3 to 8 percent slopes (Hydrologic Soil Group C). The site currently consists of a wooded lot with open areas. Topography generally slopes to the southwest towards the Charles River.

Minimize Disturbed Area and Protect Natural Features and Soil

The silt fence line defines the limit of work and that all areas outside of the clearing line are to be protected and remain undisturbed. The silt fence line shall be installed prior to the start of construction. The silt fence line shall be inspected and maintained on a weekly basis and/or within 12 hours of a storm event >0.5".

Phase Construction Activity

Construction will occur in a single phase.

Stabilize Soils

Soils will be stabilized by seeding. Stockpiled soils, such as top soil, will be stabilized with temporary seed no later than 14 days from the last construction activity in that area.

Permanent Seeding/ Sodding: Shall be performed upon completion of the area. These areas shall be inspected and maintained on a monthly basis and/or within 12 hours of a storm event >0.5".

Temporary Seeding/ Sodding: Shall be performed within 14 days of last construction activity in the area. These areas shall be inspected and maintained on a weekly basis and/or within 12 hours of a storm event >0.5".

Protect Slopes

Maximum allowable slopes on the project are 3:1 and these slopes will be stabilized using the methods described in the previous section.

Establish Perimeter Controls and Sediment Barriers

A silt fence erosion control barrier will be installed along the down gradient portions of project site that are to be disturbed by construction related activities. Installation will occur prior to the start of these activities and the contractor shall be aware that areas outside the erosion control barrier are to remain undisturbed. The silt fence line shall be inspected and maintained on a weekly basis and/or within 12 hours of a storm event >0.5".

Retain Sediment On-Site

Sediment is retained on site via the aforementioned erosion control barrier. Sediment that builds up along the silt fence line is manually removed during the inspection. Completed slopes are stabilized immediately as described above to avoid the on-going deposition of sediment against the erosion control barrier.

Establish Stabilized Construction Exits

A stabilized construction site exit is proposed for the project site and will be put in place upon completion of the silt fence installation. Please refer to the Comprehensive Permit Plans for proposed location and installation details. In addition to the stabilized construction exit, dump trucks hauling material to and from the site will be covered with a tarpaulin and the paved street adjacent to the site entrance will be manually swept as required to remove excess mud, dirt, or rock tracked from the site. The construction exit will be inspected and maintained on a weekly basis.

Material Handling and Waste Management

All solid waste materials will be collected at a minimum of once per week and stored in a covered metal dumpster rented from a licensed solid waste management company. All trash and construction debris from the site will be deposited in the dumpster. The dumpster will be emptied as needed and the trash will be hauled to an appropriate landfill. No construction materials or stumps will be buried on-site. All personnel will be instructed regarding the correct procedure for waste disposal. All sanitary waste will be collected from the portable units a minimum of once per week by a licensed waste hauling company. More specifically, the following guidelines will be followed:

- Fertilizers will be applied only in the minimum amounts recommended by the manufacturer.
- Fertilizers will be worked into the soil to limit exposure to stormwater.
- Fertilizers shall not be used within 25 feet of the wetland resource areas. Excess fertilizers shall be swept up from all impervious surfaces and not allowed to run into the drainage system.
- Fertilizers will be stored in a covered shed and partially used bags will be transferred to a sealable bin to avoid spills.
- Any asphalt substances used onsite will be applied according to the manufacturer's recommendation.
- Sanitary waste will be collected from portable toilets a minimum of once a week to avoid overfilling.
- A covered dumpster will be used for all waste materials.
- Salt will be applied only in the minimum amounts recommended by the manufacturer.

• Salt shall not be used within 25 feet of the wetland resource areas.

Establish Proper Building Material Staging Areas

Construction materials will be stored on-site in designated material staging areas that minimize the exposure of the materials to stormwater.

Designate Concrete Truck Washout Areas

Concrete trucks will be directed to a washout area to be established outside of the 100 foot wetland buffer. Washout areas shall consist of a layer of polyurethane sheeting draped over a rectangular area built out of straw bales.

Establish Proper Equipment/Vehicle Fueling and Maintenance Practices

The following equipment/vehicle fueling and maintenance practice(s) will be implemented to control pollutants to stormwater:

- Petroleum products related to the operation of said equipment will be stored in tightly sealed containers, which will be clearly labeled.
- Spray guns will be cleaned on a disposable tarp.

Spill Prevention and Control Plan

The following guidelines will be followed to aid in the prevention and control of unanticipated spills on-site:

- Spill kits will be included with all fueling sources and maintenance activities.
- Materials and equipment necessary for spill cleanup will be kept onsite. Equipment will include, but not be limited to, brooms, dust pans, mops, rags, gloves, goggles, kitty litter, sand, saw dust, and plastic and metal trash containers.
- All spills will be cleaned up immediately upon discovery. Spills large enough to reach the storm system will be reported to the Massachusetts DEP or National Response Center at 1-800-424-8802.

APPENDIX F

OPERATION AND MAINTENANCE PLAN - REQUIRED BY STANDARD 9

OPERATION AND MAINTENANCE PLAN

To keep the Stormwater Management System (SMS) functioning properly and to ensure that the Total Suspended Solids (TSS) are reduced, periodic maintenance is required. The owner/operator of the facility is responsible for the periodic maintenance requirements of the SMS. Continuing Care Management is the owner and will be the party responsible for the maintenance of the SMS. The following is a guideline of the specific maintenance schedules and tasks required to keep the SMS functioning properly.

Unscheduled Maintenance

The following inspections and maintenance activities must be completed after each rain event in excess of two-inches (2"), or after any snow or rain event accompanied by high winds:

1. Inspect the vegetated detention basins for debris. Remove any branches, trash or other large debris that could interfere with the proper operation of the inlet or outlet of the basins.

General Maintenance

The following inspections and maintenance activities must be completed on a regular basis as conditions warrant:

- 1. Maintain the grassy side slopes of the vegetated detention basins through regular mowing. Keep the grass between three and six inches (3"-6") in length. Remove the grass clippings to prevent them from impeding the flow of stormwater from the inlets or outlets.
- 2. During the fall and the spring remove any accumulated leaves from the catch basin and outlet control structure grates, rip-rap inlet and outlet aprons including flared end sections, detention basin(s), plunge pools, and level spreaders.

Quarterly Maintenance

The following inspections and maintenance activities must be completed quarterly (January 15, April 15, July 15, October 15 or other acceptable quarterly dates):

- 1. Sweep, vacuum, or clean the roadway area to reduce the amount of sediment entering the SMS.
- 2. Inspect the catch basin sumps for debris. Remove any branches, trash or other large debris that could interfere with the proper operation of the outlet of the catch basin. Remove accumulated sediment, by use of a clamshell bucket or vacuum truck, when it reaches a height of 18-inches but not less than annually.
- 3. Inspect the vegetated detention basins, outlet control structures, flared ends, and plunge pools and level spreaders for debris. Remove any branches, trash or other large debris that could interfere with the proper operation of the inlet or outlet of the basin. Remove any accumulated sediment, by the use of hand tools (shovels, rakes, wheelbarrows, etc.) when it exceeds three-inches (3") but not less than annually.

Annual Maintenance

The following inspections and maintenance activities must be completed annually (April 15 or another acceptable date):

1. Sweep, vacuum or clean the roadway area to reduce the amount of sediment entering the SMS.

- 2. Remove accumulated sediment from the catch basin sumps by use of a clamshell bucket or vacuum truck. Inspect the hood to ensure that it is properly secured. If excessive sediment is encountered in the catch basin sump and or the inlet to the catch basin, spot inspect infiltration systems. If more than ½" of sediment is encountered in an infiltration system, jet wash system and then remove any additional sediment from catch basin sumps.
- 3. Remove any accumulated sediment from plunge pools by the use of a clamshell bucket or by the use of hand tools (shovels, rakes, wheelbarrows, etc.). Reset any displaced rip-rap.
- 4. Remove any accumulated sediment from the vegetated detention basins, by the use of hand tools (shovels, rakes, wheelbarrows, etc.).

Water Quality Unit Maintenance

Refer to Stormceptor® Owner's Manual found in Appendix I for operational and maintenance information on the water quality units found on site.

Continuing Care Management, LLC

SALMON HEALTH AND RETIREMENT COMMUNITY

VILLAGE STREET, MEDWAY, MASSACHUSETTS

Stormwater Management System Operation & Maintenance Checklist

Unscheduled Maintenance

The following inspections and maintenance activities must be completed after each rain event in excess of two-inches (2"), or after any snow or rain event accompanied by high winds

• Inspect the detention basins for debris. Remove any branches, trash or other large debris that could interfere with the proper operation of the inlets or outlets of the basins.

General Maintenance

- Mow the grass side slopes of the detention basins through regular mowing. Keep the grass between three and six inches (3"-6") in length. Remove the grass clippings to prevent them from impeding the flow of stormwater from the inlets or outlets
- During the fall and the spring remove leaves from the catch basin and inlet control structure grates, rip-rap inlet and outlet aprons including flared end sections, detention basin(s), and plunge pools.

Quarterly Maintenance

- Sweep, vacuum, or clean the roadway area
- Inspect the catch basin sumps for debris. Remove any branches, trash or other large debris that could interfere with the proper operation of the outlet of the catch basin. Remove accumulated sediment, by use of a clamshell bucket or vacuum truck, when it reaches a height of 18-inches but not less than annually.
- Inspect the detention basins, inlet structures, flared ends, and plunge pools for debris. Remove any branches, trash or other large debris that could interfere with the proper operation of the inlet or outlet of the basin. Remove any accumulated sediment, by the use of hand tools (shovels, rakes, wheelbarrows, etc.) when it exceeds three-inches (3") but not less than annually.

Annual Maintenance

- Sweep, vacuum, or clean the roadway area.
- Remove sediment from the catch basin sumps by use of a clamshell bucket or vacuum truck. Inspect the hood to ensure that it is properly secured. If excessive sediment is encountered in the catch basin sump and or the inlet to the catch basin, spot inspect the infiltration system. If more than ½" of sediment is encountered in infiltration system, jet wash system and then remove any additional sediment from catch basin sumps.
- Remove sediment from plunge pools by the use of a clamshell bucket or by the use of hand tools (shovels, rakes, wheelbarrows, etc.). Reset any displaced rip-rap.
- Remove sediment from the detention basins with the use of hand tools (shovels, rakes, wheelbarrows, etc.).

Water Quality Unit Maintenance

• Refer to the Stormceptor® Owner's Manual (Appendix I) for operational and maintenance information on the water quality units found on site.

		CONTINUING	G CARE MANAGEMENT, LLC
		SALMON HEALTH	AND RETIREMENT COMMUNITY
		VILLAGE STREE	T, MEDWAY, MASSACHUSETTS
	<u>S</u>	TORMWATER MANAGEMENT	SYSTEM OPERATION & MAINTENANCE LOG
<u>DATE</u>	<u>TIME</u>	MAINTENANCE ACTIVITY	INFILTRATION/DENTENTION FACILIY MAINTAINED

APPENDIX G

ILLICIT DISCHARGE COMPLIANCE STATEMENT- REQUIRED BY STANDARD 10

October 9, 2015

Mr. David Travalini, Chair Medway Conservation Commission Town Hall 155 Village Street Medway, Massachusetts, 02053

Re: 259, 261, 261R, and 263 Village Street, Medway, Massachusetts Illicit Discharge Compliance Statement

Dear Mr. Travalini & Members of the Commission:

Coneco Engineers & Scientists, Incorporated (Coneco), on behalf of our client Continuing Care Management, LLC, is submitting this Illicit Discharge Compliance Statement for the above referenced property.

This Illicit Discharge Compliance Statement is to verify that to the best of our knowledge, no illicit discharges exist on the site presently, nor will they after the proposed development has been completed. The proposed stormwater management system consists of conventional curb and gutter drainage for the roadways including a series of catch basins, drain manholes and pipe which convey stormwater runoff from the roadway areas to a water quality device before entering the proposed infiltration system which will ultimately discharge any remaining runoff upstream of the bordering vegetated wetlands. Roof runoff from the proposed campus building and the majority of the residential units will be recharged through individual subsurface infiltration chambers. These chambers have been designed to accommodate flows from the 100-year storm event. Please refer to "ARCPUD Special Permit Site Plans" prepared by Coneco dated June 12, 2015 for plans showing the proposed stormwater management system. Additionally, the Long Term Pollution Prevention Plan contained herein contains measures to prevent illicit discharges.

Please don't hesitate to contact me at 508-697-3191 (extension 123) should you have any questions and/or comments pertaining to the information contained herein or require additional information and/or further action. Thank you for your time and consideration regarding this matter.

Best Regards, Coneco Engineers & Scientists, Incorporated

Tracy Z. Suarte

Tracy L. Duarte, P.E. Civil Engineer



APPENDIX H

SOIL LOGS

Job No.:	8548		Soi	l Evaluator:	Tracy L. Duarte
Client:	Continuing Care Management LLC			Witness:	N/A
Site Location:	Village Street, Medway			Excavator:	Mobile Excavating
Land Use:				Date:	April 8, 2015
Parent Material:				Weather:	Rain/ Hail 34°F
Water Resource	Conditions: Normal:	Above:	Х	Below:	

TP #15-1 Edge of Woods

Depth	Horizon	Texture	Color	Comments Infiltration Test C		Grou	ndwater	
0-13	А	SL	10YR 3/2		Depth	24"	Mottling	26"
13-25	В	LS	10YR 5/6		0-15 Min.	1/2"	wotting	
25-58	С	M-C LS	2.5Y 5/3		15-30 Min.	1/2"	Wooping	N/A
					30-45 Min.	1/2"	weeping	
					45-60 Min.		Standing	30"
					60-75 Min.		Standing	30
					Rate	2	"/hr	

TP #15-2 Open

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Groundwater	
0-10	А	SL	10YR 3/2	Roots	Depth	18"	Mottling	18"
10-18	В	SL	10YR 4/6		0-15 Min.	3/4"	Motunig	
18-84	С	V. Fine LS	2.5Y 5/3		15-30 Min.	1/2"	Waaping	68"
					30-45 Min.	1/2"	weeping	
					45-60 Min.	1/2"	Standing	79"
					60-75 Min.		Standing	70
					Rate	2	"/hr	

TP #15-3 Open

Depth	Horizon	Texture	Color	Comments Infiltration Test Ground		ndwater		
0-12	А	SL	10YR 3/4		Depth	18"	Mottling	N/A
12-18	В	Sand	10YR 4/6		0-15 Min.	2 3/4"	Motunig	11/11
18-74	С	Sand	2.5Y 5/3		15-30 Min.	2 1/2"	Weeping	N/A
					30-45 Min.	2 1/4"	weeping	
					45-60 Min.	2 1/4"	Standing	NI/A
					60-75 Min.	2 1/4"	Standing	1N/A
					Rate	9	"/hr	

TP #15-4 Open

Depth	Horizon	Texture	Color	Comments Infiltration Test Gr		Grou	ndwater	
0-12	А	SL	10YR 3/2		Depth	14"	Mottling	26"
12-24	В	LS	10YR 4/6		0-15 Min.	3/8"	Motunig	20
24-68	С	LS	2.5Y 5/3	Heavy mottling throughout	15-30 Min.	3/8"	Weening	28"
					30-45 Min.	1/4"	weeping	
					45-60 Min.	1/4"	Standing	45"
					60-75 Min.	1/4"	- standing	45
					Rate	1	"/hr	

Job No.:	8548		Soi	il Evaluator:	Tracy L. Duarte
Client:	Continuing Care Management LLC			Witness:	N/A
Site Location:	Village Street, Medway			Excavator:	Mobile Excavating
Land Use:				Date:	April 8, 2015
Parent Material:				Weather:	Rain/ Hail 34°F
Water Resource	Conditions: Normal:	Above:	Х	Below:	

TP #15-5 Wooded

Depth	Horizon	Texture	Color	Comments Infiltration Test Grour		ndwater		
0-16	А	SL	10YR 2/2	Roots	Depth	30"	Mottling	30"
16-30	В	SL	10YR 4/6		0-15 Min.	1/8"	Motting	50
30-72	С	V. Fine SL	2.5Y 5/3	Platey, heavy mottling throughout	15-30 Min.	1/16"	Weeping	36"
					30-45 Min.	1/16"	weeping	
					45-60 Min.	1/16"	Standing	60"
					60-75 Min.		Standing	00
					Rate	0.25	"/hr	

TP #15-11 Wooded

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Groundwater	
0-16	А	SL	10YR 2/2	Roots	Depth	24"	Mottling	26"
16-24	В	M-C LS	10YR 5/6		0-15 Min.	3/4"	wotting	20
24-70	С	Sand	2.5Y 5/3	Gravelly	15-30 Min.	3/4"	Wooping	N/A
					30-45 Min.	1/2"	weeping	
					45-60 Min.	1/2"	Standing	30"
					60-75 Min.	1/2"	Standing	50
					Rate	2	"/hr	

TP #15-12 Brush

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Groundwater	
0-16	А	SL	10YR 2/2	Roots	Depth	18"	Mottling	N/A
16-22	В	M-C LS	10YR 5/6		0-15 Min.	4 1/2"	Motting	11/21
22-58	С	Sand	2.5Y 5/3	Gravelly	15-30 Min.	2 1/2"	Wooping	N/A
					30-45 Min.	2 1/2"	weeping	
					45-60 Min.	2 1/2"	Standing	26"
					60-75 Min.		Standing	20
					Rate	10	"/hr	

TP #15-14 Open

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Groundwater	
0-8	А	SL	10YR 3/4		Depth	18"	Mottling	N/A
8-18	В	Fine SL	10YR 5/6		0-15 Min.	1/2"	wonning	$\pm N/T$
18-48	C1	M-C LS	2.5Y 5/2	Gravelly	15-30 Min.	1/4"	Waaping	N/A
48-50	C2	V. Fine SL	2.5Y 5/2	Platey	30-45 Min.	1/4"	weeping	
					45-60 Min.	1/4"	Standing	26"
					60-75 Min.		Standing	20
					Rate	1	"/hr	

Job No.:	8548		S	oil Evaluator:	Tracy L. Duarte
Client:	Continuing Care Management LLC			Witness:	N/A
Site Location:	Village Street, Medway			Excavator:	Mobile Excavating
Land Use:				Date:	April 8, 2015
Parent Material:				Weather:	Rain/ Hail 34°F
Water Resource	Conditions: Normal:	Above:	Х	Below:	

TP #15-15 Wooded

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Grou	ndwater
0-10	А	SL	10YR 3/2		Depth	6"	Mottling	24"
10-24	В	Fine SL	10YR 5/6		0-15 Min.	3/4"	Mottiling	24
24-36	C1	M-C LS	2.5Y 5/2	Gravelly	15-30 Min.	3/4"	Weeping	16"
36-70	C2	V. Fine SL	2.5Y 5/2	Platey	30-45 Min.	3/4"	weeping	10
					45-60 Min.		Standing	36"
					60-75 Min.		Standing	50
					Rate	3	"/hr	

TP #

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Grou	ndwater
					Depth		Mottling	
					0-15 Min.		Mottiling	
					15-30 Min.		Weeping	
					30-45 Min.		weeping	
					45-60 Min.		Standing	
					60-75 Min.		Standing	
					Rate		"/hr	

TP #

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Grou	ndwater
					Depth		Mottling	
					0-15 Min.		Mottillig	
					15-30 Min.		Wooping	
					30-45 Min.		weeping	
					45-60 Min.		Standing	
					60-75 Min.		Standing	
					Rate		"/hr	

TP #

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Grou	ndwater
					Depth		Mottling	
					0-15 Min.		worming	
					15-30 Min.		Weeping	
					30-45 Min.		weeping	
					45-60 Min.		Standing	
					60-75 Min.		Standing	
					Rate		"/hr	

Job No.:	8548		So	il Evaluator:	Tracy L. Duarte
Client:	Continuing Care Management LLC			Witness:	N/A
Site Location:	Village Street, Medway			Excavator:	Mobile Excavating
Land Use:				Date:	April 9, 2015
Parent Material:				Weather:	Rain/ 38°F
Water Resource	Conditions: Normal:	Above:	Х	Below:	

TP #15-6 Woods

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Grou	ndwater
0-14	А	SL	10YR 3/2	Leaf litter/ roots	Depth	32"	Mottling	30"
14-32	В	LS	10YR 5/6		0-15 Min.	3"	Mottillig	52
32-56	C1	M-C LS	2.5Y 5/3	Heavy mottling ring at C1/C2	15-30 Min.	3"	Weeping	40"
56-82	C2	V. Fine SL	2.5Y 5/3	interface	30-45 Min.	3"	weeping	40
					45-60 Min.		Standing	62"
					60-75 Min.		Standing	02
					Rate	12	"/hr	

TP #15-7 Woods

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Grou	ndwater
0-12	А	SL	10YR 2/2		Depth	20"	Mottling	18"
12-26	В	LS	10YR 5/6		0-15 Min.	3/8"	Motunig	10
26-66	C1	M-C LS	2.5Y 5/3	Heavy mottling/ weeping	15-30 Min.	3/8"	Weeping	42"
66-92	C2	V. Fine SL	2.5Y 5/3	Platey	30-45 Min.	3/8"	weeping	72
					45-60 Min.		Standing	82"
					60-75 Min.		Standing	02
					Rate	1.33"	"/hr	

TP #15-8 Woods

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Grou	ndwater
0-18	А	SL	10YR 3/2		Depth	28"	Mottling	30"
18-30	В	LS	10YR 5/6		0-15 Min.	1/2"	Wotting	50
30-54	C1	M-C LS	2.5Y 5/3	Heavy mottling/ weeping	15-30 Min.	1/2"	Wooping	30"
54-90	C2	V. Fine SL	2.5Y 5/3		30-45 Min.	1/2"	weeping	50
					45-60 Min.		Standing	<u>8</u> 4"
					60-75 Min.		Standing	04
					Rate	2	"/hr	

TP #15-9 Woods

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Grou	ndwater
0-14	А	SL	10YR 3/2	Roots	Depth	26"	Mottling	26"
14-26	В	LS	10YR 5/6		0-15 Min.	1/2"	Wotting	20
26-44	C1	V. Fine SL	2.5Y 5/2	Heavy mottling/ weeping	15-30 Min.	1/2"	Weeping	30"
44-88	C2	M-C LS	2.5Y 5/3	V. Gravelly	30-45 Min.	1/2"	weeping	50
					45-60 Min.		Standing	70"
					60-75 Min.		Standing	70
					D i	0	11 /1	

Rate 2 "/hr

Job No.:	8548		So	il Evaluator:	Tracy L. Duarte
Client:	Continuing Care Management LLC			Witness:	N/A
Site Location:	Village Street, Medway			Excavator:	Mobile Excavating
Land Use:				Date:	April 9, 2015
Parent Material:				Weather:	Rain/ 38°F
Water Resource	Conditions: Normal:	Above:	Х	Below:	

TP #15-10 Woods

Depth	Horizon	Texture	Color	Comments	Infiltration Test		Grou	ndwater
0-12	А	SL	10YR 3/2	Roots	Depth	24"	Mottling	36"
12-24	В	LS	10YR 4/6		0-15 Min.		Motunig	50
24-36	C1	M-C LS	2.5Y 5/3		15-30 Min.		Weeping	36"
36-60	C2	M-C Sand	2.5Y 5/3	Heavy mottling, 5% gravel	30-45 Min.		weeping	50
60-92	C3	LS	2.5Y 5/3		45-60 Min.		Standing	80"
					60-75 Min.		Standing	00
					Rate	N/A	"/hr	

Note: Unable to Saturate >1"/min.

TP #15-13

Depth	Horizon	Texture	Color	Comments	Infiltrati	on Test	Grou	ndwater
0-12	А	SL	10YR 3/2		Depth	20"	Mottling	26"
12-24	В	LS	10YR 5/6		0-15 Min.	5/8"	Motiling	20
24-53	C1	M-C LS	2.5Y 5/2	Heavy mottling, platey	15-30 Min.	5/8"	Weeping	40"
53-66	C2	V. Fine SL	2.5Y 5/3		30-45 Min.	5/8"	weeping	+0
					45-60 Min.		Standing	54"
					60-75 Min.		Standing	54
					Rate	2.5	"/hr	

TP #15-16 Open

Depth	Horizon	Texture	Color	Comments	Infiltrati	on Test	Grou	ndwater
0-12	А	SL	10YR 3/2		Depth	16"	Mottling	22"
12-20	В	F. Sand	10YR 5/6		0-15 Min.	1"	motiling	
20-76	С	V. Fine SL	2.5Y 5/2	Heavy mottling/ firm in place	15-30 Min.	1"	Wooping	40"
					30-45 Min.	1"	weeping	40
					45-60 Min.	1"	Standing	68"
					60-75 Min.		Standing	00
					Rate	4"	"/hr	

TP #15-17 Woods

Depth	Horizon	Texture	Color	Comments	Infiltrat	on Test	Grou	ndwater
0-12	А	SL	10YR 3/2	Leaf litter/ roots	Depth	16"	Mottling	N/A
12-28	В	Fine LS	10YR 4/6		0-15 Min.	2 1/2"	Motillig	1 1/ 21
28-96	С	Fine LS	2.5Y 5/2	Platey	15-30 Min.	2 1/2"	Weeping	88"
					30-45 Min.	2 1/2"	weeping	00
					45-60 Min.		Standing	۹۸"
					60-75 Min.		Standing	74
					D	10	11 /1	

Rate 10 "/hr

	Job No.:	8548				Soil E	valuator: "	Гracy L. D	uarte	
	Client:	Continuing	Care Manage	ement LLC	-		Witness: 1	N/A		
Site	Location:	Village Stree	et Medwav		-	E	xcavator:	Mobile Ex	ravating	
0.100	Lond User	, muge ouro	et, med way		-		Dato		15	
	Land Use.				-		Date.	<u>April 9, 20</u>		
Paren	t Material:				-		Weather:	Rain/ 38°F	i	
Water	r Resource	Conditions:	Normal:		Above:	Х	Below:		_	
TP #15-18	Woods									
Depth	Horizon	Texture	Color		Comments		Infiltratio	on Test	Groun	ndwater
0-12	А	SL	10YR 3/2	Leaf litter/ 1	roots		Depth	18"		NT / A
12-24	В	M. Sand	10YR 4/6			()-15 Min.		Mottling	1N/A
24-100	С	M. Sand	2.5Y 5/3			1	5-30 Min.		Weening	N/A
						3	0-45 Min.		weeping	1 N / 1 N
						4	5-60 Min.		Standing	N/A
						6	0-75 Min.		Standing	± N / ± L
							Rate	N/A	"/hr	
TP #			-				Note:	Unable to S	Saturate >1.25	"/min.
Depth	Horizon	Texture	Color		Comments		Infiltratio	on Test	Grour	ndwater
							Depth		Mottling	
						()-15 Min.		Motunig	
						1	5-30 Min.		Weening	
						3	0-45 Min.		weeping	
						4	5-60 Min.		Standing	
						6	0-75 Min.		0 000000	
							Rate		"/hr	
TP #	1	1	1							
Depth	Horizon	Texture	Color		Comments		Infiltratio	on Test	Groun	ndwater
							Depth		Mottling	
						()-15 Min.		moning	
						1	5-30 Min.		Weening	
						3	0-45 Min.		"ceping	
	<u> </u>					4	5-60 Min.		Standing	
						6	0-75 Min.		8	
ТР #							Rate		"/hr	
Depth	Horizon	Texture	Color		Comments		Infiltratio	on Test	Grour	ndwater
-P										
							Depth		Mottling	
	 					()-15 Min.		Ŭ,	
						1	5-30 Min.		Weeping	
						3	0-45 Min.		╉──┤	
						4	0.75 Min.		Standing	
						0	0-/3 Min.			

Rate

"/hr

Job No.:	8548		So	il Evaluator:	Tracy L. Duarte
Client:	Continuing Care Management LLC			Witness:	N/A
Site Location:	Village Street, Medway			Excavator:	Mobile Excavating
Land Use:				Date:	April 10, 2015
Parent Material:				Weather:	Rain/ 46°F
Water Resource	Conditions: Normal:	Above:	Х	Below:	

TP #15-19 Woods

Depth	Horizon	Texture	Color	Comments	Infiltrat	ion Test	Grou	ndwater
0-12	А	SL	10YR 3/3		Depth	16"/32"	Mottling	N/A
12-22	В	LS	10YR 4/6		0-15 Min.	1.5" / .75"	Mottiling	11/11
22-39	C1	M-C LS	2.5Y 5/2		15-30 Min.	1" / .75"	Wooping	68"
39-86	C2	Fine LS	2.5Y 5/3	5% gravel	30-45 Min.	1" / .75"	weeping	08
					45-60 Min.	1" / .75"	Standing	84"
					60-75 Min.		Standing	04
					Rate	4 / 3	"/hr	

TP #15-20 Woods

Depth	Horizon	Texture	Color	Comments	Infiltrat	ion Test	Grou	ndwater
0-12	А	SL	10YR 3/3	Roots, leaf litter	Depth	24"	Mottling	N/A
12-24	В	M-C LS	10YR 4/6		0-15 Min.		Motunig	11/21
24-48	C1	M-C LS	2.5Y 5/4		15-30 Min.		Weeping	N/A
48-72	C2	Sand	2.5Y 5/2		30-45 Min.		weeping	11/21
					45-60 Min.		Standing	N/A
					60-75 Min.		Standing	11/21

Rate N/A "/hr

TP #15-21	TP #15-21 WoodsNote: Unable to Saturate >2.75"/min.								
Depth	Horizon	Texture	Color	Comments	Infiltrati	on Test	Grou	ndwater	
0-14	А	SL	10YR 3/2		Depth	20"	Mottling	14"	
14-22	В	Fine SL	10YR 5/6	Heavy weeping	0-15 Min.	1/4"	Wotting	14	
22-38	C1	Fine SL	2.5Y 4/4	super saturated from 22" and below	15-30 Min.	1/8"	Weeping	14"	
38-60	C2	Fine SL	2.5Y 5/4	5% gravel	30-45 Min.	1/8"	weeping	14	
				Note: Pocket of fill in east corner	45-60 Min.	1/8"	Standing	55"	
				from 0-36"	60-75 Min.		Standing	55	
					Rate	0.5	"/hr		

TP #15-27 Woods

Depth	Horizon	Texture	Color	Comments	Infiltrati	on Test	Grou	ndwater
0-14	А	SL	10YR 2/2	Roots, leaf litter	Depth	18"	Mottling	26"
14-26	В	M-C LS	10YR 4/6	super saturated from 24" and below	0-15 Min.	1/4"	wonning	20
26-68	С	M-C LS	2.5Y 5/4	10% gravel, heavy mottling at B/C	15-30 Min.	1/4"	Weeping	26"
				interface	30-45 Min.	1/4"	weeping	20
					45-60 Min.		Standing	56"
					60-75 Min.		Standing	50
					Rate	1	"/hr	

APPENDIX I

STORMCEPTOR SIZING DETAILED REPORT AND OWNER'S MANUAL



Stormceptor Sizing Detailed Report PCSWMM for Stormceptor

Project Information

Date	6/10/2015
Project Name	Salmon ARCPUD
Project Number	8548
Location	Medwawy, MA

Stormwater Quality Objective

This report outlines how Stormceptor System can achieve a defined water quality objective through the removal of total suspended solids (TSS). Attached to this report is the Stormceptor Sizing Summary.

Stormceptor System Recommendation

The Stormceptor System model STC 450i achieves the water quality objective removing 83% TSS for a Fine (organics, silts and sand) particle size distribution.

The Stormceptor System

The Stormceptor oil and sediment separator is sized to treat stormwater runoff by removing pollutants through gravity separation and flotation. Stormceptor's patented design generates positive TSS removal for all rainfall events, including large storms. Significant levels of pollutants such as heavy metals, free oils and nutrients are prevented from entering natural water resources and the re-suspension of previously captured sediment (scour) does not occur.

Stormceptor provides a high level of TSS removal for small frequent storm events that represent the majority of annual rainfall volume and pollutant load. Positive treatment continues for large infrequent events, however, such events have little impact on the average annual TSS removal as they represent a small percentage of the total runoff volume and pollutant load.

Stormceptor is the only oil and sediment separator on the market sized to remove TSS for a wide range of particle sizes, including fine sediments (clays and silts), that are often overlooked in the design of other stormwater treatment devices.





Small storms dominate hydrologic activity, US EPA reports

"Early efforts in stormwater management focused on flood events ranging from the 2-yr to the 100-yr storm. Increasingly stormwater professionals have come to realize that small storms (i.e. < 1 in. rainfall) dominate watershed hydrologic parameters typically associated with water quality management issues and BMP design. These small storms are responsible for most annual urban runoff and groundwater recharge. Likewise, with the exception of eroded sediment, they are responsible for most pollutant washoff from urban surfaces. Therefore, the small storms are of most concern for the stormwater management objectives of ground water recharge, water quality resource protection and thermal impacts control."

"Most rainfall events are much smaller than design storms used for urban drainage models. In any given area, most frequently recurrent rainfall events are small (less than 1 in. of daily rainfall)."

"Continuous simulation offers possibilities for designing and managing BMPs on an individual site-by-site basis that are not provided by other widely used simpler analysis methods. Therefore its application and use should be encouraged."

– US EPA Stormwater Best Management Practice Design Guide, Volume 1 – General Considerations, 2004

Design Methodology

Each Stormceptor system is sized using PCSWMM for Stormceptor, a continuous simulation model based on US EPA SWMM. The program calculates hydrology from up-to-date local historical rainfall data and specified site parameters. With US EPA SWMM's precision, every Stormceptor unit is designed to achieve a defined water quality objective.

The TSS removal data presented follows US EPA guidelines to reduce the average annual TSS load. Stormceptor's unit process for TSS removal is settling. The settling model calculates TSS removal by analyzing (summary of analysis presented in Appendix 2):

- Site parameters
- Continuous historical rainfall, including duration, distribution, peaks (Figure 1)
- Interevent periods
- Particle size distribution
- Particle settling velocities (Stokes Law, corrected for drag)
- TSS load (Figure 2)
- Detention time of the system

The Stormceptor System maintains continuous positive TSS removal for all influent flow rates. Figure 3 illustrates the continuous treatment by Stormceptor throughout the full range of storm events analyzed. It is clear that large events do not significantly impact the average annual TSS removal. There is no decline in cumulative TSS removal, indicating scour does not occur as the flow rate increases.







Figure 1. Runoff Volume by Flow Rate for BLUE HILL – MA 736, 1948 to 2005 for 0.81 ac, 65.2% **impervious.** Small frequent storm events represent the majority of annual rainfall volume. Large infrequent events have little impact on the average annual TSS removal, as they represent a small percentage of the total annual volume of runoff.



Figure 2. Long Term Pollutant Load by Flow Rate for BLUE HILL – 736, 1948 to 2005 for 0.81 ac, 65.2% impervious. The majority of the annual pollutant load is transported by small frequent storm





events. Conversely, large infrequent events carry an insignificant percentage of the total annual pollutant load.



Figure 3. Cumulative TSS Removal by Flow Rate for BLUE HILL – 736, 1948 to 2005. Stormceptor continuously removes TSS throughout the full range of storm events analyzed. Note that large events do not significantly impact the average annual TSS removal. Therefore no decline in cumulative TSS removal indicates scour does not occur as the flow rate increases.





Appendix 1 Stormceptor Design Summary

Project Information

-	
Date	6/10/2015
Project Name	Salmon ARCPUD
Project Number	8548
Location	Medwawy, MA

Designer Information

Company	Coneco Engineers & Scientist
Contact	N/A

Notes

N/A

Drainage Area

Total Area (ac)	0.81
Imperviousness (%)	65.2

The Stormceptor System model STC 450i achieves the water quality objective removing 83% TSS for a Fine (organics, silts and sand) particle size distribution.

Rainfall

Name	BLUE HILL
State	MA
ID	736
Years of Records	1948 to 2005
Latitude	42°12'44"N
Longitude	71°6'53"W

Water Quality Objective

TSS Removal (%)	80

Upstream Storage

•	
Storage	Discharge
(ac-ft)	(cfs)
0	0

Stormceptor Sizing Summary

Stormceptor Model	TSS Removal %
STC 450i	83
STC 900	89
STC 1200	89
STC 1800	89
STC 2400	92
STC 3600	92
STC 4800	94
STC 6000	94
STC 7200	95
STC 11000	97
STC 13000	97
STC 16000	97





Particle Size Distribution

Removing silt particles from runoff ensures that the majority of the pollutants, such as hydrocarbons and heavy metals that adhere to fine particles, are not discharged into our natural water courses. The table below lists the particle size distribution used to define the annual TSS removal.

			Fine (organic	s, s	silts and sand)			
Particle Size	Distribution	Specific Gravity	Settling Velocity		Particle Size	Distribution	Specific Gravity	Settling Velocity
μm	%	•	ft/s		μm	%	•	ft/s
20	20	1.3	0.0013					
60	20	1.8	0.0051					
150	20	2.2	0.0354					
400	20	2.65	0.2123					
2000	20	2.65	0.9417					

Stormceptor Design Notes

- Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor.
- Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal.
- Only the STC 450i is adaptable to function with a catch basin inlet and/or inline pipes.
- Only the Stormceptor models STC 450i to STC 7200 may accommodate multiple inlet pipes.
- Inlet and outlet invert elevation differences are as follows:

Inlet and Outlet Pipe Invert Elevations Differences

Inlet Pipe Configuration	STC 450i	STC 900 to STC 7200	STC 11000 to STC 16000
Single inlet pipe	3 in.	1 in.	3 in.
Multiple inlet pipes	3 in.	3 in.	Only one inlet pipe.

- Design estimates are based on stable site conditions only, after construction is completed.
- Design estimates assume that the storm drain is not submerged during zero flows. For submerged applications, please contact your local Stormceptor representative.
- Design estimates may be modified for specific spills controls. Please contact your local Stormceptor representative for further assistance.
- For pricing inquiries or assistance, please contact Rinker Materials 1 (800) 909-7763 www.rinkerstormceptor.com





Appendix 2 **Summary of Design Assumptions**

SITE DETAILS

Site Drainage Area

5.10 = 1			
Total Area (ac)	0.81	Imperviousness (%)	65.2
Surface Characteristics		Infiltration Parameters	
Width (ft)	376	Horton's equation is used to estimate in	nfiltration
Slope (%)	2	Max. Infiltration Rate (in/hr)	2.44
Impervious Depression Storage (in.)	0.02	Min. Infiltration Rate (in/hr)	0.4
Pervious Depression Storage (in.)	0.2	Decay Rate (s ⁻¹)	0.00055
Impervious Manning's n	0.015	Regeneration Rate (s^{-1})	0.01
Pervious Manning's n	0.25		
		Evaporation	
Maintenance Frequency		Daily Evaporation Rate (inches/day)	0.1
Sediment build-up reduces the storage sedimentation. Frequency of maintenan assumed for TSS removal calculations	volume for nce is	Dry Weather Flow	_

assumed for TSS removal calculations. 12 Maintenance Frequency (months)

Dry Weather Flow (cfs)	No
------------------------	----

Upstream Attenuation

Stage-storage and stage-discharge relationship used to model attenuation upstream of the Stormceptor System is identified in the table below.

Storage ac-ft	Discharge cfs
0	0





PARTICLE SIZE DISTRIBUTION

Particle Size Distribution

Removing fine particles from runoff ensures the majority of pollutants, such as heavy metals, hydrocarbons, free oils and nutrients are not discharged into natural water resources. The table below identifies the particle size distribution selected to define TSS removal for the design of the Stormceptor System.

Fine (organics, silts and sand)								
Particle Size	Distribution	Specific Gravity	Settling Velocity		Particle Size	Distribution	Specific Gravity	Settling Velocity
μm	%		ft/s		μm	%		ft/s
20 60 150 400 2000	20 20 20 20 20	1.3 1.8 2.2 2.65 2.65	0.0013 0.0051 0.0354 0.2123 0.9417					



PCSWMM for Stormceptor Grain Size Distributions

Figure 1. PCSWMM for Stormceptor standard design grain size distributions.



TSS LOADING

TSS Loading Parameters

TSS Loading	Function
-------------	----------

Buildup / Washoff

Parameters

Target Event Mean Concentration (EMC) (mg/L)	125
Exponential Buildup Power	0.4
Exponential Washoff Exponential	0.2

HYDROLOGY ANALYSIS

PCSWMM for Stormceptor calculates annual hydrology with the US EPA SWMM and local continuous historical rainfall data. Performance calculations of the Stormceptor System are based on the average annual removal of TSS for the selected site parameters. The Stormceptor System is engineered to capture fine particles (silts and sands) by focusing on average annual runoff volume ensuring positive removal efficiency is maintained during all rainfall events, while preventing the opportunity for negative removal efficiency (scour).

Smaller recurring storms account for the majority of rainfall events and average annual runoff volume, as observed in the historical rainfall data analyses presented in this section.

Rainfall Station

Rainfall Station	BLUE HILL		
Rainfall File Name	MA736.NDC	Total Number of Events	9865
Latitude	42°12'44"N	Total Rainfall (in.)	2849.7
Longitude	71°6'53"W	Average Annual Rainfall (in.)	49.1
Elevation (ft)	630	Total Evaporation (in.)	163.2
Rainfall Period of Record (y)	58	Total Infiltration (in.)	975.9
Total Rainfall Period (y)	58	Percentage of Rainfall that is Runoff (%)	62.4





Rainfall Event Analysis

Rainfall Depth	No. of Events	Percentage of Total Events	Total Volume	Percentage of Annual Volume
in.		%	in.	%
0.25	7098	72.0	431	15.1
0.50	1076	10.9	393	13.8
0.75	563	5.7	350	12.3
1.00	360	3.6	311	10.9
1.25	257	2.6	288	10.1
1.50	151	1.5	207	7.3
1.75	102	1.0	165	5.8
2.00	70	0.7	130	4.6
2.25	42	0.4	89	3.1
2.50	41	0.4	98	3.4
2.75	27	0.3	71	2.5
3.00	21	0.2	61	2.1
3.25	13	0.1	40	1.4
3.50	10	0.1	34	1.2
3.75	5	0.1	18	0.6
4.00	2	0.0	8	0.3
4.25	1	0.0	4	0.1
4.50	4	0.0	18	0.6
4.75	4	0.0	18	0.6
5.00	0	0.0	0	0.0
5.25	1	0.0	5	0.2
5.50	3	0.0	16	0.6
5.75	2	0.0	11	0.4
6.00	4	0.0	23	0.8
6.25	0	0.0	0	0.0
6.50	0	0.0	0	0.0
6.75	1	0.0	7	0.2
7.00	1	0.0	7	0.2
7.25	2	0.0	14	0.5
7.50	0	0.0	0	0.0
7.75	1	0.0	8	0.3
8.00	1	0.0	8	0.3
8.25	0	0.0	0	0.0
>8.25	2	0.0	17	0.6







Pollutograph

Flow Rate	Cumulative Mass
Cts	%
0.035	72.7
0.141	88.8
0.318	96.6
0.505	99.1
1 271	99.9
1.73	100.0
2.26	100.0
2.86	100.0
3.531	100.0
4.273	100.0
5.085	100.0
5.968	100.0
7 946	100.0
9 041	100.0
10.206	100.0
11.442	100.0
12.749	100.0
14.126	100.0
15.574	100.0
17.092	100.0
18.681	100.0
20.341	100.0
23.873	100.0
25 744	100.0
27.687	100.0
29.7	100.0
31.783	100.0







Stormceptor Sizing Detailed Report PCSWMM for Stormceptor

Project Information

Date	6/10/2015
Project Name	Salmon ARCPUD
Project Number	8548
Location	Medwawy, MA

Stormwater Quality Objective

This report outlines how Stormceptor System can achieve a defined water quality objective through the removal of total suspended solids (TSS). Attached to this report is the Stormceptor Sizing Summary.

Stormceptor System Recommendation

The Stormceptor System model STC 900 achieves the water quality objective removing 86% TSS for a Fine (organics, silts and sand) particle size distribution.

The Stormceptor System

The Stormceptor oil and sediment separator is sized to treat stormwater runoff by removing pollutants through gravity separation and flotation. Stormceptor's patented design generates positive TSS removal for all rainfall events, including large storms. Significant levels of pollutants such as heavy metals, free oils and nutrients are prevented from entering natural water resources and the re-suspension of previously captured sediment (scour) does not occur.

Stormceptor provides a high level of TSS removal for small frequent storm events that represent the majority of annual rainfall volume and pollutant load. Positive treatment continues for large infrequent events, however, such events have little impact on the average annual TSS removal as they represent a small percentage of the total runoff volume and pollutant load.

Stormceptor is the only oil and sediment separator on the market sized to remove TSS for a wide range of particle sizes, including fine sediments (clays and silts), that are often overlooked in the design of other stormwater treatment devices.




Small storms dominate hydrologic activity, US EPA reports

"Early efforts in stormwater management focused on flood events ranging from the 2-yr to the 100-yr storm. Increasingly stormwater professionals have come to realize that small storms (i.e. < 1 in. rainfall) dominate watershed hydrologic parameters typically associated with water quality management issues and BMP design. These small storms are responsible for most annual urban runoff and groundwater recharge. Likewise, with the exception of eroded sediment, they are responsible for most pollutant washoff from urban surfaces. Therefore, the small storms are of most concern for the stormwater management objectives of ground water recharge, water quality resource protection and thermal impacts control."

"Most rainfall events are much smaller than design storms used for urban drainage models. In any given area, most frequently recurrent rainfall events are small (less than 1 in. of daily rainfall)."

"Continuous simulation offers possibilities for designing and managing BMPs on an individual site-by-site basis that are not provided by other widely used simpler analysis methods. Therefore its application and use should be encouraged."

– US EPA Stormwater Best Management Practice Design Guide, Volume 1 – General Considerations, 2004

Design Methodology

Each Stormceptor system is sized using PCSWMM for Stormceptor, a continuous simulation model based on US EPA SWMM. The program calculates hydrology from up-to-date local historical rainfall data and specified site parameters. With US EPA SWMM's precision, every Stormceptor unit is designed to achieve a defined water quality objective.

The TSS removal data presented follows US EPA guidelines to reduce the average annual TSS load. Stormceptor's unit process for TSS removal is settling. The settling model calculates TSS removal by analyzing (summary of analysis presented in Appendix 2):

- Site parameters
- Continuous historical rainfall, including duration, distribution, peaks (Figure 1)
- Interevent periods
- Particle size distribution
- Particle settling velocities (Stokes Law, corrected for drag)
- TSS load (Figure 2)
- Detention time of the system

The Stormceptor System maintains continuous positive TSS removal for all influent flow rates. Figure 3 illustrates the continuous treatment by Stormceptor throughout the full range of storm events analyzed. It is clear that large events do not significantly impact the average annual TSS removal. There is no decline in cumulative TSS removal, indicating scour does not occur as the flow rate increases.







Figure 1. Runoff Volume by Flow Rate for BLUE HILL – MA 736, 1948 to 2005 for 1.27 ac, 66.1% **impervious.** Small frequent storm events represent the majority of annual rainfall volume. Large infrequent events have little impact on the average annual TSS removal, as they represent a small percentage of the total annual volume of runoff.



Figure 2. Long Term Pollutant Load by Flow Rate for BLUE HILL – 736, 1948 to 2005 for 1.27 ac, 66.1% impervious. The majority of the annual pollutant load is transported by small frequent storm





events. Conversely, large infrequent events carry an insignificant percentage of the total annual pollutant load.



Figure 3. Cumulative TSS Removal by Flow Rate for BLUE HILL – 736, 1948 to 2005. Stormceptor continuously removes TSS throughout the full range of storm events analyzed. Note that large events do not significantly impact the average annual TSS removal. Therefore no decline in cumulative TSS removal indicates scour does not occur as the flow rate increases.





Appendix 1 Stormceptor Design Summary

Project Information

-	
Date	6/10/2015
Project Name	Salmon ARCPUD
Project Number	8548
Location	Medwawy, MA

Designer Information

Company	Coneco Engineers & Scientist
Contact	N/A

Notes

N/A

Drainage Area

Total Area (ac)	1.27
Imperviousness (%)	66.1

The Stormceptor System model STC 900 achieves the water quality objective removing 86% TSS for a Fine (organics, silts and sand) particle size distribution.

Rainfall

Name	BLUE HILL
State	MA
ID	736
Years of Records	1948 to 2005
Latitude	42°12'44"N
Longitude	71°6'53"W

Water Quality Objective

TSS Removal (%)	80

Upstream Storage

•	
Storage	Discharge
(ac-ft)	(cfs)
0	0

Stormceptor Sizing Summary

Stormceptor Model	TSS Removal %		
STC 450i	79		
STC 900	86		
STC 1200	86		
STC 1800	86		
STC 2400	89		
STC 3600	90		
STC 4800	92		
STC 6000	92		
STC 7200	94		
STC 11000	95		
STC 13000	95		
STC 16000	96		





Particle Size Distribution

Removing silt particles from runoff ensures that the majority of the pollutants, such as hydrocarbons and heavy metals that adhere to fine particles, are not discharged into our natural water courses. The table below lists the particle size distribution used to define the annual TSS removal.

Fine (organics, silts and sand)								
Particle Size	Distribution	Specific Gravity	Settling Velocity		Particle Size	Distribution	Specific Gravity	Settling Velocity
μm	%		ft/s		μm	%		ft/s
20 60 150 400 2000	20 20 20 20 20	1.3 1.8 2.2 2.65 2.65	0.0013 0.0051 0.0354 0.2123 0.9417					

Stormceptor Design Notes

- Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor.
- Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal.
- Only the STC 450i is adaptable to function with a catch basin inlet and/or inline pipes.
- Only the Stormceptor models STC 450i to STC 7200 may accommodate multiple inlet pipes.
- Inlet and outlet invert elevation differences are as follows:

Inlet and Outlet Pipe Invert Elevations Differences

Inlet Pipe Configuration	STC 450i	STC 900 to STC 7200	STC 11000 to STC 16000
Single inlet pipe	3 in.	1 in.	3 in.
Multiple inlet pipes	3 in.	3 in.	Only one inlet pipe.

- Design estimates are based on stable site conditions only, after construction is completed.
- Design estimates assume that the storm drain is not submerged during zero flows. For submerged applications, please contact your local Stormceptor representative.
- Design estimates may be modified for specific spills controls. Please contact your local Stormceptor representative for further assistance.
- For pricing inquiries or assistance, please contact Rinker Materials 1 (800) 909-7763 www.rinkerstormceptor.com





Appendix 2 **Summary of Design Assumptions**

SITE DETAILS

Site Drainage Area

0.00 =			
Total Area (ac)	1.27	Imperviousness (%)	66.1
Surface Characteristics		Infiltration Parameters	
Width (ft)	470	Horton's equation is used to estimate in	nfiltration
Slope (%)	2	Max. Infiltration Rate (in/hr)	2.44
Impervious Depression Storage (in.)	0.02	Min. Infiltration Rate (in/hr)	0.4
Pervious Depression Storage (in.)	0.2	Decay Rate (s ⁻¹)	0.00055
Impervious Manning's n	0.015	Regeneration Rate (s^{-1})	0.01
Pervious Manning's n	0.25		
		Evaporation	
Maintenance Frequency		Daily Evaporation Rate (inches/day)	0.1
Sediment build-up reduces the storage volume for sedimentation. Frequency of maintenance is		Dry Weather Flow	

Sediment build-up reduces the storage v	/olume loi	
sedimentation. Frequency of maintenance is		
assumed for TSS removal calculations.		
Maintenance Frequency (months)	12	

J

Dry Weather Flow (cfs)	No
------------------------	----

Upstream Attenuation

Stage-storage and stage-discharge relationship used to model attenuation upstream of the Stormceptor System is identified in the table below.

Storage ac-ft	Discharge cfs
0	0





PARTICLE SIZE DISTRIBUTION

Particle Size Distribution

Removing fine particles from runoff ensures the majority of pollutants, such as heavy metals, hydrocarbons, free oils and nutrients are not discharged into natural water resources. The table below identifies the particle size distribution selected to define TSS removal for the design of the Stormceptor System.

Fine (organics, silts and sand)								
Particle Size	Distribution	Specific Gravity	Settling Velocity		Particle Size	Distribution	Specific Gravity	Settling Velocity
μm	%		ft/s		μm	%		ft/s
20 60 150 400 2000	20 20 20 20 20	1.3 1.8 2.2 2.65 2.65	0.0013 0.0051 0.0354 0.2123 0.9417					



PCSWMM for Stormceptor Grain Size Distributions

Figure 1. PCSWMM for Stormceptor standard design grain size distributions.



TSS LOADING

TSS Loading Parameters

TSS Loading Function

Buildup / Washoff

Parameters

Target Event Mean Concentration (EMC) (mg/L)	125
Exponential Buildup Power	0.4
Exponential Washoff Exponential	0.2

HYDROLOGY ANALYSIS

PCSWMM for Stormceptor calculates annual hydrology with the US EPA SWMM and local continuous historical rainfall data. Performance calculations of the Stormceptor System are based on the average annual removal of TSS for the selected site parameters. The Stormceptor System is engineered to capture fine particles (silts and sands) by focusing on average annual runoff volume ensuring positive removal efficiency is maintained during all rainfall events, while preventing the opportunity for negative removal efficiency (scour).

Smaller recurring storms account for the majority of rainfall events and average annual runoff volume, as observed in the historical rainfall data analyses presented in this section.

Rainfall Station

Rainfall Station	BLUE HILL		
Rainfall File Name	MA736.NDC	Total Number of Events	9865
Latitude	42°12'44"N	Total Rainfall (in.)	2849.7
Longitude	71°6'53"W	Average Annual Rainfall (in.)	49.1
Elevation (ft)	630	Total Evaporation (in.)	168.1
Rainfall Period of Record (y)	58	Total Infiltration (in.)	951.3
Total Rainfall Period (y)	58	Percentage of Rainfall that is Runoff (%)	63.0





Rainfall Event Analysis

Rainfall Depth	No. of Events	Percentage of Total Events	Total Volume	Percentage of Annual Volume
in.		%	in.	%
0.25	7098	72.0	431	15.1
0.50	1076	10.9	393	13.8
0.75	563	5.7	350	12.3
1.00	360	3.6	311	10.9
1.25	257	2.6	288	10.1
1.50	151	1.5	207	7.3
1.75	102	1.0	165	5.8
2.00	70	0.7	130	4.6
2.25	42	0.4	89	3.1
2.50	41	0.4	98	3.4
2.75	27	0.3	71	2.5
3.00	21	0.2	61	2.1
3.25	13	0.1	40	1.4
3.50	10	0.1	34	1.2
3.75	5	0.1	18	0.6
4.00	2	0.0	8	0.3
4.25	1	0.0	4	0.1
4.50	4	0.0	18	0.6
4.75	4	0.0	18	0.6
5.00	0	0.0	0	0.0
5.25	1	0.0	5	0.2
5.50	3	0.0	16	0.6
5.75	2	0.0	11	0.4
6.00	4	0.0	23	0.8
6.25	0	0.0	0	0.0
6.50	0	0.0	0	0.0
6.75	1	0.0	7	0.2
7.00	1	0.0	7	0.2
7.25	2	0.0	14	0.5
7.50	0	0.0	0	0.0
7.75	1	0.0	8	0.3
8.00	1	0.0	8	0.3
8.25	0	0.0	0	0.0
>8.25	2	0.0	17	0.6







Pollutograph

Flow Rate	Cumulative Mass
cfs	%
0.035	68.5
0.141	85.0
0.318	93.2
0.505	97.3
1 271	99.6
1.73	99.8
2.26	99.9
2.86	100.0
3.531	100.0
4.273	100.0
5.085	100.0
5.968	100.0
7 946	100.0
9.041	100.0
10.206	100.0
11.442	100.0
12.749	100.0
14.126	100.0
15.574	100.0
17.092	100.0
20.341	100.0
22.072	100.0
23.873	100.0
25.744	100.0
27.687	100.0
29.7	100.0
31.783	100.0







Stormceptor Sizing Detailed Report PCSWMM for Stormceptor

Project Information

Date	6/10/2015
Project Name	Salmon ARCPUD
Project Number	8548
Location	Medwawy, MA

Stormwater Quality Objective

This report outlines how Stormceptor System can achieve a defined water quality objective through the removal of total suspended solids (TSS). Attached to this report is the Stormceptor Sizing Summary.

Stormceptor System Recommendation

The Stormceptor System model STC 4800 achieves the water quality objective removing 80% TSS for a Fine (organics, silts and sand) particle size distribution.

The Stormceptor System

The Stormceptor oil and sediment separator is sized to treat stormwater runoff by removing pollutants through gravity separation and flotation. Stormceptor's patented design generates positive TSS removal for all rainfall events, including large storms. Significant levels of pollutants such as heavy metals, free oils and nutrients are prevented from entering natural water resources and the re-suspension of previously captured sediment (scour) does not occur.

Stormceptor provides a high level of TSS removal for small frequent storm events that represent the majority of annual rainfall volume and pollutant load. Positive treatment continues for large infrequent events, however, such events have little impact on the average annual TSS removal as they represent a small percentage of the total runoff volume and pollutant load.

Stormceptor is the only oil and sediment separator on the market sized to remove TSS for a wide range of particle sizes, including fine sediments (clays and silts), that are often overlooked in the design of other stormwater treatment devices.





Small storms dominate hydrologic activity, US EPA reports

"Early efforts in stormwater management focused on flood events ranging from the 2-yr to the 100-yr storm. Increasingly stormwater professionals have come to realize that small storms (i.e. < 1 in. rainfall) dominate watershed hydrologic parameters typically associated with water quality management issues and BMP design. These small storms are responsible for most annual urban runoff and groundwater recharge. Likewise, with the exception of eroded sediment, they are responsible for most pollutant washoff from urban surfaces. Therefore, the small storms are of most concern for the stormwater management objectives of ground water recharge, water quality resource protection and thermal impacts control."

"Most rainfall events are much smaller than design storms used for urban drainage models. In any given area, most frequently recurrent rainfall events are small (less than 1 in. of daily rainfall)."

"Continuous simulation offers possibilities for designing and managing BMPs on an individual site-by-site basis that are not provided by other widely used simpler analysis methods. Therefore its application and use should be encouraged."

– US EPA Stormwater Best Management Practice Design Guide, Volume 1 – General Considerations, 2004

Design Methodology

Each Stormceptor system is sized using PCSWMM for Stormceptor, a continuous simulation model based on US EPA SWMM. The program calculates hydrology from up-to-date local historical rainfall data and specified site parameters. With US EPA SWMM's precision, every Stormceptor unit is designed to achieve a defined water quality objective.

The TSS removal data presented follows US EPA guidelines to reduce the average annual TSS load. Stormceptor's unit process for TSS removal is settling. The settling model calculates TSS removal by analyzing (summary of analysis presented in Appendix 2):

- Site parameters
- Continuous historical rainfall, including duration, distribution, peaks (Figure 1)
- Interevent periods
- Particle size distribution
- Particle settling velocities (Stokes Law, corrected for drag)
- TSS load (Figure 2)
- Detention time of the system

The Stormceptor System maintains continuous positive TSS removal for all influent flow rates. Figure 3 illustrates the continuous treatment by Stormceptor throughout the full range of storm events analyzed. It is clear that large events do not significantly impact the average annual TSS removal. There is no decline in cumulative TSS removal, indicating scour does not occur as the flow rate increases.







Figure 1. Runoff Volume by Flow Rate for BLUE HILL – MA 736, 1948 to 2005 for 6.14 ac, 56.2% **impervious.** Small frequent storm events represent the majority of annual rainfall volume. Large infrequent events have little impact on the average annual TSS removal, as they represent a small percentage of the total annual volume of runoff.



Figure 2. Long Term Pollutant Load by Flow Rate for BLUE HILL – 736, 1948 to 2005 for 6.14 ac, 56.2% impervious. The majority of the annual pollutant load is transported by small frequent storm





events. Conversely, large infrequent events carry an insignificant percentage of the total annual pollutant load.



Figure 3. Cumulative TSS Removal by Flow Rate for BLUE HILL – 736, 1948 to 2005. Stormceptor continuously removes TSS throughout the full range of storm events analyzed. Note that large events do not significantly impact the average annual TSS removal. Therefore no decline in cumulative TSS removal indicates scour does not occur as the flow rate increases.





Appendix 1 Stormceptor Design Summary

Project Information

-	
Date	6/10/2015
Project Name	Salmon ARCPUD
Project Number	8548
Location	Medwawy, MA

Designer Information

Company	Coneco Engineers & Scientist
Contact	N/A

Notes

N/A

Drainage Area

Total Area (ac)	6.14
Imperviousness (%)	56.2

The Stormceptor System model STC 4800 achieves the water quality objective removing 80% TSS for a Fine (organics, silts and sand) particle size distribution.

Rainfall

Name	BLUE HILL
State	MA
ID	736
Years of Records	1948 to 2005
Latitude	42°12'44"N
Longitude	71°6'53"W

Water Quality Objective

TSS Removal (%)	80

Upstream Storage

Storage	Discharge
(ac-ft)	(cfs)
0	0

Stormceptor Sizing Summary

Stormceptor Model	TSS Removal %
STC 450i	61
STC 900	71
STC 1200	71
STC 1800	71
STC 2400	76
STC 3600	76
STC 4800	80
STC 6000	81
STC 7200	84
STC 11000	87
STC 13000	88
STC 16000	89





Particle Size Distribution

Removing silt particles from runoff ensures that the majority of the pollutants, such as hydrocarbons and heavy metals that adhere to fine particles, are not discharged into our natural water courses. The table below lists the particle size distribution used to define the annual TSS removal.

Fine (organics, silts and sand)								
Particle Size	Distribution	Specific Gravity	Settling Velocity		Particle Size	Distribution	Specific Gravity	Settling Velocity
μm	%		ft/s		μm	%		ft/s
20 60 150 400 2000	20 20 20 20 20	1.3 1.8 2.2 2.65 2.65	0.0013 0.0051 0.0354 0.2123 0.9417					

Stormceptor Design Notes

- Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor.
- Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal.
- Only the STC 450i is adaptable to function with a catch basin inlet and/or inline pipes.
- Only the Stormceptor models STC 450i to STC 7200 may accommodate multiple inlet pipes.
- Inlet and outlet invert elevation differences are as follows:

Inlet and Outlet Pipe Invert Elevations Differences

Inlet Pipe Configuration	STC 450i	STC 900 to STC 7200	STC 11000 to STC 16000
Single inlet pipe	3 in.	1 in.	3 in.
Multiple inlet pipes	3 in.	3 in.	Only one inlet pipe.

- Design estimates are based on stable site conditions only, after construction is completed.
- Design estimates assume that the storm drain is not submerged during zero flows. For submerged applications, please contact your local Stormceptor representative.
- Design estimates may be modified for specific spills controls. Please contact your local Stormceptor representative for further assistance.
- For pricing inquiries or assistance, please contact Rinker Materials 1 (800) 909-7763 www.rinkerstormceptor.com





Appendix 2 Summary of Design Assumptions

SITE DETAILS

Site Drainage Area

onto Brannago / nou			
Total Area (ac)	6.14	Imperviousness (%)	56.2
Surface Characteristics		Infiltration Parameters	
Width (ft)	1034	Horton's equation is used to estimate in	nfiltration
Slope (%)	2	Max. Infiltration Rate (in/hr)	2.44
Impervious Depression Storage (in.)	0.02	Min. Infiltration Rate (in/hr)	0.4
Pervious Depression Storage (in.)	0.2	Decay Rate (s ⁻¹)	0.00055
Impervious Manning's n	0.015	Regeneration Rate (s^{-1})	0.01
Pervious Manning's n	0.25		
		Evaporation	
Maintenance Frequency		Daily Evaporation Rate (inches/day)	0.1
Sediment build-up reduces the storage volume for sedimentation. Frequency of maintenance is assumed for TSS removal calculations		Dry Weather Flow	-

Maintenance Frequency (months) 12

Upstream Attenuation

Stage-storage and stage-discharge relationship used to model attenuation upstream of the Stormceptor System is identified in the table below.

Storage ac-ft	Discharge cfs
0	0





PARTICLE SIZE DISTRIBUTION

Particle Size Distribution

Removing fine particles from runoff ensures the majority of pollutants, such as heavy metals, hydrocarbons, free oils and nutrients are not discharged into natural water resources. The table below identifies the particle size distribution selected to define TSS removal for the design of the Stormceptor System.

Fine (organics, silts and sand)								
Particle Size	Distribution	Specific Gravity	Settling Velocity		Particle Size	Distribution	Specific Gravity	Settling Velocity
μm	%		ft/s		μm	%		ft/s
20 60 150 400 2000	20 20 20 20 20	1.3 1.8 2.2 2.65 2.65	0.0013 0.0051 0.0354 0.2123 0.9417					



PCSWMM for Stormceptor Grain Size Distributions

Figure 1. PCSWMM for Stormceptor standard design grain size distributions.



TSS LOADING

TSS Loading Parameters

TSS Loading Function

Buildup / Washoff

Parameters

Target Event Mean Concentration (EMC) (mg/L)	125
Exponential Buildup Power	0.4
Exponential Washoff Exponential	0.2

HYDROLOGY ANALYSIS

PCSWMM for Stormceptor calculates annual hydrology with the US EPA SWMM and local continuous historical rainfall data. Performance calculations of the Stormceptor System are based on the average annual removal of TSS for the selected site parameters. The Stormceptor System is engineered to capture fine particles (silts and sands) by focusing on average annual runoff volume ensuring positive removal efficiency is maintained during all rainfall events, while preventing the opportunity for negative removal efficiency (scour).

Smaller recurring storms account for the majority of rainfall events and average annual runoff volume, as observed in the historical rainfall data analyses presented in this section.

Rainfall Station

Rainfall Station	BLUE HILL		
Rainfall File Name	MA736.NDC	Total Number of Events	9865
Latitude	42°12'44"N	Total Rainfall (in.)	2849.7
Longitude	71°6'53"W	Average Annual Rainfall (in.)	49.1
Elevation (ft)	630	Total Evaporation (in.)	147.7
Rainfall Period of Record (y)	58	Total Infiltration (in.)	1233.2
Total Rainfall Period (y)	58	Percentage of Rainfall that is Runoff (%)	53.0





Rainfall Event Analysis

Rainfall Depth	No. of Events	Percentage of Total Events	Total Volume	Percentage of Annual Volume
in.		%	in.	%
0.25	7098	72.0	431	15.1
0.50	1076	10.9	393	13.8
0.75	563	5.7	350	12.3
1.00	360	3.6	311	10.9
1.25	257	2.6	288	10.1
1.50	151	1.5	207	7.3
1.75	102	1.0	165	5.8
2.00	70	0.7	130	4.6
2.25	42	0.4	89	3.1
2.50	41	0.4	98	3.4
2.75	27	0.3	71	2.5
3.00	21	0.2	61	2.1
3.25	13	0.1	40	1.4
3.50	10	0.1	34	1.2
3.75	5	0.1	18	0.6
4.00	2	0.0	8	0.3
4.25	1	0.0	4	0.1
4.50	4	0.0	18	0.6
4.75	4	0.0	18	0.6
5.00	0	0.0	0	0.0
5.25	1	0.0	5	0.2
5.50	3	0.0	16	0.6
5.75	2	0.0	11	0.4
6.00	4	0.0	23	0.8
6.25	0	0.0	0	0.0
6.50	0	0.0	0	0.0
6.75	1	0.0	7	0.2
7.00	1	0.0	7	0.2
7.25	2	0.0	14	0.5
7.50	0	0.0	0	0.0
7.75	1	0.0	8	0.3
8.00	1	0.0	8	0.3
8.25	0	0.0	0	0.0
>8.25	2	0.0	17	0.6







Pollutograph

Flow Rate	Cumulative Mass
CTS	%
0.035	45.0
0.141	66.5
0.318	77.5
0.883	04.3 88.0
1 271	92.3
1.73	94.8
2.26	96.6
2.86	97.9
3.531	98.6
4.273	99.1
5.085	99.4
5.968	99.6
6.922	99.7
0.041	99.0
10 206	99.9
11 442	100.0
12.749	100.0
14.126	100.0
15.574	100.0
17.092	100.0
18.681	100.0
20.341	100.0
22.072	100.0
23.873	100.0
20.744	100.0
29.7	100.0
31.783	100.0

Cumulative Mass Transported by Flow Rate For area: 6.14 (ac), imperviousness: 56.2%, rainfall station: BLUE HILL 100-90 80 Annual Mass Transported (%) 70 60-50 40 30 20 10 0+ **FITT** 1.1.1 I I I 1 1 | []] 2.0 2.5 3.0 3.5 4.5 5.0 0.0 0.5 1.0 1.5 4.0 Flow (cfs)





Stormceptor Sizing Detailed Report PCSWMM for Stormceptor

Project Information

Date	6/10/2015
Project Name	Salmon ARCPUD
Project Number	8548
Location	Medwawy, MA

Stormwater Quality Objective

This report outlines how Stormceptor System can achieve a defined water quality objective through the removal of total suspended solids (TSS). Attached to this report is the Stormceptor Sizing Summary.

Stormceptor System Recommendation

The Stormceptor System model STC 900 achieves the water quality objective removing 82% TSS for a Fine (organics, silts and sand) particle size distribution.

The Stormceptor System

The Stormceptor oil and sediment separator is sized to treat stormwater runoff by removing pollutants through gravity separation and flotation. Stormceptor's patented design generates positive TSS removal for all rainfall events, including large storms. Significant levels of pollutants such as heavy metals, free oils and nutrients are prevented from entering natural water resources and the re-suspension of previously captured sediment (scour) does not occur.

Stormceptor provides a high level of TSS removal for small frequent storm events that represent the majority of annual rainfall volume and pollutant load. Positive treatment continues for large infrequent events, however, such events have little impact on the average annual TSS removal as they represent a small percentage of the total runoff volume and pollutant load.

Stormceptor is the only oil and sediment separator on the market sized to remove TSS for a wide range of particle sizes, including fine sediments (clays and silts), that are often overlooked in the design of other stormwater treatment devices.





Small storms dominate hydrologic activity, US EPA reports

"Early efforts in stormwater management focused on flood events ranging from the 2-yr to the 100-yr storm. Increasingly stormwater professionals have come to realize that small storms (i.e. < 1 in. rainfall) dominate watershed hydrologic parameters typically associated with water quality management issues and BMP design. These small storms are responsible for most annual urban runoff and groundwater recharge. Likewise, with the exception of eroded sediment, they are responsible for most pollutant washoff from urban surfaces. Therefore, the small storms are of most concern for the stormwater management objectives of ground water recharge, water quality resource protection and thermal impacts control."

"Most rainfall events are much smaller than design storms used for urban drainage models. In any given area, most frequently recurrent rainfall events are small (less than 1 in. of daily rainfall)."

"Continuous simulation offers possibilities for designing and managing BMPs on an individual site-by-site basis that are not provided by other widely used simpler analysis methods. Therefore its application and use should be encouraged."

– US EPA Stormwater Best Management Practice Design Guide, Volume 1 – General Considerations, 2004

Design Methodology

Each Stormceptor system is sized using PCSWMM for Stormceptor, a continuous simulation model based on US EPA SWMM. The program calculates hydrology from up-to-date local historical rainfall data and specified site parameters. With US EPA SWMM's precision, every Stormceptor unit is designed to achieve a defined water quality objective.

The TSS removal data presented follows US EPA guidelines to reduce the average annual TSS load. Stormceptor's unit process for TSS removal is settling. The settling model calculates TSS removal by analyzing (summary of analysis presented in Appendix 2):

- Site parameters
- Continuous historical rainfall, including duration, distribution, peaks (Figure 1)
- Interevent periods
- Particle size distribution
- Particle settling velocities (Stokes Law, corrected for drag)
- TSS load (Figure 2)
- Detention time of the system

The Stormceptor System maintains continuous positive TSS removal for all influent flow rates. Figure 3 illustrates the continuous treatment by Stormceptor throughout the full range of storm events analyzed. It is clear that large events do not significantly impact the average annual TSS removal. There is no decline in cumulative TSS removal, indicating scour does not occur as the flow rate increases.







Figure 1. Runoff Volume by Flow Rate for BLUE HILL – MA 736, 1948 to 2005 for 2.81 ac, 50.2% impervious. Small frequent storm events represent the majority of annual rainfall volume. Large infrequent events have little impact on the average annual TSS removal, as they represent a small percentage of the total annual volume of runoff.



Figure 2. Long Term Pollutant Load by Flow Rate for BLUE HILL – 736, 1948 to 2005 for 2.81 ac, 50.2% impervious. The majority of the annual pollutant load is transported by small frequent storm





events. Conversely, large infrequent events carry an insignificant percentage of the total annual pollutant load.



Figure 3. Cumulative TSS Removal by Flow Rate for BLUE HILL – 736, 1948 to 2005. Stormceptor continuously removes TSS throughout the full range of storm events analyzed. Note that large events do not significantly impact the average annual TSS removal. Therefore no decline in cumulative TSS removal indicates scour does not occur as the flow rate increases.





Appendix 1 Stormceptor Design Summary

Project Information

-	
Date	6/10/2015
Project Name	Salmon ARCPUD
Project Number	8548
Location	Medwawy, MA

Designer Information

Company	Coneco Engineers & Scientist
Contact	N/A

Notes

N/A

Drainage Area

Total Area (ac)	2.81
Imperviousness (%)	50.2

The Stormceptor System model STC 900 achieves the water quality objective removing 82% TSS for a Fine (organics, silts and sand) particle size distribution.

Rainfall

Name	BLUE HILL
State	MA
ID	736
Years of Records	1948 to 2005
Latitude	42°12'44"N
Longitude	71°6'53"W

Water Quality Objective

TSS Removal (%)	80

Upstream Storage

•	
Storage	Discharge
(ac-ft)	(cfs)
0	0

Stormceptor Sizing Summary

Stormceptor Model	TSS Removal %		
STC 450i	73		
STC 900	82		
STC 1200	82		
STC 1800	81		
STC 2400	85		
STC 3600	86		
STC 4800	89		
STC 6000	89		
STC 7200	91		
STC 11000	93		
STC 13000	93		
STC 16000	94		





Particle Size Distribution

Removing silt particles from runoff ensures that the majority of the pollutants, such as hydrocarbons and heavy metals that adhere to fine particles, are not discharged into our natural water courses. The table below lists the particle size distribution used to define the annual TSS removal.

Fine (organics, silts and sand)								
Particle Size	Distribution	Specific Gravity	Settling Velocity		Particle Size	Distribution	Specific Gravity	Settling Velocity
μm	%		ft/s		μm	%		ft/s
20 60 150 400 2000	20 20 20 20 20	1.3 1.8 2.2 2.65 2.65	0.0013 0.0051 0.0354 0.2123 0.9417					

Stormceptor Design Notes

- Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor.
- Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal.
- Only the STC 450i is adaptable to function with a catch basin inlet and/or inline pipes.
- Only the Stormceptor models STC 450i to STC 7200 may accommodate multiple inlet pipes.
- Inlet and outlet invert elevation differences are as follows:

Inlet and Outlet Pipe Invert Elevations Differences

Inlet Pipe Configuration	STC 450i	STC 900 to STC 7200	STC 11000 to STC 16000
Single inlet pipe	3 in.	1 in.	3 in.
Multiple inlet pipes	3 in.	3 in.	Only one inlet pipe.

- Design estimates are based on stable site conditions only, after construction is completed.
- Design estimates assume that the storm drain is not submerged during zero flows. For submerged applications, please contact your local Stormceptor representative.
- Design estimates may be modified for specific spills controls. Please contact your local Stormceptor representative for further assistance.
- For pricing inquiries or assistance, please contact Rinker Materials 1 (800) 909-7763 www.rinkerstormceptor.com





Appendix 2 **Summary of Design Assumptions**

SITE DETAILS

Site Drainage Area

2.81	Imperviousness (%)	50.2
	Infiltration Parameters	
700	Horton's equation is used to estimate in	nfiltration
2	Max. Infiltration Rate (in/hr)	2.44
0.02	Min. Infiltration Rate (in/hr)	0.4
0.2	Decay Rate (s ⁻¹)	
0.015	Regeneration Rate (s^{-1})	0.01
0.25		
	Evaporation	
	Daily Evaporation Rate (inches/day)	0.1
Sediment build-up reduces the storage volume for sedimentation. Frequency of maintenance is assumed for TSS removal calculations		-
	2.81 700 2 0.02 0.2 0.015 0.25	2.81 Imperviousness (%) Infiltration Parameters 700 Horton's equation is used to estimate in 2 Max. Infiltration Rate (in/hr) 0.02 Min. Infiltration Rate (in/hr) 0.2 Decay Rate (s ⁻¹) 0.015 Regeneration Rate (s ⁻¹) 0.25 Evaporation Daily Evaporation Rate (inches/day) volume for nee is Dry Weather Flow

Maintenance Frequency (months) 12

Dry Weather Flow (cfs)	No
------------------------	----

Upstream Attenuation

Stage-storage and stage-discharge relationship used to model attenuation upstream of the Stormceptor System is identified in the table below.

Storage ac-ft	Discharge cfs
0	0





PARTICLE SIZE DISTRIBUTION

Particle Size Distribution

Removing fine particles from runoff ensures the majority of pollutants, such as heavy metals, hydrocarbons, free oils and nutrients are not discharged into natural water resources. The table below identifies the particle size distribution selected to define TSS removal for the design of the Stormceptor System.

Fine (organics, silts and sand)								
Particle Size	Distribution	Specific Gravity	Settling Velocity		Particle Size	Distribution	Specific Gravity	Settling Velocity
μm	%		ft/s		μm	%		ft/s
20 60 150 400 2000	20 20 20 20 20	1.3 1.8 2.2 2.65 2.65	0.0013 0.0051 0.0354 0.2123 0.9417					



PCSWMM for Stormceptor Grain Size Distributions

Figure 1. PCSWMM for Stormceptor standard design grain size distributions.



TSS LOADING

TSS Loading Parameters

TSS Loading Function

Buildup / Washoff

Parameters

Target Event Mean Concentration (EMC) (mg/L)	125
Exponential Buildup Power	0.4
Exponential Washoff Exponential	0.2

HYDROLOGY ANALYSIS

PCSWMM for Stormceptor calculates annual hydrology with the US EPA SWMM and local continuous historical rainfall data. Performance calculations of the Stormceptor System are based on the average annual removal of TSS for the selected site parameters. The Stormceptor System is engineered to capture fine particles (silts and sands) by focusing on average annual runoff volume ensuring positive removal efficiency is maintained during all rainfall events, while preventing the opportunity for negative removal efficiency (scour).

Smaller recurring storms account for the majority of rainfall events and average annual runoff volume, as observed in the historical rainfall data analyses presented in this section.

Rainfall Station

Rainfall Station	BLUE HILL		
Rainfall File Name	MA736.NDC	Total Number of Events	9865
Latitude	42°12'44"N	Total Rainfall (in.)	2849.7
Longitude	71°6'53"W	Average Annual Rainfall (in.)	49.1
Elevation (ft)	630	Total Evaporation (in.)	129.6
Rainfall Period of Record (y)	58	Total Infiltration (in.)	1401.3
Total Rainfall Period (y)	58	Percentage of Rainfall that is Runoff (%)	47.9





Rainfall Event Analysis

Rainfall Depth	No. of Events	Percentage of Total Events	Total Volume	Percentage of Annual Volume
in.		%	in.	%
0.25	7098	72.0	431	15.1
0.50	1076	10.9	393	13.8
0.75	563	5.7	350	12.3
1.00	360	3.6	311	10.9
1.25	257	2.6	288	10.1
1.50	151	1.5	207	7.3
1.75	102	1.0	165	5.8
2.00	70	0.7	130	4.6
2.25	42	0.4	89	3.1
2.50	41	0.4	98	3.4
2.75	27	0.3	71	2.5
3.00	21	0.2	61	2.1
3.25	13	0.1	40	1.4
3.50	10	0.1	34	1.2
3.75	5	0.1	18	0.6
4.00	2	0.0	8	0.3
4.25	1	0.0	4	0.1
4.50	4	0.0	18	0.6
4.75	4	0.0	18	0.6
5.00	0	0.0	0	0.0
5.25	1	0.0	5	0.2
5.50	3	0.0	16	0.6
5.75	2	0.0	11	0.4
6.00	4	0.0	23	0.8
6.25	0	0.0	0	0.0
6.50	0	0.0	0	0.0
6.75	1	0.0	7	0.2
7.00	1	0.0	7	0.2
7.25	2	0.0	14	0.5
7.50	0	0.0	0	0.0
7.75	1	0.0	8	0.3
8.00	1	0.0	8	0.3
8.25	0	0.0	0	0.0
>8.25	2	0.0	17	0.6







Pollutograph

Flow Rate	Cumulative Mass
CIS	70
0.035	61.7
0.141	79.2
0.318	88.0
0.505	95.4
1 271	98.4
1.73	99.2
2.26	99.6
2.86	99.7
3.531	99.9
4.273	99.9
5.085	100.0
5.968	100.0
6.922	100.0
7.946	100.0
9.041	100.0
10.206	100.0
11.442	100.0
14 126	100.0
15 574	100.0
17.092	100.0
18.681	100.0
20.341	100.0
22.072	100.0
23.873	100.0
25.744	100.0
27.687	100.0
29.7	100.0
31.783	100.0





Stormceptor® Owner's Manual



Stormceptor is protected by one or more of the following patents:

Canadian Patent No. 2,137,942 Canadian Patent No. 2,175,277 Canadian Patent No. 2,180,305 Canadian Patent No. 2,180,383 Canadian Patent No. 2,206,338 Canadian Patent No. 2,327,768 U.S. Patent No. 5,753,115 U.S. Patent No. 5,849,181 U.S. Patent No. 6,068,765 U.S. Patent No. 6,371,690 U.S. Patent No. 7,582,216 U.S. Patent No. 7,666,303 Australia Patent No. 693.164 Australia Patent No. 707,133 Australia Patent No. 729,096 Australia Patent No. 779,401 Australia Patent No. 2008,279,378 Australia Patent No. 2008,288,900 Indonesia Patent No. 0007058 Japan Patent No. 3581233 Japan Patent No. 9-11476 Korean Patent No. 0519212 Malaysia Patent No. 118987 New Zealand Patent No. 314,646 New Zealand Patent No. 583,008 New Zealand Patent No. 583,583 South African Patent No. 2010/00682 South African Patent No. 2010/01796 Other Patents Pending

Table of Contents

- 1 Stormceptor Overview
- 2 Stormceptor Operation & Components
- 3 Stormceptor Identification
- 4 Stormceptor Inspection & Maintenance Recommended Stormceptor Inspection Procedure Recommended Stormceptor Maintenance Procedure
- 5 Contact Information (Stormceptor Licensees)

Congratulations!

Your selection of a Stormceptor[®] means that you have chosen the most recognized and efficient stormwater oil/sediment separator available for protecting the environment. Stormceptor is a pollution control device often referred to as a "Hydrodynamic Separator (HDS)" or an "Oil Grit Separator (OGS)", engineered to remove and retain pollutants from stormwater runoff to protect our lakes, rivers and streams from the harmful effects of non-point source pollution.

1 – Stormceptor Overview

Stormceptor is a patented stormwater quality structure most often utilized as a treatment component of the underground storm drain network for stormwater pollution prevention. Stormceptor is designed to remove sediment, total suspended solids (TSS), other pollutants attached to sediment, hydrocarbons and free oil from stormwater runoff. Collectively the Stormceptor provides spill protection and prevents non-point source pollution from entering downstream waterways.

Key benefits of Stormceptor include:

- Removes sediment, suspended solids, debris, nutrients, heavy metals, and hydrocarbons (oil and grease) from runoff and snowmelt.
- Will not scour or re-suspend trapped pollutants.
- Provides sediment and oil storage.
- Provides spill control for accidents, commercial and industrial developments.
- · Easy to inspect and maintain (vacuum truck).
- "STORMCEPTOR" is clearly marked on the access cover (excluding inlet designs).
- Relatively small footprint.
- 3rd Party tested and independently verified.
- Dedicated team of experts available to provide support.

Model Types:

- STC (Standard)
- STF (Fiberglass)
- EOS (Extended Oil Storage)
- OSR (Oil and Sand Removal)
- MAX (Custom designed unit, specific to site)

Configuration Types:

- Inlet unit (accommodates inlet flow entry, and multi-pipe entry)
- In-Line (accommodates multi-pipe entry)
- Submerged Unit (accommodates the site's tailwater conditions)
- Series Unit (combines treatment in two systems)
Please Maintain Your Stormceptor

To ensure long-term environmental protection through continued performance as originally designed for your site, **Stormceptor must be maintained**, as any stormwater treatment practice does. The need for maintenance is determined through inspection of the Stormceptor. Procedures for inspection are provided within this document. Maintenance of the Stormceptor is performed from the surface via vacuum truck.

If you require information about Stormceptor, or assistance in finding resources to facilitate inspections or maintenance of your Stormceptor please call your local Stormceptor Licensee or Imbrium[®] Systems.

2 – Stormceptor Operation & Components

Stormceptor is a flexibly designed underground stormwater quality treatment device that is unparalleled in its effectiveness for pollutant capture and retention using patented flow separation technology.

Stormceptor creates a non-turbulent treatment environment below the insert platform within the system. The insert diverts water into the lower chamber, allowing free oils and debris to rise, and sediment to settle under relatively low velocity conditions. These pollutants are trapped and stored below the insert and protected from large runoff events for later removal during the maintenance procedure.

With thousands of units operating worldwide, Stormceptor delivers reliable protection every day, in every storm. The patented Stormceptor design prohibits the scour and release of captured pollutants, ensuring superior water quality treatment and protection during even the most extreme storm events. Stormceptor's proven performance is backed by the longest record of lab and field verification in the industry.

Stormceptor Schematic and Component Functions

Below are schematics of two common Stormceptor configurations with key components identified and their functions briefly described.



- Manhole access cover provides access to the subsurface components
- Precast reinforced concrete structure provides the vessel's watertight structural support
- Fiberglass insert separates vessel into upper and lower chambers
- Weir directs incoming stormwater and oil spills into the lower chamber
- Orifice plate prevents scour of accumulated pollutants
- Inlet drop tee conveys stormwater into the lower chamber
- Fiberglass skirt provides double-wall containment of hydrocarbons
- Outlet riser pipe conveys treated water to the upper chamber; primary vacuum line access port for sediment removal
- Oil inspection port primary access for measuring oil depth and oil removal
- Safety grate safety measure to cover riser pipe in the event of manned entry into vessel

3 – Stormceptor Identification

Stormceptor is available in both precast concrete and fiberglass vessels, with precast concrete often being the dominant material of construction.

In the Stormceptor, a patented, engineered fiberglass insert separates the structure into an upper chamber and lower chamber. The lower chamber will remain full of water, as this is where the pollutants are sequestered for later removal. Multiple Stormceptor model (STC, OSR, EOS, MAX and STF) configurations exist, each to be inspected and maintained in a similar fashion.

Each unit is easily identifiable as a Stormceptor by the trade name "Stormceptor" embossed on each access cover at the surface. To determine the location of "inlet" Stormceptor units with horizontal catch basin inlet, look down into the grate as the Stormceptor insert will be visible. The name "Stormceptor" is not embossed on inlet models due to the variability of inlet grates used/ approved across North America.

⁶ Stormceptor® Owner's Manual

Once the location of the Stormceptor is determined, the model number may be identified by comparing the measured depth from the fiberglass insert level at the outlet pipe's invert (water level) to the bottom of the tank using **Table 1**.

In addition, starting in 1996 a metal serial number tag containing the model number has been affixed to the inside of the unit, on the fiberglass insert. If the unit does not have a serial number, or if there is any uncertainty regarding the size of the unit using depth measurements, please contact your local Stormceptor Representative for assistance.

Sizes/Models

Typical general dimensions and capacities of the standard precast STC, EOS & OSR Stormceptor models in both USA and Canada/International (excluding South East Asia and Australia) are provided in **Tables 1 and 2**. Typical rim to invert measurements are provided later in this document. The total depth for cleaning will be the sum of the depth from outlet pipe invert (generally the water level) to rim (grade) and the depth from outlet pipe invert to the precast bottom of the unit. Note that depths and capacities may vary slightly between regions.

STC Model	Insert to Base (in.)	EOS Model	Insert to Base (in.)	OSR Model	Insert to Base (in.)	Typical STF m (in.)
450	60	4-175	60	65	60	1.5 (60)
900	55	9-365	55	140	55	1.5 (61)
1200	71	12-590	71			1.8 (73)
1800	105	18-1000	105			2.9 (115)
2400	94	24-1400	94	250	94	2.3 (89)
3600	134	36-1700	134			3.2 (127)
4800	128	48-2000	128	390	128	2.9 (113)
6000	150	60-2500	150			3.5 (138)
7200	134	72-3400	134	560	134	3.3 (128)
11000*	128	110-5000*	128	780*	128	
13000*	150	130-6000*	150			
16000*	134	160-7800*	134	1125*	134	

Table 1A. (US)	Stormceptor	Dimensions -	Insert to	Base of	Structure
----------------	-------------	---------------------	-----------	---------	-----------

Notes:

1. Depth Below Pipe Inlet Invert to the Bottom of Base Slab can vary slightly by manufacturing facility, and can be modified to accommodate specific site designs, pollutant loads or site conditions. Contact your local representative for assistance.

*Consist of two chamber structures in series.

STC Model	Insert to Base (m)	EOS Model	Insert to Base (m)	OSR Model	Insert to Base (m)	Typical STF m (in.)
300	1.5	300	1.5	300	1.7	1.5 (60)
750	1.5	750	1.5	750	1.6	1.5 (61)
1000	1.8	1000	1.8			1.8 (73)
1500	2.8					2.9 (115)
2000	2.8	2000	2.8	2000	2.6	2.3 (89)
3000	3.7	3000	3.7			3.2 (127)
4000	3.4	4000	3.4	4000	3.6	2.9 (113)
5000	4.0	5000	4.0			3.5 (138)
6000	3.7	6000	3.7	6000	3.7	3.3 (128)
9000*	3.4	9000*	3.4	9000*	3.6	
11000*	4.0	10000*	4.0			
14000*	3.7	14000*	3.7	14000*	3.7	

Table 1B. (CA & Int'l) Stormceptor Dimensions – Insert to Base of Structure

Notes:

1. Depth Below Pipe Inlet Invert to the Bottom of Base Slab can vary slightly by manufacturing facility, and can be modified to accommodate specific site designs, pollutant loads or site conditions. Contact your local representative for assistance.

*Consist of two chamber structures in series.

Table 2A. (US) Storage Capacities

STC Model	Hydrocarbon Storage Capacity	Sediment Capacity	EOS Model	Hydrocarbon Storage Capacity	OSR Model	Hydrocarbon Storage Capacity	Sediment Capacity
	gal	ft ³		gal		gal	ft ³
450	86	46	4-175	175	065	115	46
900	251	89	9-365	365	140	233	58
1200	251	127	12-590	591			
1800	251	207	18-1000	1198			
2400	840	205	24-1400	1457	250	792	156
3600	840	373	36-1700	1773			
4800	909	543	48-2000	2005	390	1233	465
6000	909	687	60-2500	2514			
7200	1059	839	72-3400	3418	560	1384	690
11000*	2797	1089	110-5000*	5023	780*	2430	930
13000*	2797	1374	130-6000*	6041			
16000*	3055	1677	160-7800*	7850	1125*	2689	1378

Notes:

1. Hydrocarbon & Sediment capacities can be modified to accommodate specific site design requirements, contact your local representative for assistance.

*Consist of two chamber structures in series.

STC Model	Hydrocarbon Storage Capacity	Sediment Capacity	EOS Model Hydrocarbon Storage Capacity		OSR Model	Hydrocarbon Storage Capacity	Sediment Capacity
		L		L			L .
300	300	1450	300	662	300	300	1500
750	915	3000	750	1380	750	900	3000
1000	915	3800	1000	2235			
1500	915	6205					
2000	2890	7700	2000	5515	2000	2790	7700
3000	2890	11965	3000	6710			
4000	3360	16490	4000	7585	4000	4700	22200
5000	3360	20940	5000	9515			
6000	3930	26945	6000	12940	6000	5200	26900
9000*	10555	32980	9000*	19010	9000*	9300	33000
11000*	10555	37415	10000*	22865			
14000*	11700	53890	14000*	29715	14000*	10500	53900

Table 2B. (CA & Int'l) Storage Capacities

Notes:

1. Hydrocarbon & Sediment capacities can be modified to accommodate specific site design requirements, contact your local representative for assistance.

*Consist of two chamber structures in series.

4 – Stormceptor Inspection & Maintenance

Regular inspection and maintenance is a proven, cost-effective way to maximize water resource protection for all stormwater pollution control practices, and is required to insure proper functioning of the Stormceptor. Both inspection and maintenance of the Stormceptor is easily performed from the surface. Stormceptor's patented technology has no moving parts, simplifying the inspection and maintenance process.

Please refer to the following information and guidelines before conducting inspection and maintenance activities.

When is inspection needed?

- Post-construction inspection is required prior to putting the Stormceptor into service.
- Routine inspections are recommended during the first year of operation to accurately assess the sediment accumulation.
- Inspection frequency in subsequent years is based on the maintenance plan developed in the first year.
- Inspections should also be performed immediately after oil, fuel, or other chemical spills.

When is maintenance cleaning needed?

 For optimum performance, the unit should be cleaned out once the sediment depth reaches the recommended maintenance sediment depth, which is approximately 15% of the unit's total storage capacity (see **Table 2**). The frequency should be adjusted based on historical inspection results due to variable site pollutant loading.

- Sediment removal is easier when removed on a regular basis at or prior to the recommended maintenance sediment depths, as sediment build-up can compact making removal more difficult.
- The unit should be cleaned out immediately after an oil, fuel or chemical spill.

What conditions can compromise Stormceptor performance?

- If construction sediment and debris is not removed prior to activating the Stormceptor unit, maintenance frequency may be reduced.
- If the system is not maintained regularly and fills with sediment and debris beyond the capacity as indicated in **Table 2**, pollutant removal efficiency may be reduced.
- If an oil spill(s) exceeds the oil capacity of the system, subsequent spills may not be captured.
- If debris clogs the inlet of the system, removal efficiency of sediment and hydrocarbons may be reduced.
- If a downstream blockage occurs, a backwater condition may occur for the Stormceptor and removal efficiency of sediment and hydrocarbons may be reduced.

What training is required?

The Stormceptor is to be inspected and maintained by professional vacuum cleaning service providers with experience in the maintenance of underground tanks, sewers and catch basins. For typical inspection and maintenance activities, no specific supplemental training is required for the Stormceptor. Information provided within this Manual (provided to the site owner) contains sufficient guidance to maintain the system properly.

In unusual circumstances, such as if a damaged component needs replacement or some other condition requires manned entry into the vessel, confined space entry procedures must be followed. Only professional maintenance service providers trained in these procedures should enter the vessel. Service provider companies typically have personnel who are trained and certified in confined space entry procedures according to local, state, and federal standards.

What equipment is typically required for inspection?

- Manhole access cover lifting tool
- Oil dipstick / Sediment probe with ball valve (typically ³/₄-inch to 1-inch diameter)
- Flashlight
- Camera
- Data log / Inspection Report
- · Safety cones and caution tape
- · Hard hat, safety shoes, safety glasses, and chemical-resistant gloves

Recommended Stormceptor Inspection Procedure:

- Stormceptor is to be inspected from grade through a standard surface manhole access cover.
- Sediment and oil depth inspections are performed with a sediment probe and oil dipstick.
- Oil depth is measured through the oil inspection port, either a 4-inch (100 mm) or 6-inch (150 mm) diameter port.
- Sediment depth can be measured through the oil inspection port or the 24-inch (610 mm) diameter outlet riser pipe.
- Inspections also involve a visual inspection of the internal components of the system.



Figure 4.



What equipment is typically required for maintenance?

- · Vacuum truck equipped with water hose and jet nozzle
- Small pump and tubing for oil removal
- Manhole access cover lifting tool
- Oil dipstick / Sediment probe with ball valve (typically ³/₄-inch to 1-inch diameter)
- Flashlight
- Camera
- Data log / Inspection Report
- Safety cones
- Hard hats, safety shoes, safety glasses, chemical-resistant gloves, and hearing protection for service providers
- Gas analyzer, respiratory gear, and safety harness for specially trained personnel if confined space entry is required

Recommended Stormceptor Maintenance Procedure

Maintenance of Stormceptor is performed using a vacuum truck.

No entry into the unit is required for maintenance. **DO NOT ENTER THE STORMCEPTOR CHAMBER** unless you have the proper personal safety equipment, have been trained and are qualified to enter a confined space, as identified by local Occupational Safety and Health Regulations (e.g. 29 CFR 1910.146 or Canada Occupational Safety and Health Regulations – SOR/86-304). Without the proper equipment, training and permit, entry into confined spaces can result in serious bodily harm and potentially death. Consult local, provincial, and/or state regulations to determine the requirements for confined space entry. Be aware, and take precaution that the Stormceptor fiberglass insert may be slippery. In addition, be aware that some units do not have a safety grate to cover the outlet riser pipe that leads to the submerged, lower chamber.

- Ideally maintenance should be conducted during dry weather conditions when no flow is entering the unit.
- Stormceptor is to be maintained through a standard surface manhole access cover.
- Insert the oil dipstick into the oil inspection port. If oil is present, pump off the oil layer into separate containment using a small pump and tubing.
- Maintenance cleaning of accumulated sediment is performed with a vacuum truck.
 - For 6-ft (1800 mm) diameter models and larger, the vacuum hose is inserted into the lower chamber via the 24-inch (610 mm) outlet riser pipe.
 - For 4-ft (1200 mm) diameter model, the removable drop tee is lifted out, and the vacuum hose is inserted into the lower chamber via the 12-inch (305 mm) drop tee hole.



- Using the vacuum hose, decant the water from the lower chamber into a separate containment tank or to the sanitary sewer, if permitted by the local regulating authority.
- Remove the sediment sludge from the bottom of the unit using the vacuum hose. For large Stormceptor units, a flexible hose is often connected to the primary vacuum line for ease of movement in the lower chamber.
- Units that have not been maintained regularly, have surpassed the maximum recommended sediment capacity, or contain damaged components may require manned entry by trained personnel using safe and proper confined space entry procedures.

A maintenance worker stationed at the above ground surface uses a vacuum hose to evacuate water, sediment, and debris from the system.

What is required for proper disposal?

The requirements for the disposal of material removed from Stormceptor units are similar to that of any other stormwater treatment Best Management Practices (BMP). Local guidelines should be consulted prior to disposal of the separator contents. In most areas the sediment, once dewatered, can be disposed of in a sanitary landfill. It is not anticipated that the sediment would be classified as hazardous waste. This could be site and pollutant dependent. In some cases, approval from the disposal facility operator/agency may be required.

What about oil spills?

Stormceptor is often implemented in areas where there is high potential for oil, fuel or other hydrocarbon or chemical spills. Stormceptor units should be cleaned immediately after a spill occurs by a licensed liquid waste hauler. You should also notify the appropriate regulatory agencies as required in the event of a spill.

What if I see an oil rainbow or sheen at the Stormceptor outlet?

With a steady influx of water with high concentrations of oil, a sheen may be noticeable at the Stormceptor outlet. This may occur because a hydrocarbon rainbow or sheen can be seen at

very small oil concentrations (< 10 ppm). Stormceptor is effective at removing 95% of free oil, and the appearance of a sheen at the outlet with high influent oil concentrations does not mean that the unit is not working to this level of removal. In addition, if the influent oil is emulsified, the Stormceptor will not be able to remove it. The Stormceptor is designed for free oil removal and not emulsified or dissolved oil conditions.

What factors affect the costs involved with inspection/maintenance?

The Vacuum Service Industry for stormwater drainage and sewer systems is a well-established sector of the service industry that cleans underground tanks, sewers and catch basins. Costs to clean Stormceptor units will vary. Inspection and maintenance costs are most often based on unit size, the number of units on a site, sediment/oil/hazardous material loads, transportation distances, tipping fees, disposal requirements and other local regulations.

What factors predict maintenance frequency?

Maintenance frequency will vary with the amount of pollution on your site (number of hydrocarbon spills, amount of sediment, site activity and use, etc.). It is recommended that the frequency of maintenance be increased or reduced based on local conditions. If the sediment load is high from an unstable site or sediment loads transported from upstream catchments, maintenance may be required semi-annually. Conversely once a site has stabilized, maintenance may be required less frequently (for example: two to seven year, site and situation dependent). Maintenance should be performed immediately after an oil spill or once the sediment depth in Stormceptor reaches the value specified in **Table 3** based on the unit size.

STC Model	Maintenance Sediment depth (in)	EOS Model	Maintenance Sediment depth (in)	Oil Storage Depth (in)	OSR Model	Maintenance Sediment depth (in)
450	8	4-175	9	24	065	8
900	8	9-365	9	24	140	8
1200	10	12-590	11	39		
1800	15					
2400	12	24-1400	14	68	250	12
3600	17	36-1700	19	79		
4800	15	48-2000	16	68	390	17
6000	18	60-2500	20	79		
7200	15	72-3400	17	79	560	17
11000*	17	110-5000*	16	68	780*	17
13000*	20	130-6000*	20	79		
16000*	17	160-7800*	17	79	1125*	17

Table 3A. (US) Recommended Sediment Depths Indicating Maintenance

Note:

1. The values above are for typical standard units.

*Per structure.

STC Model	Maintenance Sediment depth (mm)	EOS Model	Maintenance Sediment depth (mm)	Oil Storage Depth (mm)	OSR Model	Maintenance Sediment depth (mm)
300	225	300	225	610	300	200
750	230	750	230	610	750	200
1000	275	1000	275	990		
1500	400					
2000	350	2000	350	1727	2000	300
3000	475	3000	475	2006		
4000	400	4000	400	1727	4000	375
5000	500	5000	500	2006		
6000	425	6000	425	2006	6000	375
9000*	400	9000*	400	1727	9000*	425
11000*	500	10000*	500	2006		
14000*	425	14000*	425	2006	14000*	425

Table 3B. (CA & Int'l) Recommended Sediment Depths Indicating Maintenance

Note:

1. The values above are for typical standard units.

*Per structure.

Replacement parts

Since there are no moving parts during operation in a Stormceptor, broken, damaged, or worn parts are not typically encountered. Therefore, inspection and maintenance activities are generally focused on pollutant removal. However, if replacements parts are necessary, they may be purchased by contacting your local Stormceptor Representative, or Imbrium Systems.

The benefits of regular inspection and maintenance are many – from ensuring maximum operation efficiency, to keeping maintenance costs low, to the continued protection of natural waterways – and provide the key to Stormceptor's long and effective service life.

Stormceptor Inspection and Maintenance Log

Stormceptor Model No:				
Allowable Sediment Depth:				
Serial Number:				
Installation Date:				
Location Description of Unit:				
Other Comments:				

Contact Information

Questions regarding the Stormceptor can be addressed by contacting your area Stormceptor Licensee, Imbrium Systems, or visit our website at www.stormceptor.com.

Stormceptor Licensees:

CANADA

Lafarge Canada Inc. www.lafargepipe.com 403-292-9502 / 1-888-422-4022 780-468-5910 204-958-6348	Calgary, AB Edmonton, AB Winnipeg, MB, NW. ON, SK
Langley Concrete Group www.langleyconcretegroup.com 604-502-5236	BC
Hanson Pipe & Precast Inc. www.hansonpipeandprecast.com 519-622-7574 / 1-888-888-3222	ON
Lécuyer et Fils Ltée. www.lecuyerbeton.com 450-454-3928 / 1-800-561-0970	QC
Strescon Limited www.strescon.com 902-494-7400 506-633-8877	NS, NF NB, PE

UNITED STATES

Rinker Materials www.rinkerstormceptor.com 1-800-909-7763

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STORMWATER MANAGEMENT REPORT VOLUME II

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> JUNE 12, 2015 Revised: October 13, 2015

APPENDIX J

INFILTRATION TRENCH SIZING



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Area Listing (selected nodes)

	Area	CN	Description
(a	acres)		(subcatchment-numbers)
	5.519	98	Roofs, HSG A (1BW, 1LP, 2BW, 2LP, 2WS, 3BW, 3LP, 4BW, 4LP, 4WS, 5BW, 5LP, 6BW, 6LP, 6WS, 7LP, 8LP, 10WS, 12WP, 12WS, 14WP, 14WS, 16WP, 16WS, 18WP, 18WS, 19WP, 20WP, 20WS, 21WP, 22WP, 22WS, 23WP, 24WS, 25WP, 26WS, 27WP, 28WS, 29WP, 30WS, 31WP, 33WP, 88S, CEC, CWC, ILC, ILE, ILW, NC)
;	5.519	98	TOTAL AREA

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Soil Listing (selected nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
5.519	HSG A	1BW, 1LP, 2BW, 2LP, 2WS, 3BW, 3LP, 4BW, 4LP, 4WS, 5BW, 5LP, 6BW, 6LP, 6WS, 7LP, 8LP, 10WS, 12WP, 12WS, 14WP, 14WS, 16WP, 16WS, 18WP, 18WS, 19WP, 20WP, 20WS, 21WP, 22WP, 22WS, 23WP, 24WS, 25WP, 26WS, 27WP, 28WS, 29WP, 30WS, 31WP, 33WP, 88S, CEC, CWC, ILC, ILE, ILW, NC
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
0.000	Other	
5.519		TOTAL AREA

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 HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
HSG-A (acres) 5.519	HSG-B (acres) 0.000	HSG-C (acres) 0.000	HSG-D (acres) 0.000	Other (acres) 0.000	l otal (acres) 5.519	Ground Cover Roofs	Subcatchment Numbers 1BW, 1LP, 2BW, 2LP, 2WS, 3BW, 3LP, 4BW, 4LP, 4WS, 5BW, 5LP, 6BW, 6LP, 6WS, 7LP, 8LP, 10WS, 12WP, 12WS, 14WP, 14WS, 16WP, 16WS, 18WP, 18WS, 19WP, 20WP, 20WS, 21WP, 22WP, 22WS, 23WP, 22WS, 23WP, 24WS, 25WP, 26WS, 27WP, 28WS, 29WP, 30WS,
5.519	0.000	0.000	0.000	0.000	5.519	TOTAL	CEC, CWC, ILC, ILE, ILW, NC
						AREA	

Ground Covers (selected nodes)

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1BW:1BW	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.17 cfs 0.013 af
Subcatchment1LP:1 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment2BW: 2 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 2LP: 2 LP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.17 cfs 0.013 af
Subcatchment 2WS: 2 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment3BW: 3 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment3LP: 3 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment4BW: 4 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 4LP: 4 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 4WS: 4 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment5BW: 5 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment5LP: 5LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment6BW: 6 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 6LP: 6 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment6WS: 6 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment7LP: 7 LP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.17 cfs 0.013 af

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Subcatchment 8LP: 8 LP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.22 cfs 0.016 af
Subcatchment 10WS: 10 WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.17 cfs 0.013 af
Subcatchment 12WP: 12 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 12WS: 12 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment14WP:14 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment14WS:14 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 16WP: 16 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 16WS: 16 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 18WP: 18 WP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.22 cfs 0.016 af
Subcatchment 18WS: 18 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 19WP: 19 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 20WP: 20 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 20WS: 20 WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.17 cfs 0.013 af
Subcatchment 21WP: 21 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 22WP: 22 WP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.22 cfs 0.016 af
Subcatchment 22WS: 22 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 23WP: 23 WP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.17 cfs 0.013 af
Subcatchment 24WS: 24 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>2.77" Tc=5.0 min CN=98 Runoff=0.19 cfs 0.014 af

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Subcatchment 25WP: 25 WP	Runoff Area=2,640 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 26WS: 26 WS	Runoff Area=2,640 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 27WP: 27 WP	Runoff Area=2,400 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=0.17 cfs 0.013 af
Subcatchment 28WS: 28 WS	Runoff Area=2,640 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 29WP: 29 WP	Runoff Area=2,640 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 30WS: 30 WS	Runoff Area=2,400 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=0.17 cfs 0.013 af
Subcatchment 31WP: 31 WP	Runoff Area=2,640 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=0.19 cfs 0.014 af
Subcatchment 33WP: 33 WP	Runoff Area=3,000 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=0.22 cfs 0.016 af
Subcatchment 88S: 8WS	Runoff Area=2,400 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=0.17 cfs 0.013 af
Subcatchment CEC: Central East -	Runoff Area=17,152 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=1.23 cfs 0.091 af
Subcatchment CWC: Central West -	Runoff Area=36,000 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=2.58 cfs 0.191 af
Subcatchment ILC: IL Attached - Campus	Runoff Area=17,150 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=1.23 cfs 0.091 af
Subcatchment ILE: IL Attached - Campus	Runoff Area=8,575 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=0.62 cfs 0.046 af
Subcatchment ILW: IL Attached - Campus	Runoff Area=17,000 sf 100.00 Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=1.22 cfs 0.090 af
Subcatchment NC: North - Campus	Runoff Area=31,750 sf 100.00' Tc=5.0 min	% Impervious Runoff Depth>2.77" CN=98 Runoff=2.28 cfs 0.168 af
Pond IT 22: 20 CULTEC R-330XL	Peak Elev=177.01' Storag	e=719 cf Inflow=0.59 cfs 0.044 af Outflow=0.06 cfs 0.044 af
Pond IT10: 12 CULTEC R-330XL	Peak Elev=181.04' Storag	e=457 cf Inflow=0.38 cfs 0.028 af Outflow=0.04 cfs 0.028 af

8548.0 - Salmon Senior Community -	Medway - Propo Type III 24-hr 2-Year Rainfall=3.20"
Prepared by MICrosoπ HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD	Software Solutions LLC Printed 10/9/2015
Pond IT11: 28 CULTEC R-330XL	Peak Elev=180.40' Storage=891 cf Inflow=0.76 cfs 0.056 af
	Outflow=0.08 cfs 0.056 af
Pond IT11A · 6 CI II TEC P-330VI	Peak Elev-182 70' Storage-221 cf Inflow-0.19 cfs 0.014 af
FOND TITA: 0 COLTEC R-330XE	Outflow=0.02 cfs 0.014 af
Pond IT12: 14 CULTEC R-330XL	Peak Elev=180.43' Storage=472 cf Inflow=0.40 cfs 0.030 af
	Outflow=0.04 cfs 0.030 af
Bond IT12: 12 CI II TEC B 220VI	Peak Elev-177 72' Storage-426 cf Inflow-0.36 cfs 0.027 af
FONUTI 13: 12 COLTEC R-330AL	Outflow=0.04 cfs 0.027 af
Pond IT14: 12 CULTEC R-330XL	Peak Elev=177.47' Storage=426 cf Inflow=0.36 cfs 0.027 af
	Outflow=0.04 cfs 0.027 af
	Deals Flay, 179, 12' Storage, 472 of Inflaw, 0,40 of a 0,020 of
PONd 1115: 14 CULTEC R-330XL	Peak Elev=178.13 Storage=472 cf Innow=0.40 cfs 0.030 at Outflow=0.04 cfs 0.030 at
Pond IT16: 45 - 330XL	Peak Elev=176.97' Storage=1,489 cf Inflow=1.23 cfs 0.091 af
	Outflow=0.12 cfs 0.091 af
	Deals Flave 474.041 Observes 705 of Julians 0.00 of a 0.040 of
Pond 1117: 24 - 330XL	Peak Elev=1/4.31 Storage=/05 CF Inflow=0.62 Cfs 0.046 at
Pond IT18: 48 - 330XL	Peak Elev=174.88' Storage=1,455 cf Inflow=1.23 cfs 0.091 af
	Outflow=0.12 cfs 0.091 af
Pond I 119: 48 - 330XL	Peak Elev=172.66 Storage=1,437 ct Inflow=1.22 cts 0.090 at
Pond IT20: 100 - 330XL	Peak Elev=176.93' Storage=3,123 cf Inflow=2.58 cfs 0.191 af
	Outflow=0.24 cfs 0.191 af
Pond IT21: 25 CULTEC R-330XL	Peak Elev=171.25' Storage=903 ct Inflow=0.74 cts 0.055 at
Pond IT22A: 6 CULTEC R-330XL	Peak Elev=178.57' Storage=189 cf Inflow=0.17 cfs 0.013 af
	Outflow=0.02 cfs 0.013 af
Pond 1123: 88 - 330XL	Peak Elev=176.92' Storage=2,743 cf Inflow=2.28 cfs 0.168 af
Pond IT24: 8 CULTEC R-330XL	Peak Elev=177.33' Storage=244 cf Inflow=0.22 cfs 0.016 af
	Outflow=0.02 cfs 0.016 af
Pond IT25: 12 CULTEC R-330XL	Peak Elev=189.04' Storage=454 cf Inflow=0.38 cfs 0.028 af
	Outflow=0.04 cts 0.028 at
Pond IT26: 18 CULTEC R-330XL	Peak Elev=184.40' Storage=642 cf Inflow=0.53 cfs 0.039 af
	Outflow=0.05 cfs 0.039 af
Pond IT29: 27 CULTEC R-330XL	Peak Elev=184.96' Storage=905 cf Inflow=0.76 cfs 0.056 af
	Outflow=0.08 cfs 0.056 at

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HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD S	oftware Solutions LL	C Page 9		
Pond IT30: 15 CULTEC R-330XL	Peak Elev=182.22'	Storage=399 cf Inflow=0.36 cfs 0.027 af		
		Outflow=0.04 cfs 0.027 af		
Dond IT21: 27 CILL TEC D 220VI	Poak Flov-177 02'	Storage-976 of Inflow-0.74 of 0.055 of		
Pond 1131: 27 CULTEC R-330XL	Feak Elev=177.95	Outflow=0.08 cfs 0.055 af		
Pond IT8: 20 CULTEC R-330XL	Peak Elev=179.19'	Storage=666 cf Inflow=0.57 cfs 0.042 af		
		Outflow=0.06 cfs 0.042 af		
Band ITO: 6 CI II TEC B 220VI	Poak Flov-180 00'	Storage-196 cf Inflow-0.17 cfs 0.013 af		
Folid 119. 8 COLTEC R-330XL	1 eak Liev=100.03	Outflow=0.02 cfs 0.013 af		

Total Runoff Area = 5.519 ac Runoff Volume = 1.276 af Average Runoff Depth = 2.77" 0.00% Pervious = 0.000 ac 100.00% Impervious = 5.519 ac

Summary for Subcatchment 1BW: 1BW

Runoff = 0.17 cfs @ 12.07 hrs, Volume= 0.013 af, Depth> 2.77"



Summary for Subcatchment 1LP: 1 LP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 2BW: 2 BW

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 2LP: 2 LP

Runoff = 0.17 cfs @ 12.07 hrs, Volume= 0.013 af, Depth> 2.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"



Time (hours)

Summary for Subcatchment 2WS: 2 WS

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 3BW: 3 BW

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 3LP: 3 LP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 4BW: 4 BW

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 4LP: 4 LP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 4WS: 4 WS

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 5BW: 5 BW

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



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Summary for Subcatchment 5LP: 5LP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 6BW: 6 BW

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"


Summary for Subcatchment 6LP: 6 LP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 6WS: 6 WS

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 7LP: 7 LP

Runoff = 0.17 cfs @ 12.07 hrs, Volume= 0.013 af, Depth> 2.77"



Summary for Subcatchment 8LP: 8 LP

Runoff = 0.22 cfs @ 12.07 hrs, Volume= 0.016 af, Depth> 2.77"

0.06 0.05 0.04 0.03 0.02 0.01 0.01

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"



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Summary for Subcatchment 10WS: 10 WS

Runoff = 0.17 cfs @ 12.07 hrs, Volume= 0.013 af, Depth> 2.77"





Summary for Subcatchment 12WP: 12 WP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 12WS: 12 WS

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 14WP: 14 WP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 14WS: 14 WS

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 16WP: 16 WP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 16WS: 16 WS

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 18WP: 18 WP

Runoff = 0.22 cfs @ 12.07 hrs, Volume= 0.016 af, Depth> 2.77"





Summary for Subcatchment 18WS: 18 WS

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 19WP: 19 WP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 20WP: 20 WP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 20WS: 20 WS

Runoff = 0.17 cfs @ 12.07 hrs, Volume= 0.013 af, Depth> 2.77"

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Time (hours)

0.05 0.04 0.03 0.02 0.01 0.01

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"



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Summary for Subcatchment 21WP: 21 WP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 22WP: 22 WP

Runoff = 0.22 cfs @ 12.07 hrs, Volume= 0.016 af, Depth> 2.77"

Area (sf)	CN Description				
3,000	98 Roofs, HSG A				
3,000	3,000 100.00% Impervious Area				
Tc Length (min) (feet)	Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs)				
5.0	Direct Entry,				
Subcatchment 22WP: 22 WP					



Summary for Subcatchment 22WS: 22 WS

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 23WP: 23 WP

Runoff = 0.17 cfs @ 12.07 hrs, Volume= 0.013 af, Depth> 2.77"

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Time (hours)

0.06-0.05-0.04-0.03-0.02-0.01-0-

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"



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Summary for Subcatchment 24WS: 24 WS

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 25WP: 25 WP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 26WS: 26 WS

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 27WP: 27 WP

Runoff = 0.17 cfs @ 12.07 hrs, Volume= 0.013 af, Depth> 2.77"

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Time (hours)

0.02-0.01-0-

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"



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Summary for Subcatchment 28WS: 28 WS

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 29WP: 29 WP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 30WS: 30 WS

Runoff = 0.17 cfs @ 12.07 hrs, Volume= 0.013 af, Depth> 2.77"

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Time (hours)

0.07-0.06-0.05-0.04-0.03-0.02-0.01-0-0-

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"



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Summary for Subcatchment 31WP: 31 WP

Runoff = 0.19 cfs @ 12.07 hrs, Volume= 0.014 af, Depth> 2.77"



Summary for Subcatchment 33WP: 33 WP

Runoff = 0.22 cfs @ 12.07 hrs, Volume= 0.016 af, Depth> 2.77"

A	Area (sf)	CN	Description			
	3,000	98	Roofs, HSC	Э А		
	3,000	100.00% Impervious Area				
Tc (min)	Length (feet)	Slop (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description	
5.0 Direct Entry,						
Subcatchment 33WP: 33 WP						



Summary for Subcatchment 88S: 8WS

Runoff = 0.17 cfs @ 12.07 hrs, Volume= 0.013 af, Depth> 2.77"

Area (sf)	CN Description				
2,400	98 Roofs, HSG A				
2,400	2,400 100.00% Impervious Area				
Tc Length (min) (feet)	Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs)				
5.0	Direct Entry,				
Subcatchment 88S: 8WS Hydrograph					
0 10 1					



Summary for Subcatchment CEC: Central East - Campus

Runoff = 1.23 cfs @ 12.07 hrs, Volume= 0.091 af, Depth> 2.77"



Summary for Subcatchment CWC: Central West - Campus

Runoff = 2.58 cfs @ 12.07 hrs, Volume= 0.191 af, Depth> 2.77"



Summary for Subcatchment ILC: IL Attached - Campus - 6 units (center)

Runoff = 1.23 cfs @ 12.07 hrs, Volume= 0.091 af, Depth> 2.77"



Summary for Subcatchment ILE: IL Attached - Campus - 3 units (east)

Runoff = 0.62 cfs @ 12.07 hrs, Volume= 0.046 af, Depth> 2.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"

A	rea (sf)	CN	Description				
	8,575	98	3 Roofs, HSG A				
	8,575	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft	Velocity (ft/sec)	Capacity (cfs)	Description		
5.0		•			Direct Entry,		

Subcatchment ILE: IL Attached - Campus - 3 units (east)



Summary for Subcatchment ILW: IL Attached - Campus - 6 units (west)

Runoff = 1.22 cfs @ 12.07 hrs, Volume= 0.090 af, Depth> 2.77"

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Time (hours)

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.20"



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Summary for Subcatchment NC: North - Campus

Runoff = 2.28 cfs @ 12.07 hrs, Volume= 0.168 af, Depth> 2.77"


Summary for Pond IT 22: 20 CULTEC R-330XL

Inflow Area	=	0.190 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event	
Inflow	=	0.59 cfs @	12.07 hrs,	Volume	= 0.044	af			
Outflow	=	0.06 cfs @	12.83 hrs,	Volume	= 0.044	af, Atte	en= 90%,	Lag= 45.4 mi	n
Discarded	=	0.06 cfs @	12.83 hrs,	Volume	= 0.044	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.01' @ 12.83 hrs Surf.Area= 860 sf Storage= 719 cf

Plug-Flow detention time= 96.0 min calculated for 0.044 af (100% of inflow) Center-of-Mass det. time= 94.9 min (832.8 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	955 cf	22.33'W x 38.50'L x 4.04'H Field A
			3,475 cf Overall - 1,088 cf Embedded = 2,387 cf x 40.0% Voids
#2A	176.46'	1,088 cf	Cultec R-330XL x 20 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 4 rows
		2,043 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area	
Discard	ed OutFlow M filtration (Ext	Max=0.06 cfs	@ 12.83 hrs HW=177.01' (Free Discharge) rols 0.06 cfs)	

Pond IT 22: 20 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 4 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 4 Rows x 52.0" Wide + 12.0" Spacing x 3 + 12.0" Side Stone x 2 = 22.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

20 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 4 Rows = 1,087.8 cf Chamber Storage

3,475.2 cf Field - 1,087.8 cf Chambers = 2,387.3 cf Stone x 40.0% Voids = 954.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,042.8 cf = 0.047 af Overall Storage Efficiency = 58.8%

20 Chambers 128.7 cy Field 88.4 cy Stone







Pond IT 22: 20 CULTEC R-330XL

Summary for Pond IT10: 12 CULTEC R-330XL

Inflow Area	=	0.121 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event	
Inflow	=	0.38 cfs @	12.07 hrs,	Volume	= 0.028	af			
Outflow	=	0.04 cfs @	12.80 hrs,	Volume	= 0.028	af, Atte	en= 90%,	Lag= 43.5 n	nin
Discarded	=	0.04 cfs @	12.80 hrs,	Volume	= 0.028	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 181.04' @ 12.80 hrs Surf.Area= 536 sf Storage= 457 cf

Plug-Flow detention time= 93.5 min calculated for 0.028 af (100% of inflow) Center-of-Mass det. time= 92.5 min (830.3 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	179.46'	602 cf	17.00'W x 31.50'L x 4.04'H Field A
			2,164 cf Overall - 659 cf Embedded = 1,505 cf x 40.0% Voids
#2A	180.46'	659 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,261 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	179.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.04 cfs	@ 12.80 hrs HW=181.04' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Pond IT10: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 659.4 cf Chamber Storage

2,164.3 cf Field - 659.4 cf Chambers = 1,504.9 cf Stone x 40.0% Voids = 602.0 cf Stone Storage

Chamber Storage + Stone Storage = 1,261.4 cf = 0.029 af Overall Storage Efficiency = 58.3%

12 Chambers 80.2 cy Field 55.7 cy Stone







Pond IT10: 12 CULTEC R-330XL

Summary for Pond IT11: 28 CULTEC R-330XL

Inflow Area	=	0.242 ac,10	0.00% Impe	ervious,	Inflow E	Depth >	2.77"	for 2-Yea	ar event
Inflow	=	0.76 cfs @	12.07 hrs,	Volume	=	0.056	af		
Outflow	=	0.08 cfs @	12.77 hrs,	Volume	=	0.056	af, Atte	en= 90%,	Lag= 42.2 min
Discarded	=	0.08 cfs @	12.77 hrs,	Volume	=	0.056	af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 180.40' @ 12.77 hrs Surf.Area= 1,207 sf Storage= 891 cf

Plug-Flow detention time= 86.1 min calculated for 0.056 af (100% of inflow) Center-of-Mass det. time= 85.0 min (822.9 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.98'	1,337 cf	38.33'W x 31.50'L x 4.04'H Field A
			4,880 cf Overall - 1,539 cf Embedded = 3,342 cf x 40.0% Voids
#2A	179.98'	1,539 cf	Cultec R-330XL x 28 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 7 rows
		2,875 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	178.98'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.08 cfs	@ 12.77 hrs HW=180.40' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond IT11: 28 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 7 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 7 Rows x 52.0" Wide + 12.0" Spacing x 6 + 12.0" Side Stone x 2 = 38.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

28 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 7 Rows = 1,538.6 cf Chamber Storage

4,880.3 cf Field - 1,538.6 cf Chambers = 3,341.7 cf Stone x 40.0% Voids = 1,336.7 cf Stone Storage

Chamber Storage + Stone Storage = 2,875.3 cf = 0.066 af Overall Storage Efficiency = 58.9%

28 Chambers 180.8 cy Field 123.8 cy Stone







Pond IT11: 28 CULTEC R-330XL

Summary for Pond IT11A: 6 CULTEC R-330XL

Inflow Area	=	0.061 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event	
Inflow	=	0.19 cfs @	12.07 hrs,	Volume	= 0.01	4 af			
Outflow	=	0.02 cfs @	12.69 hrs,	Volume	= 0.01	4 af, At	ten= 89%,	Lag= 37.2 mir	n
Discarded	=	0.02 cfs @	12.69 hrs,	Volume	= 0.01	4 af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 182.70' @ 12.69 hrs Surf.Area= 280 sf Storage= 221 cf

Plug-Flow detention time= 80.4 min calculated for 0.014 af (100% of inflow) Center-of-Mass det. time= 79.6 min (817.5 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	181.21'	314 cf	16.00'W x 17.50'L x 4.04'H Field A
			1,132 cf Overall - 346 cf Embedded = 785 cf x 40.0% Voids
#2A	182.21'	346 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		661 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	181.21'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Exf	lax=0.02 cfs	e @ 12.69 hrs HW=182.70' (Free Discharge) trols 0.02 cfs)

Pond IT11A: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

2 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 15.50' Row Length +12.0" End Stone x 2 = 17.50' Base Length 3 Rows x 52.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 16.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 346.5 cf Chamber Storage

1,131.7 cf Field - 346.5 cf Chambers = 785.2 cf Stone x 40.0% Voids = 314.1 cf Stone Storage

Chamber Storage + Stone Storage = 660.5 cf = 0.015 af Overall Storage Efficiency = 58.4%

6 Chambers 41.9 cy Field 29.1 cy Stone







Pond IT11A: 6 CULTEC R-330XL

Summary for Pond IT12: 14 CULTEC R-330XL

Inflow Area	ι =	0.129 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event	
Inflow	=	0.40 cfs @	12.07 hrs,	Volume	= 0.030	af			
Outflow	=	0.04 cfs @	12.70 hrs,	Volume	= 0.030	af, Atte	en= 89%,	Lag= 38.0 mir	n
Discarded	=	0.04 cfs @	12.70 hrs,	Volume	= 0.030	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 180.43' @ 12.70 hrs Surf.Area= 613 sf Storage= 472 cf

Plug-Flow detention time= 80.9 min calculated for 0.030 af (100% of inflow) Center-of-Mass det. time= 80.1 min (818.0 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.96'	689 cf	11.67'W x 52.50'L x 4.04'H Field A
			2,476 cf Overall - 753 cf Embedded = 1,723 cf x 40.0% Voids
#2A	179.96'	753 cf	Cultec R-330XL x 14 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,442 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	178.96'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.04 cfs	@ 12.70 hrs HW=180.43' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Pond IT12: 14 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

14 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 752.6 cf Chamber Storage

2,475.5 cf Field - 752.6 cf Chambers = 1,723.0 cf Stone x 40.0% Voids = 689.2 cf Stone Storage

Chamber Storage + Stone Storage = 1,441.7 cf = 0.033 af Overall Storage Efficiency = 58.2%

14 Chambers 91.7 cy Field 63.8 cy Stone







Pond IT12: 14 CULTEC R-330XL

Summary for Pond IT13: 12 CULTEC R-330XL

Inflow Area	I =	0.116 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event	
Inflow	=	0.36 cfs @	12.07 hrs,	Volume	= 0.027	af			
Outflow	=	0.04 cfs @	12.72 hrs,	Volume	= 0.027	af, Atte	en= 89%,	Lag= 39.1	min
Discarded	=	0.04 cfs @	12.72 hrs,	Volume	= 0.027	' af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.72' @ 12.72 hrs Surf.Area= 531 sf Storage= 426 cf

Plug-Flow detention time= 83.9 min calculated for 0.027 af (100% of inflow) Center-of-Mass det. time= 83.1 min (821.0 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.21'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	177.21'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.21'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.04 cfs	@ 12.72 hrs HW=177.72' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Pond IT13: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT13: 12 CULTEC R-330XL

Summary for Pond IT14: 12 CULTEC R-330XL

Inflow Area	ι =	0.116 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event	
Inflow	=	0.36 cfs @	12.07 hrs,	Volume	= 0.027	' af			
Outflow	=	0.04 cfs @	12.72 hrs,	Volume	= 0.027	af, Atte	en= 89%,	Lag= 39.1	min
Discarded	=	0.04 cfs @	12.72 hrs,	Volume	= 0.027	' af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.47' @ 12.72 hrs Surf.Area= 531 sf Storage= 426 cf

Plug-Flow detention time= 83.9 min calculated for 0.027 af (100% of inflow) Center-of-Mass det. time= 83.1 min (821.0 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.96'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	176.96'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.96'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.04 cfs	a @ 12.72 hrs HW=177.47' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Pond IT14: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT14: 12 CULTEC R-330XL

Summary for Pond IT15: 14 CULTEC R-330XL

Inflow Area	I =	0.129 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event	
Inflow	=	0.40 cfs @	12.07 hrs,	Volume	= 0.030	af			
Outflow	=	0.04 cfs @	12.70 hrs,	Volume	= 0.030	af, Atte	en= 89%,	Lag= 38.0 n	nin
Discarded	=	0.04 cfs @	12.70 hrs,	Volume	= 0.030	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.13' @ 12.70 hrs Surf.Area= 613 sf Storage= 472 cf

Plug-Flow detention time= 80.9 min calculated for 0.030 af (100% of inflow) Center-of-Mass det. time= 80.1 min (818.0 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.66'	689 cf	11.67'W x 52.50'L x 4.04'H Field A
			2,476 cf Overall - 753 cf Embedded = 1,723 cf x 40.0% Voids
#2A	177.66'	753 cf	Cultec R-330XL x 14 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,442 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.66'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.04 cfs	@ 12.70 hrs HW=178.13' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Pond IT15: 14 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

14 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 752.6 cf Chamber Storage

2,475.5 cf Field - 752.6 cf Chambers = 1,723.0 cf Stone x 40.0% Voids = 689.2 cf Stone Storage

Chamber Storage + Stone Storage = 1,441.7 cf = 0.033 af Overall Storage Efficiency = 58.2%

14 Chambers 91.7 cy Field 63.8 cy Stone







Pond IT15: 14 CULTEC R-330XL

Summary for Pond IT16: 45 - 330XL

Inflow Area	a =	0.394 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event
Inflow	=	1.23 cfs @	12.07 hrs,	Volume	= 0.091	af		
Outflow	=	0.12 cfs @	12.85 hrs,	Volume	= 0.091	af, Att	en= 90%,	Lag= 46.8 min
Discarded	=	0.12 cfs @	12.85 hrs,	Volume	= 0.091	af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 176.97' @ 12.85 hrs Surf.Area= 1,840 sf Storage= 1,489 cf

Plug-Flow detention time= 97.3 min calculated for 0.091 af (100% of inflow) Center-of-Mass det. time= 96.2 min (834.0 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	2,013 cf	27.67'W x 66.50'L x 4.04'H Field A
			7,436 cf Overall - 2,403 cf Embedded = 5,033 cf x 40.0% Voids
#2A	176.46'	2,403 cf	Cultec R-330XL x 45 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 5 rows
		4,416 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area	
Discard	ed OutFlow M filtration (Exf	Max=0.12 cfs	@ 12.85 hrs HW=176.97' (Free Discharge) rols 0.12 cfs)	

Pond IT16: 45 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 5 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 5 Rows x 52.0" Wide + 12.0" Spacing x 4 + 12.0" Side Stone x 2 = 27.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

45 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 5 Rows = 2,402.9 cf Chamber Storage

7,436.0 cf Field - 2,402.9 cf Chambers = 5,033.0 cf Stone x 40.0% Voids = 2,013.2 cf Stone Storage

Chamber Storage + Stone Storage = 4,416.2 cf = 0.101 af Overall Storage Efficiency = 59.4%

45 Chambers 275.4 cy Field 186.4 cy Stone





8548.0 - Salmon Senior Community - Medway - Propo Type III 24-hr 2-Year Rainfall=3.20"Prepared by MicrosoftPrinted 10/9/2015HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLCPage 85



Pond IT16: 45 - 330XL

Summary for Pond IT17: 24 - 330XL

Inflow Area	I =	0.197 ac,10	0.00% Impe	ervious, li	nflow Depth >	2.77"	for 2-Yea	ar event
Inflow	=	0.62 cfs @	12.07 hrs,	Volume=	0.046	af		
Outflow	=	0.07 cfs @	12.71 hrs,	Volume=	0.045	af, Atte	en= 89%,	Lag= 38.3 min
Discarded	=	0.07 cfs @	12.71 hrs,	Volume=	0.045	af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 174.31' @ 12.71 hrs Surf.Area= 1,040 sf Storage= 705 cf

Plug-Flow detention time= 77.2 min calculated for 0.045 af (100% of inflow) Center-of-Mass det. time= 76.5 min (814.3 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	172.96'	1,153 cf	33.00'W x 31.50'L x 4.04'H Field A
			4,201 cf Overall - 1,319 cf Embedded = 2,882 cf x 40.0% Voids
#2A	173.96'	1,319 cf	Cultec R-330XL x 24 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		2,472 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	172.96'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Ext	Max=0.07 cfs	@ 12.71 hrs HW=174.31' (Free Discharge) trols 0.07 cfs)

Pond IT17: 24 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

24 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 1,318.8 cf Chamber Storage

4,201.3 cf Field - 1,318.8 cf Chambers = 2,882.5 cf Stone x 40.0% Voids = 1,153.0 cf Stone Storage

Chamber Storage + Stone Storage = 2,471.8 cf = 0.057 af Overall Storage Efficiency = 58.8%

24 Chambers 155.6 cy Field 106.8 cy Stone





8548.0 - Salmon Senior Community - Medway - Propo Type III 24-hr 2-Year Rainfall=3.20"Prepared by MicrosoftPrinted 10/9/2015HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLCPage 88



Pond IT17: 24 - 330XL

Summary for Pond IT18: 48 - 330XL

Inflow Area	I =	0.394 ac,10	0.00% Impe	ervious,	Inflow Dep	oth > 2.	.77" f	or 2-Yea	ar event
Inflow	=	1.23 cfs @	12.07 hrs,	Volume	= 0).091 af			
Outflow	=	0.12 cfs @	12.80 hrs,	Volume	= 0).091 af	, Atter	i= 90%, I	Lag= 43.8 min
Discarded	=	0.12 cfs @	12.80 hrs,	Volume	= 0).091 af			-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 174.88' @ 12.80 hrs Surf.Area= 1,964 sf Storage= 1,455 cf

Plug-Flow detention time= 88.6 min calculated for 0.091 af (100% of inflow) Center-of-Mass det. time= 87.8 min (825.6 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	173.46'	2,146 cf	33.00'W x 59.50'L x 4.04'H Field A
			7,936 cf Overall - 2,571 cf Embedded = 5,365 cf x 40.0% Voids
#2A	174.46'	2,571 cf	Cultec R-330XL x 48 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		4,717 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	173.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Exf	Max=0.12 cfs	e @ 12.80 hrs HW=174.88' (Free Discharge) trols 0.12 cfs)

Pond IT18: 48 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

48 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 2,570.6 cf Chamber Storage

7,935.8 cf Field - 2,570.6 cf Chambers = 5,365.2 cf Stone x 40.0% Voids = 2,146.1 cf Stone Storage

Chamber Storage + Stone Storage = 4,716.7 cf = 0.108 af Overall Storage Efficiency = 59.4%

48 Chambers 293.9 cy Field 198.7 cy Stone





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Pond IT18: 48 - 330XL

Summary for Pond IT19: 48 - 330XL

Inflow Area	ι =	0.390 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event
Inflow	=	1.22 cfs @	12.07 hrs,	Volume	= 0.090	af		
Outflow	=	0.12 cfs @	12.79 hrs,	Volume	= 0.090	af, Atte	en= 90%,	Lag= 43.3 mir
Discarded	=	0.12 cfs @	12.79 hrs,	Volume	= 0.090	af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 172.66' @ 12.79 hrs Surf.Area= 1,964 sf Storage= 1,437 cf

Plug-Flow detention time= 87.6 min calculated for 0.090 af (100% of inflow) Center-of-Mass det. time= 86.6 min (824.4 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	171.25'	2,146 cf	33.00'W x 59.50'L x 4.04'H Field A
			7,936 cf Overall - 2,571 cf Embedded = 5,365 cf x 40.0% Voids
#2A	172.25'	2,571 cf	Cultec R-330XL x 48 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		4,717 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	171.25'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.12 cfs	@ 12.79 hrs HW=172.66' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.12 cfs)

Pond IT19: 48 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

48 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 2,570.6 cf Chamber Storage

7,935.8 cf Field - 2,570.6 cf Chambers = 5,365.2 cf Stone x 40.0% Voids = 2,146.1 cf Stone Storage

Chamber Storage + Stone Storage = 4,716.7 cf = 0.108 af Overall Storage Efficiency = 59.4%

48 Chambers 293.9 cy Field 198.7 cy Stone





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Pond IT19: 48 - 330XL
Summary for Pond IT20: 100 - 330XL

Inflow Area	1 =	0.826 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event
Inflow	=	2.58 cfs @	12.07 hrs,	Volume=	= 0.191	af		
Outflow	=	0.24 cfs @	12.87 hrs,	Volume:	= 0.191	af, Atte	en= 91%,	Lag= 48.0 min
Discarded	=	0.24 cfs @	12.87 hrs,	Volume=	= 0.191	af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 176.93' @ 12.87 hrs Surf.Area= 3,994 sf Storage= 3,123 cf

Plug-Flow detention time= 98.2 min calculated for 0.190 af (100% of inflow) Center-of-Mass det. time= 97.1 min (835.0 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	4,325 cf	54.33'W x 73.50'L x 4.04'H Field A
			16,140 cf Overall - 5,327 cf Embedded = 10,813 cf x 40.0% Voids
#2A	176.46'	5,327 cf	Cultec R-330XL x 100 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 10 rows
		9,653 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Ext	Max=0.24 cfs	@ 12.87 hrs HW=176.93' (Free Discharge) trols 0.24 cfs)

Pond IT20: 100 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 10 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

10 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 71.50' Row Length +12.0" End Stone x 2 = 73.50' Base Length 10 Rows x 52.0" Wide + 12.0" Spacing x 9 + 12.0" Side Stone x 2 = 54.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

100 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 10 Rows = 5,327.5 cf Chamber Storage

16,140.4 cf Field - 5,327.5 cf Chambers = 10,812.9 cf Stone x 40.0% Voids = 4,325.2 cf Stone Storage

Chamber Storage + Stone Storage = 9,652.6 cf = 0.222 af Overall Storage Efficiency = 59.8%

100 Chambers 597.8 cy Field 400.5 cy Stone





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Pond IT20: 100 - 330XL

Summary for Pond IT21: 25 CULTEC R-330XL

Inflow Area	=	0.237 ac,10	0.00% Impe	ervious,	Inflow Dept	th > 2.	77" for	2-Year	event	
Inflow	=	0.74 cfs @	12.07 hrs,	Volume	= 0	.055 af				
Outflow	=	0.07 cfs @	12.86 hrs,	Volume	= 0	.055 af,	Atten= 9	90%, La	ig= 47.1 n	nin
Discarded	=	0.07 cfs @	12.86 hrs,	Volume	= 0	.055 af			-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 171.25' @ 12.86 hrs Surf.Area= 1,065 sf Storage= 903 cf

Plug-Flow detention time= 99.3 min calculated for 0.055 af (100% of inflow) Center-of-Mass det. time= 98.6 min (836.4 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	169.69'	1,178 cf	27.67'W x 38.50'L x 4.04'H Field A
			4,305 cf Overall - 1,360 cf Embedded = 2,945 cf x 40.0% Voids
#2A	170.69'	1,360 cf	Cultec R-330XL x 25 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 5 rows
		2,538 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	169.69'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.07 cfs	@ 12.86 hrs HW=171.25' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.07 cfs)

Pond IT21: 25 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 5 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 5 Rows x 52.0" Wide + 12.0" Spacing x 4 + 12.0" Side Stone x 2 = 27.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

25 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 5 Rows = 1,359.8 cf Chamber Storage

4,305.0 cf Field - 1,359.8 cf Chambers = 2,945.2 cf Stone x 40.0% Voids = 1,178.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,537.9 cf = 0.058 af Overall Storage Efficiency = 59.0%

25 Chambers 159.4 cy Field 109.1 cy Stone







Pond IT21: 25 CULTEC R-330XL

Summary for Pond IT22A: 6 CULTEC R-330XL

Inflow Area	ι =	0.055 ac,10	0.00% Impe	ervious,	Inflow	Depth >	2.77"	for 2-Yea	ar event	
Inflow	=	0.17 cfs @	12.07 hrs,	Volume	=	0.013	af			
Outflow	=	0.02 cfs @	12.60 hrs,	Volume	=	0.013	af, Att	en= 87%,	Lag= 31.6	min
Discarded	=	0.02 cfs @	12.60 hrs,	Volume	=	0.013	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.57' @ 12.60 hrs Surf.Area= 288 sf Storage= 189 cf

Plug-Flow detention time= 62.3 min calculated for 0.013 af (100% of inflow) Center-of-Mass det. time= 61.4 min (799.2 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	177.46'	279 cf	6.33'W x 45.50'L x 3.54'H Field A
			1,021 cf Overall - 324 cf Embedded = 696 cf x 40.0% Voids
#2A	177.96'	324 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 1 rows
		603 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices						
#1	Discarded	177.46'	2.410 in/hr Exfiltration over Wetted area						
Discard	Discarded OutFlow Max=0.02 cfs @ 12.60 hrs HW=178.57' (Free Discharge) -1=Exfiltration (Exfiltration Controls 0.02 cfs)								

Pond IT22A: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 1 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 1 Rows x 52.0" Wide + 12.0" Side Stone x 2 = 6.33' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 1 Rows = 324.1 cf Chamber Storage

1,020.6 cf Field - 324.1 cf Chambers = 696.5 cf Stone x 40.0% Voids = 278.6 cf Stone Storage

Chamber Storage + Stone Storage = 602.7 cf = 0.014 af Overall Storage Efficiency = 59.1%

6 Chambers 37.8 cy Field 25.8 cy Stone







Pond IT22A: 6 CULTEC R-330XL

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Summary for Pond IT23: 88 - 330XL

Inflow Area	I =	0.729 ac,10	0.00% Imper	rvious, Inflov	v Depth >	2.77"	for 2-Yea	ar event
Inflow	=	2.28 cfs @	12.07 hrs, \	√olume=	0.168	af		
Outflow	=	0.22 cfs @	12.86 hrs, \	/olume=	0.168	af, Atte	en= 90%,	Lag= 47.3 min
Discarded	=	0.22 cfs @	12.86 hrs, \	/olume=	0.168	af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 176.92' @ 12.86 hrs Surf.Area= 3,550 sf Storage= 2,743 cf

Plug-Flow detention time= 96.1 min calculated for 0.168 af (100% of inflow) Center-of-Mass det. time= 95.4 min (833.2 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	3,854 cf	59.67'W x 59.50'L x 4.04'H Field A
			14,349 cf Overall - 4,713 cf Embedded = 9,636 cf x 40.0% Voids
#2A	176.46'	4,713 cf	Cultec R-330XL x 88 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 11 rows
		8,567 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.22 cfs filtration Cont	@ 12.86 hrs HW=176.92' (Free Discharge) trols 0.22 cfs)

Pond IT23: 88 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 11 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 11 Rows x 52.0" Wide + 12.0" Spacing x 10 + 12.0" Side Stone x 2 = 59.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

88 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 11 Rows = 4,712.8 cf Chamber Storage

14,348.6 cf Field - 4,712.8 cf Chambers = 9,635.8 cf Stone x 40.0% Voids = 3,854.3 cf Stone Storage

Chamber Storage + Stone Storage = 8,567.1 cf = 0.197 af Overall Storage Efficiency = 59.7%

88 Chambers 531.4 cy Field 356.9 cy Stone





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Pond IT23: 88 - 330XL

Summary for Pond IT24: 8 CULTEC R-330XL

Inflow Area	I =	0.069 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event
Inflow	=	0.22 cfs @	12.07 hrs,	Volume	= 0.016	af		
Outflow	=	0.02 cfs @	12.66 hrs,	Volume	= 0.016	af, Atte	en= 88%,	Lag= 35.3 min
Discarded	=	0.02 cfs @	12.66 hrs,	Volume	= 0.016	af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.33' @ 12.66 hrs Surf.Area= 352 sf Storage= 244 cf

Plug-Flow detention time= 73.2 min calculated for 0.016 af (100% of inflow) Center-of-Mass det. time= 72.3 min (810.1 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.21'	322 cf	11.17'W x 31.50'L x 3.54'H Field A
			1,246 cf Overall - 440 cf Embedded = 806 cf x 40.0% Voids
#2A	176.71'	440 cf	Cultec R-330XL x 8 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		762 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.21'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Exf	Max=0.02 cfs	s @ 12.66 hrs HW=177.33' (Free Discharge) trols 0.02 cfs)

Pond IT24: 8 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 2 Rows x 52.0" Wide + 6.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.17' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

8 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 439.6 cf Chamber Storage

1,245.8 cf Field - 439.6 cf Chambers = 806.2 cf Stone x 40.0% Voids = 322.5 cf Stone Storage

Chamber Storage + Stone Storage = 762.1 cf = 0.017 af Overall Storage Efficiency = 61.2%

8 Chambers 46.1 cy Field 29.9 cy Stone







Pond IT24: 8 CULTEC R-330XL

Summary for Pond IT25: 12 CULTEC R-330XL

Inflow Area	I =	0.121 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event	
Inflow	=	0.38 cfs @	12.07 hrs,	Volume	= 0.028	af			
Outflow	=	0.04 cfs @	12.76 hrs,	Volume	= 0.028	af, Atte	en= 90%,	Lag= 41.4	min
Discarded	=	0.04 cfs @	12.76 hrs,	Volume	= 0.028	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 189.04' @ 12.76 hrs Surf.Area= 531 sf Storage= 454 cf

Plug-Flow detention time= 90.0 min calculated for 0.028 af (100% of inflow) Center-of-Mass det. time= 89.0 min (826.8 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	187.46'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	188.46'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	187.46'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow	Max=0.04 cfs	@ 12.76 hrs HW=189.04' (Free Discharge)	

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Pond IT25: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT25: 12 CULTEC R-330XL

Summary for Pond IT26: 18 CULTEC R-330XL

Inflow Area	ι =	0.171 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event
Inflow	=	0.53 cfs @	12.07 hrs,	Volume	= 0.039	af		
Outflow	=	0.05 cfs @	12.80 hrs,	Volume	= 0.039	af, Atte	en= 90%,	Lag= 43.8 min
Discarded	=	0.05 cfs @	12.80 hrs,	Volume	= 0.039	af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 184.40' @ 12.80 hrs Surf.Area= 774 sf Storage= 642 cf

Plug-Flow detention time= 92.9 min calculated for 0.039 af (100% of inflow) Center-of-Mass det. time= 91.8 min (829.7 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	182.86'	862 cf	17.00'W x 45.50'L x 4.04'H Field A
			3,126 cf Overall - 972 cf Embedded = 2,154 cf x 40.0% Voids
#2A	183.86'	972 cf	Cultec R-330XL x 18 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,834 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	182.86'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow I filtration (Ext	Max=0.05 cfs filtration Cont	@ 12.80 hrs HW=184.40' (Free Discharge) rols 0.05 cfs)

Pond IT26: 18 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

18 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 972.4 cf Chamber Storage

3,126.2 cf Field - 972.4 cf Chambers = 2,153.9 cf Stone x 40.0% Voids = 861.5 cf Stone Storage

Chamber Storage + Stone Storage = 1,833.9 cf = 0.042 af Overall Storage Efficiency = 58.7%

18 Chambers 115.8 cy Field 79.8 cy Stone







Pond IT26: 18 CULTEC R-330XL

Summary for Pond IT29: 27 CULTEC R-330XL

Inflow Area	I =	0.242 ac,10	0.00% Impe	ervious,	Inflow Depth	> 2.77'	for 2-Yea	ar event
Inflow	=	0.76 cfs @	12.07 hrs,	Volume	= 0.0)56 af		
Outflow	=	0.08 cfs @	12.79 hrs,	Volume	= 0.0)56 af, A ^r	tten= 90%,	Lag= 43.4 min
Discarded	=	0.08 cfs @	12.79 hrs,	Volume	= 0.0)56 af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 184.96' @ 12.79 hrs Surf.Area= 1,131 sf Storage= 905 cf

Plug-Flow detention time= 90.5 min calculated for 0.056 af (100% of inflow) Center-of-Mass det. time= 89.8 min (827.6 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	183.46'	1,251 cf	17.00'W x 66.50'L x 4.04'H Field A
			4,569 cf Overall - 1,442 cf Embedded = 3,127 cf x 40.0% Voids
#2A	184.46'	1,442 cf	Cultec R-330XL x 27 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		2,693 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	183.46'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow	Max=0.08 cfs	@ 12.79 hrs HW=184.96' (Free Discharge)	

1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond IT29: 27 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

27 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 1,441.8 cf Chamber Storage

4,569.1 cf Field - 1,441.8 cf Chambers = 3,127.3 cf Stone x 40.0% Voids = 1,250.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,692.7 cf = 0.062 af Overall Storage Efficiency = 58.9%

27 Chambers 169.2 cy Field 115.8 cy Stone







Pond IT29: 27 CULTEC R-330XL

Summary for Pond IT30: 15 CULTEC R-330XL

Inflow Area	a =	0.116 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event	
Inflow	=	0.36 cfs @	12.07 hrs,	Volume	= 0.027	af			
Outflow	=	0.04 cfs @	12.62 hrs,	Volume	= 0.027	af, Atte	en= 88%,	Lag= 33.0 m	nin
Discarded	=	0.04 cfs @	12.62 hrs,	Volume	= 0.027	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 182.22' @ 12.62 hrs Surf.Area= 655 sf Storage= 399 cf

Plug-Flow detention time= 65.4 min calculated for 0.027 af (100% of inflow) Center-of-Mass det. time= 64.4 min (802.2 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	180.96'	732 cf	17.00'W x 38.50'L x 4.04'H Field A
			2,645 cf Overall - 816 cf Embedded = 1,829 cf x 40.0% Voids
#2A	181.96'	816 cf	Cultec R-330XL x 15 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,548 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	180.96'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.04 cfs	@ 12.62 hrs HW=182.22' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Pond IT30: 15 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

15 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 815.9 cf Chamber Storage

2,645.3 cf Field - 815.9 cf Chambers = 1,829.4 cf Stone x 40.0% Voids = 731.8 cf Stone Storage

Chamber Storage + Stone Storage = 1,547.6 cf = 0.036 af Overall Storage Efficiency = 58.5%

15 Chambers 98.0 cy Field 67.8 cy Stone







Pond IT30: 15 CULTEC R-330XL

Summary for Pond IT31: 27 CULTEC R-330XL

Inflow Area	=	0.237 ac,10	0.00% Impe	ervious,	Inflow [Depth >	2.77"	for 2-Yea	ar event
Inflow	=	0.74 cfs @	12.07 hrs,	Volume	=	0.055	af		
Outflow	=	0.08 cfs @	12.77 hrs,	Volume	=	0.055	af, Atte	en= 90%,	Lag= 42.1 mir
Discarded	=	0.08 cfs @	12.77 hrs,	Volume	=	0.055	af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.93' @ 12.77 hrs Surf.Area= 1,131 sf Storage= 876 cf

Plug-Flow detention time= 87.7 min calculated for 0.055 af (100% of inflow) Center-of-Mass det. time= 86.6 min (824.4 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.46'	1,251 cf	17.00'W x 66.50'L x 4.04'H Field A
			4,569 cf Overall - 1,442 cf Embedded = 3,127 cf x 40.0% Voids
#2A	177.46'	1,442 cf	Cultec R-330XL x 27 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		2,693 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.46'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.08 cfs	@ 12.77 hrs HW=177.93' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond IT31: 27 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

27 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 1,441.8 cf Chamber Storage

4,569.1 cf Field - 1,441.8 cf Chambers = 3,127.3 cf Stone x 40.0% Voids = 1,250.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,692.7 cf = 0.062 af Overall Storage Efficiency = 58.9%

27 Chambers 169.2 cy Field 115.8 cy Stone







Pond IT31: 27 CULTEC R-330XL

Summary for Pond IT8: 20 CULTEC R-330XL

Inflow Area	ι =	0.182 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event
Inflow	=	0.57 cfs @	12.07 hrs,	Volume	= 0.042	af		
Outflow	=	0.06 cfs @	12.72 hrs,	Volume	= 0.042	af, Atte	en= 89%,	Lag= 38.9 min
Discarded	=	0.06 cfs @	12.72 hrs,	Volume	= 0.042	af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.19' @ 12.72 hrs Surf.Area= 858 sf Storage= 666 cf

Plug-Flow detention time= 82.8 min calculated for 0.042 af (100% of inflow) Center-of-Mass det. time= 81.8 min (819.6 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	177.71'	960 cf	11.67'W x 73.50'L x 4.04'H Field A
			3,466 cf Overall - 1,065 cf Embedded = 2,400 cf x 40.0% Voids
#2A	178.71'	1,065 cf	Cultec R-330XL x 20 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		2,026 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	177.71'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow	Max=0.06 cfs	@ 12.72 hrs HW=179.19' (Free Discharg	e)

1=Exfiltration (Exfiltration Controls 0.06 cfs)

Pond IT8: 20 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

10 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 71.50' Row Length +12.0" End Stone x 2 = 73.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

20 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 1,065.5 cf Chamber Storage

3,465.7 cf Field - 1,065.5 cf Chambers = 2,400.2 cf Stone x 40.0% Voids = 960.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,025.6 cf = 0.047 af Overall Storage Efficiency = 58.4%

20 Chambers 128.4 cy Field 88.9 cy Stone







Pond IT8: 20 CULTEC R-330XL

Summary for Pond IT9: 6 CULTEC R-330XL

Inflow Area	I =	0.055 ac,10	0.00% Impe	ervious,	Inflow Depth >	2.77"	for 2-Yea	ar event
Inflow	=	0.17 cfs @	12.07 hrs,	Volume	= 0.013	af		
Outflow	=	0.02 cfs @	12.66 hrs,	Volume	= 0.013	af, Atte	en= 88%,	Lag= 35.6 min
Discarded	=	0.02 cfs @	12.66 hrs,	Volume	= 0.013	af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 180.09' @ 12.66 hrs Surf.Area= 280 sf Storage= 196 cf

Plug-Flow detention time= 73.7 min calculated for 0.013 af (100% of inflow) Center-of-Mass det. time= 73.1 min (810.9 - 737.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.96'	258 cf	16.00'W x 17.50'L x 3.54'H Field A
			992 cf Overall - 346 cf Embedded = 645 cf x 40.0% Voids
#2A	179.46'	346 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		605 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices					
#1	Discarded	178.96'	2.410 in/hr Exfiltration over Wetted area					
Discard	Discarded OutFlow Max=0.02 cfs @ 12.66 hrs HW=180.09' (Free Discharge) -1=Exfiltration (Exfiltration Controls 0.02 cfs)							

Pond IT9: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

2 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 15.50' Row Length +12.0" End Stone x 2 = 17.50' Base Length 3 Rows x 52.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 16.00' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 346.5 cf Chamber Storage

991.7 cf Field - 346.5 cf Chambers = 645.2 cf Stone x 40.0% Voids = 258.1 cf Stone Storage

Chamber Storage + Stone Storage = 604.5 cf = 0.014 afOverall Storage Efficiency = 61.0%

6 Chambers 36.7 cy Field 23.9 cy Stone







Pond IT9: 6 CULTEC R-330XL
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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1BW:1BW	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.25 cfs 0.019 af
Subcatchment1LP:1 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 2BW: 2 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 2LP: 2 LP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.25 cfs 0.019 af
Subcatchment 2WS: 2 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment3BW: 3 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 3LP: 3 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 4BW: 4 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 4LP: 4 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment4WS: 4 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment5BW: 5 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment5LP: 5LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment6BW: 6 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 6LP: 6 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment6WS: 6 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment7LP: 7 LP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.25 cfs 0.019 af

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Subcatchment 8LP: 8 LP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.32 cfs 0.024 af
Subcatchment10WS:10WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.25 cfs 0.019 af
Subcatchment 12WP: 12 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 12WS: 12 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 14WP: 14 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 14WS: 14 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 16WP: 16 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 16WS: 16 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 18WP: 18 WP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.32 cfs 0.024 af
Subcatchment 18WS: 18 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 19WP: 19 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 20WP: 20 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 20WS: 20 WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.25 cfs 0.019 af
Subcatchment 21WP: 21 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 22WP: 22 WP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.32 cfs 0.024 af
Subcatchment 22WS: 22 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 23WP: 23 WP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.25 cfs 0.019 af
Subcatchment 24WS: 24 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af

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Subcatchment 25WP: 25 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 26WS: 26 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 27WP: 27 WP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.25 cfs 0.019 af
Subcatchment 28WS: 28 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 29WP: 29 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 30WS: 30 WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.25 cfs 0.019 af
Subcatchment 31WP: 31 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.28 cfs 0.021 af
Subcatchment 33WP: 33 WP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.32 cfs 0.024 af
Subcatchment 88S: 8WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.25 cfs 0.019 af
Subcatchment CEC: Central East -	Runoff Area=17,152 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=1.82 cfs 0.136 af
Subcatchment CWC: Central West -	Runoff Area=36,000 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=3.82 cfs 0.285 af
Subcatchment ILC: IL Attached - Campus	Runoff Area=17,150 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=1.82 cfs 0.136 af
Subcatchment ILE: IL Attached - Campus	 Runoff Area=8,575 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=0.91 cfs 0.068 af
Subcatchment ILW: IL Attached - Campus	Runoff Area=17,000 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=1.80 cfs 0.135 af
Subcatchment NC: North - Campus	Runoff Area=31,750 sf 100.00% Impervious Runoff Depth>4.15" Tc=5.0 min CN=98 Runoff=3.37 cfs 0.252 af
Pond IT 22: 20 CULTEC R-330XL	Peak Elev=177.79' Storage=1,233 cf Inflow=0.88 cfs 0.066 af Outflow=0.06 cfs 0.057 af
Pond IT10: 12 CULTEC R-330XL	Peak Elev=181.84' Storage=781 cf Inflow=0.56 cfs 0.042 af Outflow=0.04 cfs 0.037 af

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Pond IT11: 28 CULTEC R-330XL	Peak Elev=181.08' Storage=1,532 c	of Inflow=1.12 cfs 0.084 af Outflow=0.08 cfs 0.075 af
Pond IT11A: 6 CULTEC R-330XL	Peak Elev=183.43' Storage=377 o	of Inflow=0.28 cfs 0.021 af Outflow=0.02 cfs 0.020 af
Pond IT12: 14 CULTEC R-330XL	Peak Elev=181.15' Storage=806 o	of Inflow=0.60 cfs 0.045 af Outflow=0.05 cfs 0.042 af
Pond IT13: 12 CULTEC R-330XL	Peak Elev=178.47' Storage=727 o	of Inflow=0.54 cfs 0.040 af Outflow=0.04 cfs 0.037 af
Pond IT14: 12 CULTEC R-330XL	Peak Elev=178.22' Storage=727 o	of Inflow=0.54 cfs 0.040 af Outflow=0.04 cfs 0.037 af
Pond IT15: 14 CULTEC R-330XL	Peak Elev=178.85' Storage=806 o	of Inflow=0.60 cfs 0.045 af Outflow=0.05 cfs 0.042 af
Pond IT16: 45 - 330XL	Peak Elev=177.71' Storage=2,564 o	of Inflow=1.82 cfs 0.136 af Outflow=0.13 cfs 0.115 af
Pond IT17: 24 - 330XL	Peak Elev=174.93' Storage=1,213 c	f Inflow=0.91 cfs 0.068 af Outflow=0.07 cfs 0.063 af
Pond IT18: 48 - 330XL	Peak Elev=175.56' Storage=2,508 c	of Inflow=1.82 cfs 0.136 af Outflow=0.13 cfs 0.119 af
Pond IT19: 48 - 330XL	Peak Elev=173.33' Storage=2,477 o	of Inflow=1.80 cfs 0.135 af Outflow=0.13 cfs 0.119 af
Pond IT20: 100 - 330XL	Peak Elev=177.64' Storage=5,403 c	of Inflow=3.82 cfs 0.285 af Outflow=0.25 cfs 0.238 af
Pond IT21: 25 CULTEC R-330XL	Peak Elev=172.04' Storage=1,551 c	f Inflow=1.10 cfs 0.082 af Outflow=0.08 cfs 0.069 af
Pond IT22A: 6 CULTEC R-330XL	Peak Elev=179.19' Storage=320 o	of Inflow=0.25 cfs 0.019 af Outflow=0.03 cfs 0.019 af
Pond IT23: 88 - 330XL	Peak Elev=177.63' Storage=4,742 c	of Inflow=3.37 cfs 0.252 af Outflow=0.23 cfs 0.212 af
Pond IT24: 8 CULTEC R-330XL	Peak Elev=177.98' Storage=416 c	of Inflow=0.32 cfs 0.024 af Outflow=0.03 cfs 0.023 af
Pond IT25: 12 CULTEC R-330XL	Peak Elev=189.84' Storage=774 o	of Inflow=0.56 cfs 0.042 af Outflow=0.04 cfs 0.038 af
Pond IT26: 18 CULTEC R-330XL	Peak Elev=185.17' Storage=1,099 o	f Inflow=0.79 cfs 0.059 af Outflow=0.06 cfs 0.052 af
Pond IT29: 27 CULTEC R-330XL	Peak Elev=185.70' Storage=1,552 c	of Inflow=1.12 cfs 0.084 af Outflow=0.08 cfs 0.074 af

8548.0 - Salmon Senior Community - Medway - Prop <i>Type III 24-hr</i> 10-Year Rainfall=4.70" Prepared by Microsoft Printed 10/9/2015 HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLC Page 135		
Pond IT30: 15 CULTEC R-330XL	Peak Elev=182.78' Storage=684 cf Inflow=0.54 cfs 0.040 af Outflow=0.05 cfs 0.040 af	
Pond IT31: 27 CULTEC R-330XL	Peak Elev=178.64' Storage=1,503 cf Inflow=1.10 cfs 0.082 af Outflow=0.08 cfs 0.073 af	
Pond IT8: 20 CULTEC R-330XL	Peak Elev=179.90' Storage=1,138 cf Inflow=0.84 cfs 0.063 af Outflow=0.07 cfs 0.058 af	
Pond IT9: 6 CULTEC R-330XL	Peak Elev=180.74' Storage=334 cf Inflow=0.25 cfs 0.019 af Outflow=0.02 cfs 0.018 af	
Total Runoff Area – 5 519 ac	Runoff Volume – 1 907 af Average Runoff Depth – 4 15	

Total Runoff Area = 5.519 ac Runoff Volume = 1.907 af Average Runoff Depth = 4.15" 0.00% Pervious = 0.000 ac 100.00% Impervious = 5.519 ac

Summary for Subcatchment 1BW: 1BW

Runoff = 0.25 cfs @ 12.07 hrs, Volume= 0.019 af, Depth> 4.15"



Summary for Subcatchment 1LP: 1 LP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 2BW: 2 BW

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 2LP: 2 LP

Runoff = 0.25 cfs @ 12.07 hrs, Volume= 0.019 af, Depth> 4.15"



Summary for Subcatchment 2WS: 2 WS

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 3BW: 3 BW

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 3LP: 3 LP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 4BW: 4 BW

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 4LP: 4 LP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 4WS: 4 WS

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 5BW: 5 BW

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



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Summary for Subcatchment 5LP: 5LP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 6BW: 6 BW

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 6LP: 6 LP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 6WS: 6 WS

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 7LP: 7 LP

Runoff = 0.25 cfs @ 12.07 hrs, Volume= 0.019 af, Depth> 4.15"



Summary for Subcatchment 8LP: 8 LP

Runoff = 0.32 cfs @ 12.07 hrs, Volume= 0.024 af, Depth> 4.15"



Summary for Subcatchment 10WS: 10 WS

Runoff = 0.25 cfs @ 12.07 hrs, Volume= 0.019 af, Depth> 4.15"



Summary for Subcatchment 12WP: 12 WP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 12WS: 12 WS

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 14WP: 14 WP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 14WS: 14 WS

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 16WP: 16 WP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 16WS: 16 WS

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 18WP: 18 WP

Runoff = 0.32 cfs @ 12.07 hrs, Volume= 0.024 af, Depth> 4.15"



Summary for Subcatchment 18WS: 18 WS

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 19WP: 19 WP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 20WP: 20 WP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 20WS: 20 WS

Runoff = 0.25 cfs @ 12.07 hrs, Volume= 0.019 af, Depth> 4.15"



Summary for Subcatchment 21WP: 21 WP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 22WP: 22 WP

Runoff = 0.32 cfs @ 12.07 hrs, Volume= 0.024 af, Depth> 4.15"


Summary for Subcatchment 22WS: 22 WS

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 23WP: 23 WP

Runoff = 0.25 cfs @ 12.07 hrs, Volume= 0.019 af, Depth> 4.15"



Summary for Subcatchment 24WS: 24 WS

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 25WP: 25 WP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 26WS: 26 WS

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 27WP: 27 WP

Runoff = 0.25 cfs @ 12.07 hrs, Volume= 0.019 af, Depth> 4.15"



Summary for Subcatchment 28WS: 28 WS

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 29WP: 29 WP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 30WS: 30 WS

Runoff = 0.25 cfs @ 12.07 hrs, Volume= 0.019 af, Depth> 4.15"



Summary for Subcatchment 31WP: 31 WP

Runoff = 0.28 cfs @ 12.07 hrs, Volume= 0.021 af, Depth> 4.15"



Summary for Subcatchment 33WP: 33 WP

Runoff = 0.32 cfs @ 12.07 hrs, Volume= 0.024 af, Depth> 4.15"



Summary for Subcatchment 88S: 8WS

Runoff = 0.25 cfs @ 12.07 hrs, Volume= 0.019 af, Depth> 4.15"



Summary for Subcatchment CEC: Central East - Campus

Runoff = 1.82 cfs @ 12.07 hrs, Volume= 0.136 af, Depth> 4.15"



Summary for Subcatchment CWC: Central West - Campus

Runoff = 3.82 cfs @ 12.07 hrs, Volume= 0.285 af, Depth> 4.15"

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8

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10

11

12

Time (hours)

13

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.70"



14

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20

Summary for Subcatchment ILC: IL Attached - Campus - 6 units (center)

Runoff = 1.82 cfs @ 12.07 hrs, Volume= 0.136 af, Depth> 4.15"



Summary for Subcatchment ILE: IL Attached - Campus - 3 units (east)

Runoff = 0.91 cfs @ 12.07 hrs, Volume= 0.068 af, Depth> 4.15"



Summary for Subcatchment ILW: IL Attached - Campus - 6 units (west)

Runoff = 1.80 cfs @ 12.07 hrs, Volume= 0.135 af, Depth> 4.15"



Summary for Subcatchment NC: North - Campus

Runoff = 3.37 cfs @ 12.07 hrs, Volume= 0.252 af, Depth> 4.15"



Summary for Pond IT 22: 20 CULTEC R-330XL

Inflow Area	a =	0.190 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.15"	for 10-Y	ear event	
Inflow	=	0.88 cfs @	12.07 hrs,	Volume	= 0.066	af			
Outflow	=	0.06 cfs @	13.17 hrs,	Volume	= 0.057	af, Atte	en= 93%,	Lag= 65.7	min
Discarded	=	0.06 cfs @	13.17 hrs,	Volume	= 0.057	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.79' @ 13.17 hrs Surf.Area= 860 sf Storage= 1,233 cf

Plug-Flow detention time= 151.7 min calculated for 0.056 af (86% of inflow) Center-of-Mass det. time= 109.0 min (843.8 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	955 cf	22.33'W x 38.50'L x 4.04'H Field A
			3,475 cf Overall - 1,088 cf Embedded = 2,387 cf x 40.0% Voids
#2A	176.46'	1,088 cf	Cultec R-330XL x 20 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 4 rows
		2,043 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.06 cfs	@ 13.17 hrs HW=177.79' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.06 cfs)

Pond IT 22: 20 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 4 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 4 Rows x 52.0" Wide + 12.0" Spacing x 3 + 12.0" Side Stone x 2 = 22.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

20 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 4 Rows = 1,087.8 cf Chamber Storage

3,475.2 cf Field - 1,087.8 cf Chambers = 2,387.3 cf Stone x 40.0% Voids = 954.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,042.8 cf = 0.047 af Overall Storage Efficiency = 58.8%

20 Chambers 128.7 cy Field 88.4 cy Stone







Pond IT 22: 20 CULTEC R-330XL

Summary for Pond IT10: 12 CULTEC R-330XL

Inflow Area	=	0.121 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.15"	for 10-Y	ear event	
Inflow	=	0.56 cfs @	12.07 hrs,	Volume	= 0.042	af			
Outflow	=	0.04 cfs @	13.07 hrs,	Volume	= 0.037	af, Atte	en= 92%,	Lag= 60.1 i	min
Discarded	=	0.04 cfs @	13.07 hrs,	Volume	= 0.037	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 181.84' @ 13.07 hrs Surf.Area= 536 sf Storage= 781 cf

Plug-Flow detention time= 149.0 min calculated for 0.037 af (88% of inflow) Center-of-Mass det. time= 110.5 min (845.2 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	179.46'	602 cf	17.00'W x 31.50'L x 4.04'H Field A
			2,164 cf Overall - 659 cf Embedded = 1,505 cf x 40.0% Voids
#2A	180.46'	659 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,261 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	179.46'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.04 cfs	a @ 13.07 hrs HW=181.84' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Pond IT10: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 659.4 cf Chamber Storage

2,164.3 cf Field - 659.4 cf Chambers = 1,504.9 cf Stone x 40.0% Voids = 602.0 cf Stone Storage

Chamber Storage + Stone Storage = 1,261.4 cf = 0.029 af Overall Storage Efficiency = 58.3%

12 Chambers 80.2 cy Field 55.7 cy Stone







Pond IT10: 12 CULTEC R-330XL

Summary for Pond IT11: 28 CULTEC R-330XL

Inflow Area	ι =	0.242 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.15"	for 10-Y	ear event
Inflow	=	1.12 cfs @	12.07 hrs,	Volume	= 0.084	l af		
Outflow	=	0.08 cfs @	13.10 hrs,	Volume	= 0.075	5 af, Att	en= 93%,	Lag= 62.0 min
Discarded	=	0.08 cfs @	13.10 hrs,	Volume	= 0.075	5 af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 181.08' @ 13.10 hrs Surf.Area= 1,207 sf Storage= 1,532 cf

Plug-Flow detention time= 146.5 min calculated for 0.075 af (89% of inflow) Center-of-Mass det. time= 111.0 min (845.8 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.98'	1,337 cf	38.33'W x 31.50'L x 4.04'H Field A
			4,880 cf Overall - 1,539 cf Embedded = 3,342 cf x 40.0% Voids
#2A	179.98'	1,539 cf	Cultec R-330XL x 28 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 7 rows
		2,875 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	178.98'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.08 cfs	@ 13.10 hrs HW=181.08' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond IT11: 28 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 7 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 7 Rows x 52.0" Wide + 12.0" Spacing x 6 + 12.0" Side Stone x 2 = 38.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

28 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 7 Rows = 1,538.6 cf Chamber Storage

4,880.3 cf Field - 1,538.6 cf Chambers = 3,341.7 cf Stone x 40.0% Voids = 1,336.7 cf Stone Storage

Chamber Storage + Stone Storage = 2,875.3 cf = 0.066 af Overall Storage Efficiency = 58.9%

28 Chambers 180.8 cy Field 123.8 cy Stone





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Pond IT11: 28 CULTEC R-330XL

Summary for Pond IT11A: 6 CULTEC R-330XL

Inflow Area	=	0.061 ac,10	0.00% Impe	ervious,	Inflow	Depth >	4.15"	for 10)-Year e	vent
Inflow	=	0.28 cfs @	12.07 hrs,	Volume	=	0.021	af			
Outflow	=	0.02 cfs @	12.96 hrs,	Volume	=	0.020	af, At	ten= 91°	%, Lag=	53.5 min
Discarded	=	0.02 cfs @	12.96 hrs,	Volume	=	0.020	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 183.43' @ 12.96 hrs Surf.Area= 280 sf Storage= 377 cf

Plug-Flow detention time= 136.2 min calculated for 0.020 af (94% of inflow) Center-of-Mass det. time= 113.0 min (847.7 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	181.21'	314 cf	16.00'W x 17.50'L x 4.04'H Field A
			1,132 cf Overall - 346 cf Embedded = 785 cf x 40.0% Voids
#2A	182.21'	346 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		661 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	181.21'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Exf	Max=0.02 cfs	a @ 12.96 hrs HW=183.43' (Free Discharge) trols 0.02 cfs)

Pond IT11A: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

2 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 15.50' Row Length +12.0" End Stone x 2 = 17.50' Base Length 3 Rows x 52.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 16.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 346.5 cf Chamber Storage

1,131.7 cf Field - 346.5 cf Chambers = 785.2 cf Stone x 40.0% Voids = 314.1 cf Stone Storage

Chamber Storage + Stone Storage = 660.5 cf = 0.015 af Overall Storage Efficiency = 58.4%

6 Chambers 41.9 cy Field 29.1 cy Stone







Pond IT11A: 6 CULTEC R-330XL

Summary for Pond IT12: 14 CULTEC R-330XL

Inflow Area	ι =	0.129 ac,10	0.00% Impe	ervious,	Inflow Depth	h > 4.1	5" for	10-Ye	ar event	
Inflow	=	0.60 cfs @	12.07 hrs,	Volume	= 0.0	045 af				
Outflow	=	0.05 cfs @	12.99 hrs,	Volume	= 0.0	042 af,	Atten= 9	2%, L	.ag= 54.9	min
Discarded	=	0.05 cfs @	12.99 hrs,	Volume	= 0.0	042 af			-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 181.15' @ 12.99 hrs Surf.Area= 613 sf Storage= 806 cf

Plug-Flow detention time= 137.9 min calculated for 0.042 af (93% of inflow) Center-of-Mass det. time= 112.9 min (847.7 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.96'	689 cf	11.67'W x 52.50'L x 4.04'H Field A
			2,476 cf Overall - 753 cf Embedded = 1,723 cf x 40.0% Voids
#2A	179.96'	753 cf	Cultec R-330XL x 14 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,442 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	178.96'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.05 cfs	@ 12.99 hrs HW=181.15' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.05 cfs)

Pond IT12: 14 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

14 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 752.6 cf Chamber Storage

2,475.5 cf Field - 752.6 cf Chambers = 1,723.0 cf Stone x 40.0% Voids = 689.2 cf Stone Storage

Chamber Storage + Stone Storage = 1,441.7 cf = 0.033 af Overall Storage Efficiency = 58.2%

14 Chambers 91.7 cy Field 63.8 cy Stone







Pond IT12: 14 CULTEC R-330XL

Summary for Pond IT13: 12 CULTEC R-330XL

Inflow Area	ι =	0.116 ac,10	0.00% Impe	ervious,	Inflow Depth :	> 4.15	5" for	10-Ye	ar event	
Inflow	=	0.54 cfs @	12.07 hrs,	Volume	= 0.04	l0 af				
Outflow	=	0.04 cfs @	13.00 hrs,	Volume	= 0.03	87 af, A	Atten= 9	2%, L	.ag= 55.5	min
Discarded	=	0.04 cfs @	13.00 hrs,	Volume	= 0.03	87 af				

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.47' @ 13.00 hrs Surf.Area= 531 sf Storage= 727 cf

Plug-Flow detention time= 140.9 min calculated for 0.037 af (92% of inflow) Center-of-Mass det. time= 112.5 min (847.2 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.21'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	177.21'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.21'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.04 cfs	@ 13.00 hrs HW=178.47' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Pond IT13: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT13: 12 CULTEC R-330XL
Summary for Pond IT14: 12 CULTEC R-330XL

Inflow Area	=	0.116 ac,10	0.00% Impe	ervious,	Inflow Dep	oth > 4	4.15" fo	or 10-Ye	ear event	
Inflow	=	0.54 cfs @	12.07 hrs,	Volume	= (0.040 at	f			
Outflow	=	0.04 cfs @	13.00 hrs,	Volume	= (0.037 at	f, Atten:	= 92%,	Lag= 55.5 n	nin
Discarded	=	0.04 cfs @	13.00 hrs,	Volume	= (0.037 at	f			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.22' @ 13.00 hrs Surf.Area= 531 sf Storage= 727 cf

Plug-Flow detention time= 140.9 min calculated for 0.037 af (92% of inflow) Center-of-Mass det. time= 112.5 min (847.2 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.96'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	176.96'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.96'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.04 cfs	@ 13.00 hrs HW=178.22' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Pond IT14: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT14: 12 CULTEC R-330XL

Summary for Pond IT15: 14 CULTEC R-330XL

Inflow Area	ι =	0.129 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.15"	for 10-Y	ear event
Inflow	=	0.60 cfs @	12.07 hrs,	Volume	= 0.045	5 af		
Outflow	=	0.05 cfs @	12.99 hrs,	Volume	= 0.042	2 af, Atte	en= 92%,	Lag= 54.9 min
Discarded	=	0.05 cfs @	12.99 hrs,	Volume	= 0.042	2 af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.85' @ 12.99 hrs Surf.Area= 613 sf Storage= 806 cf

Plug-Flow detention time= 137.9 min calculated for 0.042 af (93% of inflow) Center-of-Mass det. time= 112.9 min (847.7 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.66'	689 cf	11.67'W x 52.50'L x 4.04'H Field A
			2,476 cf Overall - 753 cf Embedded = 1,723 cf x 40.0% Voids
#2A	177.66'	753 cf	Cultec R-330XL x 14 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,442 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	176.66'	2.410 in/hr Exfiltration over Wetted area	
Discard	ed OutFlow I filtration (Ext	Max=0.05 cfs filtration Cont	@ 12.99 hrs HW=178.85' (Free Discharge) rols 0.05 cfs)	

Pond IT15: 14 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

14 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 752.6 cf Chamber Storage

2,475.5 cf Field - 752.6 cf Chambers = 1,723.0 cf Stone x 40.0% Voids = 689.2 cf Stone Storage

Chamber Storage + Stone Storage = 1,441.7 cf = 0.033 af Overall Storage Efficiency = 58.2%

14 Chambers 91.7 cy Field 63.8 cy Stone







Pond IT15: 14 CULTEC R-330XL

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Summary for Pond IT16: 45 - 330XL

Inflow Area	1 =	0.394 ac,10	0.00% Impe	ervious,	Inflow	Depth >	4.15	5" for	10-Y	ear eve	ent
Inflow	=	1.82 cfs @	12.07 hrs,	Volume	=	0.136	af				
Outflow	=	0.13 cfs @	13.29 hrs,	Volume	=	0.115	af, A	Atten=	93%,	Lag= 7	'3.2 min
Discarded	=	0.13 cfs @	13.29 hrs,	Volume	=	0.115	af				

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.71' @ 13.29 hrs Surf.Area= 1,840 sf Storage= 2,564 cf

Plug-Flow detention time= 153.2 min calculated for 0.115 af (84% of inflow) Center-of-Mass det. time= 107.5 min (842.3 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	2,013 cf	27.67'W x 66.50'L x 4.04'H Field A
			7,436 cf Overall - 2,403 cf Embedded = 5,033 cf x 40.0% Voids
#2A	176.46'	2,403 cf	Cultec R-330XL x 45 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 5 rows
		4,416 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow I filtration (Exi	Max=0.13 cfs filtration Cont	@ 13.29 hrs HW=177.71' (Free Discharge) rols 0.13 cfs)

Pond IT16: 45 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 5 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 5 Rows x 52.0" Wide + 12.0" Spacing x 4 + 12.0" Side Stone x 2 = 27.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

45 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 5 Rows = 2,402.9 cf Chamber Storage

7,436.0 cf Field - 2,402.9 cf Chambers = 5,033.0 cf Stone x 40.0% Voids = 2,013.2 cf Stone Storage

Chamber Storage + Stone Storage = 4,416.2 cf = 0.101 af Overall Storage Efficiency = 59.4%

45 Chambers 275.4 cy Field 186.4 cy Stone





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Pond IT16: 45 - 330XL

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Summary for Pond IT17: 24 - 330XL

Inflow Area	ι =	0.197 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.15"	for 10-Ye	ear event
Inflow	=	0.91 cfs @	12.07 hrs,	Volume	= 0.068	3 af		
Outflow	=	0.07 cfs @	13.03 hrs,	Volume	= 0.063	3 af, At	tten= 92%,	Lag= 57.6 min
Discarded	=	0.07 cfs @	13.03 hrs,	Volume	= 0.063	3 af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 174.93' @ 13.03 hrs Surf.Area= 1,040 sf Storage= 1,213 cf

Plug-Flow detention time= 138.7 min calculated for 0.063 af (93% of inflow) Center-of-Mass det. time= 113.5 min (848.2 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	172.96'	1,153 cf	33.00'W x 31.50'L x 4.04'H Field A
			4,201 cf Overall - 1,319 cf Embedded = 2,882 cf x 40.0% Voids
#2A	173.96'	1,319 cf	Cultec R-330XL x 24 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		2,472 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	172.96'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.07 cfs	@ 13.03 hrs HW=174.93' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.07 cfs)

Pond IT17: 24 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

24 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 1,318.8 cf Chamber Storage

4,201.3 cf Field - 1,318.8 cf Chambers = 2,882.5 cf Stone x 40.0% Voids = 1,153.0 cf Stone Storage

Chamber Storage + Stone Storage = 2,471.8 cf = 0.057 af Overall Storage Efficiency = 58.8%

24 Chambers 155.6 cy Field 106.8 cy Stone





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Pond IT17: 24 - 330XL

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Summary for Pond IT18: 48 - 330XL

Inflow Area	a =	0.394 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.15	5" for	10-Ye	ar event	
Inflow	=	1.82 cfs @	12.07 hrs,	Volume=	= 0.130	6 af				
Outflow	=	0.13 cfs @	13.18 hrs,	Volume=	= 0.11	9 af, <i>1</i>	Atten= 9	3%, L	.ag= 66.7	min
Discarded	=	0.13 cfs @	13.18 hrs,	Volume=	= 0.119	9 af			-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 175.56' @ 13.18 hrs Surf.Area= 1,964 sf Storage= 2,508 cf

Plug-Flow detention time= 149.7 min calculated for 0.119 af (88% of inflow) Center-of-Mass det. time= 109.8 min (844.5 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	173.46'	2,146 cf	33.00'W x 59.50'L x 4.04'H Field A
			7,936 cf Overall - 2,571 cf Embedded = 5,365 cf x 40.0% Voids
#2A	174.46'	2,571 cf	Cultec R-330XL x 48 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		4,717 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	173.46'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow	Max=0.13 cfs	@ 13.18 hrs HW=175.56' (Free Discharge)	

1=Exfiltration (Exfiltration Controls 0.13 cfs)

Pond IT18: 48 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

48 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 2,570.6 cf Chamber Storage

7,935.8 cf Field - 2,570.6 cf Chambers = 5,365.2 cf Stone x 40.0% Voids = 2,146.1 cf Stone Storage

Chamber Storage + Stone Storage = 4,716.7 cf = 0.108 af Overall Storage Efficiency = 59.4%

48 Chambers 293.9 cy Field 198.7 cy Stone





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Pond IT18: 48 - 330XL

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Summary for Pond IT19: 48 - 330XL

Inflow Area	ι =	0.390 ac,10	0.00% Impe	ervious,	Inflow	Depth >	4.15	for	10-Ye	ear even	t
Inflow	=	1.80 cfs @	12.07 hrs,	Volume	=	0.135	af				
Outflow	=	0.13 cfs @	13.16 hrs,	Volume	=	0.119	af, A	tten= 9)3%, I	Lag= 65	.6 min
Discarded	=	0.13 cfs @	13.16 hrs,	Volume	=	0.119	af				

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 173.33' @ 13.16 hrs Surf.Area= 1,964 sf Storage= 2,477 cf

Plug-Flow detention time= 148.9 min calculated for 0.119 af (88% of inflow) Center-of-Mass det. time= 110.1 min (844.9 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	171.25'	2,146 cf	33.00'W x 59.50'L x 4.04'H Field A
			7,936 cf Overall - 2,571 cf Embedded = 5,365 cf x 40.0% Voids
#2A	172.25'	2,571 cf	Cultec R-330XL x 48 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		4,717 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	171.25'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.13 cfs	@ 13.16 hrs HW=173.33' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.13 cfs)

Pond IT19: 48 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

48 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 2,570.6 cf Chamber Storage

7,935.8 cf Field - 2,570.6 cf Chambers = 5,365.2 cf Stone x 40.0% Voids = 2,146.1 cf Stone Storage

Chamber Storage + Stone Storage = 4,716.7 cf = 0.108 af Overall Storage Efficiency = 59.4%

48 Chambers 293.9 cy Field 198.7 cy Stone





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Pond IT19: 48 - 330XL

Summary for Pond IT20: 100 - 330XL

Inflow Area	ι =	0.826 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.15"	for 10-Y	ear event
Inflow	=	3.82 cfs @	12.07 hrs,	Volume=	= 0.285	af		
Outflow	=	0.25 cfs @	13.41 hrs,	Volume=	= 0.238	af, Atte	en= 93%,	Lag= 80.4 min
Discarded	=	0.25 cfs @	13.41 hrs,	Volume=	= 0.238	af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.64' @ 13.41 hrs Surf.Area= 3,994 sf Storage= 5,403 cf

Plug-Flow detention time= 154.3 min calculated for 0.237 af (83% of inflow) Center-of-Mass det. time= 105.8 min (840.6 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	4,325 cf	54.33'W x 73.50'L x 4.04'H Field A
			16,140 cf Overall - 5,327 cf Embedded = 10,813 cf x 40.0% Voids
#2A	176.46'	5,327 cf	Cultec R-330XL x 100 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 10 rows
		9,653 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Exf	Max=0.25 cfs	@ 13.41 hrs HW=177.64' (Free Discharge) rols 0.25 cfs)

Pond IT20: 100 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 10 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

10 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 71.50' Row Length +12.0" End Stone x 2 = 73.50' Base Length 10 Rows x 52.0" Wide + 12.0" Spacing x 9 + 12.0" Side Stone x 2 = 54.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

100 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 10 Rows = 5,327.5 cf Chamber Storage

16,140.4 cf Field - 5,327.5 cf Chambers = 10,812.9 cf Stone x 40.0% Voids = 4,325.2 cf Stone Storage

Chamber Storage + Stone Storage = 9,652.6 cf = 0.222 af Overall Storage Efficiency = 59.8%

100 Chambers 597.8 cy Field 400.5 cy Stone





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Pond IT20: 100 - 330XL

Summary for Pond IT21: 25 CULTEC R-330XL

Inflow Area	=	0.237 ac,10	0.00% Impe	ervious,	Inflow De	pth >	4.15"	for 10-Y	ear event
Inflow	=	1.10 cfs @	12.07 hrs,	Volume	=	0.082	af		
Outflow	=	0.08 cfs @	13.26 hrs,	Volume	=	0.069	af, Atte	en= 93%,	Lag= 71.5 min
Discarded	=	0.08 cfs @	13.26 hrs,	Volume	=	0.069	af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 172.04' @ 13.26 hrs Surf.Area= 1,065 sf Storage= 1,551 cf

Plug-Flow detention time= 153.8 min calculated for 0.069 af (84% of inflow) Center-of-Mass det. time= 107.7 min (842.4 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	169.69'	1,178 cf	27.67'W x 38.50'L x 4.04'H Field A
			4,305 cf Overall - 1,360 cf Embedded = 2,945 cf x 40.0% Voids
#2A	170.69'	1,360 cf	Cultec R-330XL x 25 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 5 rows
		2,538 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	169.69'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.08 cfs	@ 13.26 hrs HW=172.04' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond IT21: 25 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 5 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 5 Rows x 52.0" Wide + 12.0" Spacing x 4 + 12.0" Side Stone x 2 = 27.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

25 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 5 Rows = 1,359.8 cf Chamber Storage

4,305.0 cf Field - 1,359.8 cf Chambers = 2,945.2 cf Stone x 40.0% Voids = 1,178.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,537.9 cf = 0.058 af Overall Storage Efficiency = 59.0%

25 Chambers 159.4 cy Field 109.1 cy Stone





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Pond IT21: 25 CULTEC R-330XL

Summary for Pond IT22A: 6 CULTEC R-330XL

Inflow Area	ι =	0.055 ac,10	0.00% Impe	ervious,	Inflow Depth :	> 4.1	5" for	10-Ye	ear event	
Inflow	=	0.25 cfs @	12.07 hrs,	Volume	= 0.01	9 af				
Outflow	=	0.03 cfs @	12.78 hrs,	Volume	= 0.01	9 af,	Atten= 9	90%,	Lag= 42.7	min
Discarded	=	0.03 cfs @	12.78 hrs,	Volume	= 0.01	9 af			-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.19' @ 12.78 hrs Surf.Area= 288 sf Storage= 320 cf

Plug-Flow detention time= 103.0 min calculated for 0.019 af (100% of inflow) Center-of-Mass det. time= 102.0 min (836.8 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	177.46'	279 cf	6.33'W x 45.50'L x 3.54'H Field A
			1,021 cf Overall - 324 cf Embedded = 696 cf x 40.0% Voids
#2A	177.96'	324 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 1 rows
		603 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	177.46'	2.410 in/hr Exfiltration over Wetted area	
Discard	ed OutFlow I filtration (Ext	Max=0.03 cfs filtration Cont	@ 12.78 hrs HW=179.19' (Free Discharge) rols 0.03 cfs)	

Pond IT22A: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 1 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 1 Rows x 52.0" Wide + 12.0" Side Stone x 2 = 6.33' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 1 Rows = 324.1 cf Chamber Storage

1,020.6 cf Field - 324.1 cf Chambers = 696.5 cf Stone x 40.0% Voids = 278.6 cf Stone Storage

Chamber Storage + Stone Storage = 602.7 cf = 0.014 af Overall Storage Efficiency = 59.1%

6 Chambers 37.8 cy Field 25.8 cy Stone







Pond IT22A: 6 CULTEC R-330XL

Summary for Pond IT23: 88 - 330XL

Inflow Area	a =	0.729 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.1	5" for	10-Ye	ear event	
Inflow	=	3.37 cfs @	12.07 hrs,	Volume	= 0.252	af				
Outflow	=	0.23 cfs @	13.37 hrs,	Volume	= 0.212	af, /	Atten= 9	93%,	Lag= 78.	3 min
Discarded	=	0.23 cfs @	13.37 hrs,	Volume	= 0.212	af			-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.63' @ 13.37 hrs Surf.Area= 3,550 sf Storage= 4,742 cf

Plug-Flow detention time= 153.6 min calculated for 0.211 af (84% of inflow) Center-of-Mass det. time= 106.5 min (841.3 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	3,854 cf	59.67'W x 59.50'L x 4.04'H Field A
			14,349 cf Overall - 4,713 cf Embedded = 9,636 cf x 40.0% Voids
#2A	176.46'	4,713 cf	Cultec R-330XL x 88 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 11 rows
		8,567 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Ext	Max=0.23 cfs	@ 13.37 hrs HW=177.63' (Free Discharge) trols 0.23 cfs)

Pond IT23: 88 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 11 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 11 Rows x 52.0" Wide + 12.0" Spacing x 10 + 12.0" Side Stone x 2 = 59.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

88 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 11 Rows = 4,712.8 cf Chamber Storage

14,348.6 cf Field - 4,712.8 cf Chambers = 9,635.8 cf Stone x 40.0% Voids = 3,854.3 cf Stone Storage

Chamber Storage + Stone Storage = 8,567.1 cf = 0.197 af Overall Storage Efficiency = 59.7%

88 Chambers 531.4 cy Field 356.9 cy Stone





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Pond IT23: 88 - 330XL

Summary for Pond IT24: 8 CULTEC R-330XL

Inflow Area	a =	0.069 ac,10	0.00% Impe	ervious,	Inflow	Depth >	4.15	" for	10-Ye	ar event	
Inflow	=	0.32 cfs @	12.07 hrs,	Volume	=	0.024	af				
Outflow	=	0.03 cfs @	12.93 hrs,	Volume	=	0.023	af, A	tten= 9	91%, L	_ag= 51.	8 min
Discarded	=	0.03 cfs @	12.93 hrs,	Volume	=	0.023	af			-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 177.98' @ 12.93 hrs Surf.Area= 352 sf Storage= 416 cf

Plug-Flow detention time= 126.8 min calculated for 0.023 af (97% of inflow) Center-of-Mass det. time= 113.5 min (848.2 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.21'	322 cf	11.17'W x 31.50'L x 3.54'H Field A
			1,246 cf Overall - 440 cf Embedded = 806 cf x 40.0% Voids
#2A	176.71'	440 cf	Cultec R-330XL x 8 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		762 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.21'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Ext	Max=0.03 cfs	@ 12.93 hrs HW=177.98' (Free Discharge) rols 0.03 cfs)

Pond IT24: 8 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 2 Rows x 52.0" Wide + 6.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.17' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

8 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 439.6 cf Chamber Storage

1,245.8 cf Field - 439.6 cf Chambers = 806.2 cf Stone x 40.0% Voids = 322.5 cf Stone Storage

Chamber Storage + Stone Storage = 762.1 cf = 0.017 afOverall Storage Efficiency = 61.2%

8 Chambers 46.1 cy Field 29.9 cy Stone







Pond IT24: 8 CULTEC R-330XL

Summary for Pond IT25: 12 CULTEC R-330XL

Inflow Area	ι =	0.121 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.15"	for 10-Y	ear event	
Inflow	=	0.56 cfs @	12.07 hrs,	Volume	= 0.042	af			
Outflow	=	0.04 cfs @	13.02 hrs,	Volume	= 0.038	af, Atte	en= 92%,	Lag= 57.1 r	min
Discarded	=	0.04 cfs @	13.02 hrs,	Volume	= 0.038	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 189.84' @ 13.02 hrs Surf.Area= 531 sf Storage= 774 cf

Plug-Flow detention time= 145.8 min calculated for 0.038 af (90% of inflow) Center-of-Mass det. time= 111.6 min (846.4 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	187.46'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	188.46'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	187.46'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow	Max=0.04 cfs	@ 13.02 hrs HW=189.84' (Free Discharge)	

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Pond IT25: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT25: 12 CULTEC R-330XL
Summary for Pond IT26: 18 CULTEC R-330XL

Inflow Area	ι =	0.171 ac,10	0.00% Impe	ervious,	Inflow E	Depth >	4.15"	for 1	0-Year eve	nt
Inflow	=	0.79 cfs @	12.07 hrs,	Volume	=	0.059	af			
Outflow	=	0.06 cfs @	13.10 hrs,	Volume	=	0.052	af, Att	en= 92'	%, Lag= 6	1.5 min
Discarded	=	0.06 cfs @	13.10 hrs,	Volume	=	0.052	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 185.17' @ 13.10 hrs Surf.Area= 774 sf Storage= 1,099 cf

Plug-Flow detention time= 149.9 min calculated for 0.052 af (88% of inflow) Center-of-Mass det. time= 110.2 min (845.0 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	182.86'	862 cf	17.00'W x 45.50'L x 4.04'H Field A
			3,126 cf Overall - 972 cf Embedded = 2,154 cf x 40.0% Voids
#2A	183.86'	972 cf	Cultec R-330XL x 18 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,834 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	182.86'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow	Max=0.06 cfs	s @ 13.10 hrs HW=185.17' (Free Discharge)	

1=Exfiltration (Exfiltration Controls 0.06 cfs)

Pond IT26: 18 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

18 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 972.4 cf Chamber Storage

3,126.2 cf Field - 972.4 cf Chambers = 2,153.9 cf Stone x 40.0% Voids = 861.5 cf Stone Storage

Chamber Storage + Stone Storage = 1,833.9 cf = 0.042 af Overall Storage Efficiency = 58.7%

18 Chambers 115.8 cy Field 79.8 cy Stone







Pond IT26: 18 CULTEC R-330XL

Summary for Pond IT29: 27 CULTEC R-330XL

Inflow Area	ι =	0.242 ac,10	0.00% Impe	ervious,	Inflow I	Depth >	4.15"	for '	10-Yea	ar event	
Inflow	=	1.12 cfs @	12.07 hrs,	Volume	=	0.084	af				
Outflow	=	0.08 cfs @	13.10 hrs,	Volume	=	0.074	af, Att	en= 93	3%, La	ag= 61.8	min
Discarded	=	0.08 cfs @	13.10 hrs,	Volume	=	0.074	af			-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 185.70' @ 13.10 hrs Surf.Area= 1,131 sf Storage= 1,552 cf

Plug-Flow detention time= 148.6 min calculated for 0.074 af (88% of inflow) Center-of-Mass det. time= 110.4 min (845.2 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	183.46'	1,251 cf	17.00'W x 66.50'L x 4.04'H Field A
			4,569 cf Overall - 1,442 cf Embedded = 3,127 cf x 40.0% Voids
#2A	184.46'	1,442 cf	Cultec R-330XL x 27 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		2,693 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	183.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.08 cfs	@ 13.10 hrs HW=185.70' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond IT29: 27 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

27 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 1,441.8 cf Chamber Storage

4,569.1 cf Field - 1,441.8 cf Chambers = 3,127.3 cf Stone x 40.0% Voids = 1,250.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,692.7 cf = 0.062 af Overall Storage Efficiency = 58.9%

27 Chambers 169.2 cy Field 115.8 cy Stone





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Pond IT29: 27 CULTEC R-330XL

Summary for Pond IT30: 15 CULTEC R-330XL

Inflow Area	a =	0.116 ac,10	0.00% Impe	ervious, l	Inflow Depth >	4.15"	for 10-Y	ear event
Inflow	=	0.54 cfs @	12.07 hrs,	Volume=	.0.040	af		
Outflow	=	0.05 cfs @	12.92 hrs,	Volume=	: 0.040	af, Atte	en= 91%,	Lag= 51.0 min
Discarded	=	0.05 cfs @	12.92 hrs,	Volume=	: 0.040	af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 182.78' @ 12.92 hrs Surf.Area= 655 sf Storage= 684 cf

Plug-Flow detention time= 116.6 min calculated for 0.040 af (99% of inflow) Center-of-Mass det. time= 115.0 min (849.7 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	180.96'	732 cf	17.00'W x 38.50'L x 4.04'H Field A
			2,645 cf Overall - 816 cf Embedded = 1,829 cf x 40.0% Voids
#2A	181.96'	816 cf	Cultec R-330XL x 15 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,548 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	180.96'	2.410 in/hr Exfiltration over Wetted area	
Discard	ed OutFlow M filtration (Ext	Max=0.05 cfs filtration Cont	@ 12.92 hrs HW=182.78' (Free Discharge) rols 0.05 cfs)	

Pond IT30: 15 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

15 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 815.9 cf Chamber Storage

2,645.3 cf Field - 815.9 cf Chambers = 1,829.4 cf Stone x 40.0% Voids = 731.8 cf Stone Storage

Chamber Storage + Stone Storage = 1,547.6 cf = 0.036 af Overall Storage Efficiency = 58.5%

15 Chambers 98.0 cy Field 67.8 cy Stone







Pond IT30: 15 CULTEC R-330XL

Summary for Pond IT31: 27 CULTEC R-330XL

Inflow Area	ι =	0.237 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.15"	for 10-Y	ear event
Inflow	=	1.10 cfs @	12.07 hrs,	Volume	= 0.082	af		
Outflow	=	0.08 cfs @	13.07 hrs,	Volume	= 0.073	af, Att	en= 92%,	Lag= 60.2 min
Discarded	=	0.08 cfs @	13.07 hrs,	Volume	= 0.073	af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.64' @ 13.07 hrs Surf.Area= 1,131 sf Storage= 1,503 cf

Plug-Flow detention time= 146.5 min calculated for 0.073 af (89% of inflow) Center-of-Mass det. time= 111.2 min (845.9 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.46'	1,251 cf	17.00'W x 66.50'L x 4.04'H Field A
			4,569 cf Overall - 1,442 cf Embedded = 3,127 cf x 40.0% Voids
#2A	177.46'	1,442 cf	Cultec R-330XL x 27 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		2,693 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.08 cfs	@ 13.07 hrs HW=178.64' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond IT31: 27 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

27 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 1,441.8 cf Chamber Storage

4,569.1 cf Field - 1,441.8 cf Chambers = 3,127.3 cf Stone x 40.0% Voids = 1,250.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,692.7 cf = 0.062 af Overall Storage Efficiency = 58.9%

27 Chambers 169.2 cy Field 115.8 cy Stone





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Pond IT31: 27 CULTEC R-330XL

Summary for Pond IT8: 20 CULTEC R-330XL

Inflow Area	I =	0.182 ac,10	0.00% Impe	ervious,	Inflow E	Depth >	4.15"	for	10-Ye	ear even	t
Inflow	=	0.84 cfs @	12.07 hrs,	Volume	=	0.063	af				
Outflow	=	0.07 cfs @	13.00 hrs,	Volume	=	0.058	af, At	tten= 9	2%,	Lag= 55	.9 min
Discarded	=	0.07 cfs @	13.00 hrs,	Volume	=	0.058	af				

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.90' @ 13.00 hrs Surf.Area= 858 sf Storage= 1,138 cf

Plug-Flow detention time= 140.5 min calculated for 0.058 af (92% of inflow) Center-of-Mass det. time= 112.7 min (847.4 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	177.71'	960 cf	11.67'W x 73.50'L x 4.04'H Field A
			3,466 cf Overall - 1,065 cf Embedded = 2,400 cf x 40.0% Voids
#2A	178.71'	1,065 cf	Cultec R-330XL x 20 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		2,026 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	177.71'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.07 cfs	s @ 13.00 hrs HW=179.90' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.07 cfs)

Pond IT8: 20 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

10 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 71.50' Row Length +12.0" End Stone x 2 = 73.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

20 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 1,065.5 cf Chamber Storage

3,465.7 cf Field - 1,065.5 cf Chambers = 2,400.2 cf Stone x 40.0% Voids = 960.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,025.6 cf = 0.047 af Overall Storage Efficiency = 58.4%

20 Chambers 128.4 cy Field 88.9 cy Stone







Pond IT8: 20 CULTEC R-330XL

Summary for Pond IT9: 6 CULTEC R-330XL

Inflow Area	ι =	0.055 ac,10	0.00% Impe	ervious,	Inflow [Depth >	4.15"	for	10-Ye	ar even	t
Inflow	=	0.25 cfs @	12.07 hrs,	Volume	=	0.019	af				
Outflow	=	0.02 cfs @	12.94 hrs,	Volume	=	0.018	af, Att	en= 9	1%, l	_ag= 52.	2 min
Discarded	=	0.02 cfs @	12.94 hrs,	Volume	=	0.018	af			-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 180.74' @ 12.94 hrs Surf.Area= 280 sf Storage= 334 cf

Plug-Flow detention time= 128.0 min calculated for 0.018 af (96% of inflow) Center-of-Mass det. time= 113.3 min (848.1 - 734.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.96'	258 cf	16.00'W x 17.50'L x 3.54'H Field A
			992 cf Overall - 346 cf Embedded = 645 cf x 40.0% Voids
#2A	179.46'	346 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		605 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	178.96'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow I filtration (Exi	Max=0.02 cfs filtration Cont	@ 12.94 hrs HW=180.74' (Free Discharge) rols 0.02 cfs)

Pond IT9: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

2 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 15.50' Row Length +12.0" End Stone x 2 = 17.50' Base Length 3 Rows x 52.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 16.00' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 346.5 cf Chamber Storage

991.7 cf Field - 346.5 cf Chambers = 645.2 cf Stone x 40.0% Voids = 258.1 cf Stone Storage

Chamber Storage + Stone Storage = 604.5 cf = 0.014 afOverall Storage Efficiency = 61.0%

6 Chambers 36.7 cy Field 23.9 cy Stone







Pond IT9: 6 CULTEC R-330XL

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1BW:1BW	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.30 cfs 0.022 af
Subcatchment1LP:1 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 2BW: 2 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 2LP: 2 LP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.30 cfs 0.022 af
Subcatchment 2WS: 2 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment3BW: 3 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 3LP: 3 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 4BW: 4 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 4LP: 4 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 4WS: 4 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 5BW: 5 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 5LP: 5LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment6BW: 6 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 6LP: 6 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 6WS: 6 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment7LP:7 LP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.30 cfs 0.022 af

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Subcatchment 8LP: 8 LP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.37 cfs 0.028 af
Subcatchment10WS: 10 WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.30 cfs 0.022 af
Subcatchment 12WP: 12 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 12WS: 12 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 14WP: 14 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment14WS:14WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 16WP: 16 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 16WS: 16 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 18WP: 18 WP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.37 cfs 0.028 af
Subcatchment 18WS: 18 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 19WP: 19 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 20WP: 20 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 20WS: 20 WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.30 cfs 0.022 af
Subcatchment 21WP: 21 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 22WP: 22 WP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.37 cfs 0.028 af
Subcatchment 22WS: 22 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 23WP: 23 WP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.30 cfs 0.022 af
Subcatchment 24WS: 24 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af

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Subcatchment 25WP: 25 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 26WS: 26 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 27WP: 27 WP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.30 cfs 0.022 af
Subcatchment 28WS: 28 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 29WP: 29 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 30WS: 30 WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.30 cfs 0.022 af
Subcatchment31WP: 31 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.33 cfs 0.025 af
Subcatchment 33WP: 33 WP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.37 cfs 0.028 af
Subcatchment 88S: 8WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=0.30 cfs 0.022 af
Subcatchment CEC: Central East -	Runoff Area=17,152 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=2.13 cfs 0.160 af
Subcatchment CWC: Central West -	Runoff Area=36,000 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=4.48 cfs 0.336 af
Subcatchment ILC: IL Attached - Campus	Runoff Area=17,150 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=2.13 cfs 0.160 af
Subcatchment ILE: IL Attached - Campus	- Runoff Area=8,575 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=1.07 cfs 0.080 af
Subcatchment ILW: IL Attached - Campus	s Runoff Area=17,000 sf 100.00% Impervious Runoff Depth>4.87 Tc=5.0 min CN=98 Runoff=2.12 cfs 0.159 af
Subcatchment NC: North - Campus	Runoff Area=31,750 sf 100.00% Impervious Runoff Depth>4.87" Tc=5.0 min CN=98 Runoff=3.95 cfs 0.296 af
Pond IT 22: 20 CULTEC R-330XL	Peak Elev=178.28' Storage=1,534 cf Inflow=1.03 cfs 0.077 af Outflow=0.07 cfs 0.061 af
Pond IT10: 12 CULTEC R-330XL	Peak Elev=182.35' Storage=968 cf Inflow=0.66 cfs 0.049 af Outflow=0.05 cfs 0.040 af

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		<u> </u>
Pond IT11: 28 CULTEC R-330XL	Peak Elev=181.50' Storage=1,911 cf Inflow=1.3	1 cfs 0.098 af
	Outflow=0.0	9 cfs 0.080 af
	Deals Flass 402 001 Otarage 407 of Jufface 0.2	0. ata 0.005 at
Pond II11A: 6 CULTEC R-330XL	Peak Elev=183.88 Storage=467 cf Inflow=0.3	3 CTS 0.025 at
	Outilow=0.c	5 CIS 0.02 I al
Pond IT12: 14 CULTEC R-330XL	Peak Elev=181.59' Storage=1.000 cf Inflow=0.7	0 cfs 0.053 af
	Outflow=0.0	5 cfs 0.045 af
Pond IT13: 12 CULTEC R-330XL	Peak Elev=178.93' Storage=900 cf Inflow=0.6	3 cfs 0.047 af
	Outflow=0.0	5 cfs 0.040 af
	Deals Flave 470 001 Otara and 000 of Jufface 0.0	0 - 1- 0 0 17 - 1
Pond 1114: 12 CULTEC R-330XL	Peak Elev=178.68 Storage=900 cf Inflow=0.6	3 CTS 0.047 at
	Outilow=0.0	5 CIS 0.040 al
Pond IT15: 14 CUI TEC R-330XI	Peak Elev=179.29' Storage=1.000 cf Inflow=0.7	0 cfs 0.053 af
	Outflow=0.0	5 cfs 0.045 af
Pond IT16: 45 - 330XL	Peak Elev=178.19' Storage=3,203 cf Inflow=2.1	3 cfs 0.160 af
	Outflow=0.1	3 cfs 0.123 af
Pond IT17: 24 - 330XL	Peak Elev=175.31' Storage=1,511 ct Inflow=1.0	7 cfs 0.080 af
	Outflow=0.0	7 CIS 0.068 af
Pond IT18: 48 - 330XI	Peak Elev-175 98' Storage-3 135 cf Inflow-2 1	3 cfs 0 160 af
	Outflow=0.1	4 cfs 0.127 af
Pond IT19: 48 - 330XL	Peak Elev=173.75' Storage=3,096 cf Inflow=2.1	2 cfs 0.159 af
	Outflow=0.1	4 cfs 0.126 af
Pond IT20: 100 - 330XL	Peak Elev=178.10' Storage=6,773 ct Inflow=4.4	8 cfs 0.336 at
	Outilow=0.2	.6 CIS 0.251 al
Pond IT21: 25 CI II TEC R-330XI	Peak Elev=172 55' Storage=1 933 cf Inflow=1 2	8 cfs 0 096 af
	Outflow=0.0	8 cfs 0.074 af
Pond IT22A: 6 CULTEC R-330XL	Peak Elev=179.57' Storage=395 cf Inflow=0.3	0 cfs 0.022 af
	Outflow=0.0	3 cfs 0.022 af
		- / /
Pond IT23: 88 - 330XL	Peak Elev=178.08' Storage=5,943 ct Inflow=3.9	5 cfs 0.296 af
	Outflow=0.2	.3 CIS 0.223 af
Pond IT24: 8 CI II TEC R-330XI	Peak Elev=178 37' Storage=516 cf Inflow=0.3	7 cfs 0 028 af
	Outflow=0.0	3 cfs 0.025 af
Pond IT25: 12 CULTEC R-330XL	Peak Elev=190.35' Storage=958 cf Inflow=0.6	6 cfs 0.049 af
	Outflow=0.0	5 cfs 0.041 af
Pond 1126: 18 CULTEC R-330XL	Peak Elev=185.66 Storage=1,365 ct Inflow=0.9	3 CTS 0.069 af
	Outflow=0.0	0 CIS 0.050 AT
Pond IT29: 27 CUI TEC R-330XI	Peak Elev=186.16' Storage=1.930 cf Inflow=1.3	1 cfs_0.098 af
	Outflow=0.0	9 cfs 0.079 af

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Pond IT30: 15 CULTEC R-330XL	Peak Elev=183.12' Storage=851 cf	Inflow=0.63 cfs 0.047 af				
		Juliiow=0.05 CI3 0.045 al				
Pond IT31: 27 CULTEC R-330XL	Peak Elev=179.09' Storage=1,870 cf	Inflow=1.28 cfs 0.096 af				
	C	Outflow=0.09 cfs 0.079 af				
Pond IT8: 20 CULTEC R-330XL	Peak Elev=180.35' Storage=1,411 cf	Inflow=0.99 cfs 0.074 af				
	C C	Outflow=0.07 cfs 0.063 af				
Pond IT9: 6 CULTEC R-330XL	Peak Elev=181.15' Storage=414 cf	Inflow=0.30 cfs 0.022 af				
	(Outflow=0.02 cfs 0.020 af				
Total Punoff Aroa - 5 510 ac	Pupoff Volume - 2 242 of Avera	ao Punoff Donth - 1 87				

Total Runoff Area = 5.519 ac Runoff Volume = 2.242 af Average Runoff Depth = 4.87" 0.00% Pervious = 0.000 ac 100.00% Impervious = 5.519 ac

Summary for Subcatchment 1BW: 1BW

Runoff = 0.30 cfs @ 12.07 hrs, Volume= 0.022 af, Depth> 4.87"



Summary for Subcatchment 1LP: 1 LP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 2BW: 2 BW

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 2LP: 2 LP

Runoff = 0.30 cfs @ 12.07 hrs, Volume= 0.022 af, Depth> 4.87"



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Summary for Subcatchment 2WS: 2 WS

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 3BW: 3 BW

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 3LP: 3 LP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 4BW: 4 BW

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 4LP: 4 LP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



8548.0 - Salmon Senior Community - Medway - Prop Type III 24-hr 25-Year Rainfall=5.50"Prepared by MicrosoftPrinted 10/9/2015HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLCPage 271

Summary for Subcatchment 4WS: 4 WS

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 5BW: 5 BW

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



8548.0 - Salmon Senior Community - Medway - Prop Type III 24-hr 25-Year Rainfall=5.50"Prepared by MicrosoftPrinted 10/9/2015HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLCPage 273

Summary for Subcatchment 5LP: 5LP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 6BW: 6 BW

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"


Summary for Subcatchment 6LP: 6 LP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 6WS: 6 WS

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 7LP: 7 LP

Runoff = 0.30 cfs @ 12.07 hrs, Volume= 0.022 af, Depth> 4.87"



Summary for Subcatchment 8LP: 8 LP

Runoff = 0.37 cfs @ 12.07 hrs, Volume= 0.028 af, Depth> 4.87"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"



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Summary for Subcatchment 10WS: 10 WS

Runoff = 0.30 cfs @ 12.07 hrs, Volume= 0.022 af, Depth> 4.87"



Summary for Subcatchment 12WP: 12 WP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 12WS: 12 WS

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 14WP: 14 WP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 14WS: 14 WS

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 16WP: 16 WP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 16WS: 16 WS

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 18WP: 18 WP

Runoff = 0.37 cfs @ 12.07 hrs, Volume= 0.028 af, Depth> 4.87"





Summary for Subcatchment 18WS: 18 WS

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 19WP: 19 WP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 20WP: 20 WP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 20WS: 20 WS

Runoff = 0.30 cfs @ 12.07 hrs, Volume= 0.022 af, Depth> 4.87"



Summary for Subcatchment 21WP: 21 WP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 22WP: 22 WP

Runoff = 0.37 cfs @ 12.07 hrs, Volume= 0.028 af, Depth> 4.87"





Summary for Subcatchment 22WS: 22 WS

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 23WP: 23 WP

Runoff = 0.30 cfs @ 12.07 hrs, Volume= 0.022 af, Depth> 4.87"



Summary for Subcatchment 24WS: 24 WS

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 25WP: 25 WP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 26WS: 26 WS

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 27WP: 27 WP

Runoff = 0.30 cfs @ 12.07 hrs, Volume= 0.022 af, Depth> 4.87"



Summary for Subcatchment 28WS: 28 WS

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 29WP: 29 WP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 30WS: 30 WS

Runoff = 0.30 cfs @ 12.07 hrs, Volume= 0.022 af, Depth> 4.87"



Summary for Subcatchment 31WP: 31 WP

Runoff = 0.33 cfs @ 12.07 hrs, Volume= 0.025 af, Depth> 4.87"



Summary for Subcatchment 33WP: 33 WP

Runoff = 0.37 cfs @ 12.07 hrs, Volume= 0.028 af, Depth> 4.87"

Area (sf)	CN Description						
3,000	98 Roofs, HSG A						
3,000	100.00% Impervious Area						
Tc Length (min) (feet)	Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs)						
5.0 Direct Entry,							
Subcatchment 33WP: 33 WP							



Summary for Subcatchment 88S: 8WS

Runoff = 0.30 cfs @ 12.07 hrs, Volume= 0.022 af, Depth> 4.87"



Summary for Subcatchment CEC: Central East - Campus

Runoff = 2.13 cfs @ 12.07 hrs, Volume= 0.160 af, Depth> 4.87"

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"

Area (sf)	CN Description					
17,152	98 Roofs, HSG A					
17,152	17,152 100.00% Impervious Area					
Tc Length (min) (feet)	Slope Velocity Capacity Descr (ft/ft) (ft/sec) (cfs)	city Description cfs)				
5.0 Direct Entry,						
Subcatchment CEC: Central East - Campus						
	2.13 cfs					
2-		25-Year Rainfall=5.50"				
		Runoff Area=17,152 sf				
		Runoff Volume=0.160 af				
(cfs)		Runoff Depth>4.87"				

12 13 Time (hours) 14

Tc=5.0 min

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CN=98

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Summary for Subcatchment CWC: Central West - Campus

Runoff = 4.48 cfs @ 12.07 hrs, Volume= 0.336 af, Depth> 4.87"

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Time (hours)

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"



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Summary for Subcatchment ILC: IL Attached - Campus - 6 units (center)

Runoff = 2.13 cfs @ 12.07 hrs, Volume= 0.160 af, Depth> 4.87"



Summary for Subcatchment ILE: IL Attached - Campus - 3 units (east)

Runoff = 1.07 cfs @ 12.07 hrs, Volume= 0.080 af, Depth> 4.87"

A	rea (sf)	CN	Description				
	8,575	98	Roofs, HSC	βA			
	8,575	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft	Velocity(ft/sec)	Capacity (cfs)	Description		
5.0					Direct Entry,		
Subcatchmont II F: II Attached - Campus - 3 units (cast)							



Summary for Subcatchment ILW: IL Attached - Campus - 6 units (west)

Runoff = 2.12 cfs @ 12.07 hrs, Volume= 0.159 af, Depth> 4.87"

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Time (hours)

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=5.50"



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Summary for Subcatchment NC: North - Campus

Runoff = 3.95 cfs @ 12.07 hrs, Volume= 0.296 af, Depth> 4.87"


Summary for Pond IT 22: 20 CULTEC R-330XL

Inflow Area	ι =	0.190 ac,10	0.00% Impe	ervious,	Inflow	Depth >	4.87	" for 25-Y	ear event	
Inflow	=	1.03 cfs @	12.07 hrs,	Volume	=	0.077	af			
Outflow	=	0.07 cfs @	13.46 hrs,	Volume	=	0.061	af, A	Atten= 93%,	Lag= 83.4	min
Discarded	=	0.07 cfs @	13.46 hrs,	Volume	=	0.061	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.28' @ 13.46 hrs Surf.Area= 860 sf Storage= 1,534 cf

Plug-Flow detention time= 159.8 min calculated for 0.061 af (78% of inflow) Center-of-Mass det. time= 103.6 min (837.4 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	955 cf	22.33'W x 38.50'L x 4.04'H Field A
			3,475 cf Overall - 1,088 cf Embedded = 2,387 cf x 40.0% Voids
#2A	176.46'	1,088 cf	Cultec R-330XL x 20 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 4 rows
		2,043 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	175.46'	2.410 in/hr Exfiltration over We	tted area
Discard	led OutFlow	Max=0.07 cfs	@ 13.46 hrs HW=178.28' (Free	e Discharge)

1=Exfiltration (Exfiltration Controls 0.07 cfs)

Pond IT 22: 20 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 4 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 4 Rows x 52.0" Wide + 12.0" Spacing x 3 + 12.0" Side Stone x 2 = 22.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

20 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 4 Rows = 1,087.8 cf Chamber Storage

3,475.2 cf Field - 1,087.8 cf Chambers = 2,387.3 cf Stone x 40.0% Voids = 954.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,042.8 cf = 0.047 af Overall Storage Efficiency = 58.8%

20 Chambers 128.7 cy Field 88.4 cy Stone







Pond IT 22: 20 CULTEC R-330XL

Summary for Pond IT10: 12 CULTEC R-330XL

Inflow Area	a =	0.121 ac,10	0.00% Impe	ervious,	Inflow Depth	> 4.87	7" for 25-Y	ear event
Inflow	=	0.66 cfs @	12.07 hrs,	Volume	= 0.04	49 af		
Outflow	=	0.05 cfs @	13.29 hrs,	Volume	= 0.04	40 af, <i>I</i>	Atten= 93%,	Lag= 73.3 min
Discarded	=	0.05 cfs @	13.29 hrs,	Volume	= 0.04	40 af		•

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 182.35' @ 13.29 hrs Surf.Area= 536 sf Storage= 968 cf

Plug-Flow detention time= 159.3 min calculated for 0.040 af (81% of inflow) Center-of-Mass det. time= 106.0 min (839.9 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	179.46'	602 cf	17.00'W x 31.50'L x 4.04'H Field A
			2,164 cf Overall - 659 cf Embedded = 1,505 cf x 40.0% Voids
#2A	180.46'	659 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,261 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	179.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow I filtration (Ext	Max=0.05 cfs filtration Cont	@ 13.29 hrs HW=182.35' (Free Discharge) rols 0.05 cfs)

Pond IT10: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 659.4 cf Chamber Storage

2,164.3 cf Field - 659.4 cf Chambers = 1,504.9 cf Stone x 40.0% Voids = 602.0 cf Stone Storage

Chamber Storage + Stone Storage = 1,261.4 cf = 0.029 af Overall Storage Efficiency = 58.3%

12 Chambers 80.2 cy Field 55.7 cy Stone







Pond IT10: 12 CULTEC R-330XL

Summary for Pond IT11: 28 CULTEC R-330XL

Inflow Area	a =	0.242 ac,10	0.00% Impe	ervious,	Inflow Depth	> 4.87	" for 25-Ye	ear event
Inflow	=	1.31 cfs @	12.07 hrs,	Volume	= 0.0)98 af		
Outflow	=	0.09 cfs @	13.42 hrs,	Volume	= 0.0)80 af, <i>A</i>	Atten= 93%,	Lag= 80.7 min
Discarded	=	0.09 cfs @	13.42 hrs,	Volume	= 0.0)80 af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 181.50' @ 13.42 hrs Surf.Area= 1,207 sf Storage= 1,911 cf

Plug-Flow detention time= 157.8 min calculated for 0.080 af (81% of inflow) Center-of-Mass det. time= 104.5 min (838.4 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.98'	1,337 cf	38.33'W x 31.50'L x 4.04'H Field A
			4,880 cf Overall - 1,539 cf Embedded = 3,342 cf x 40.0% Voids
#2A	179.98'	1,539 cf	Cultec R-330XL x 28 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 7 rows
		2,875 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	178.98'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.09 cfs	@ 13.42 hrs HW=181.50' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.09 cfs)

Pond IT11: 28 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 7 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 7 Rows x 52.0" Wide + 12.0" Spacing x 6 + 12.0" Side Stone x 2 = 38.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

28 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 7 Rows = 1,538.6 cf Chamber Storage

4,880.3 cf Field - 1,538.6 cf Chambers = 3,341.7 cf Stone x 40.0% Voids = 1,336.7 cf Stone Storage

Chamber Storage + Stone Storage = 2,875.3 cf = 0.066 af Overall Storage Efficiency = 58.9%

28 Chambers 180.8 cy Field 123.8 cy Stone







Pond IT11: 28 CULTEC R-330XL

Summary for Pond IT11A: 6 CULTEC R-330XL

Inflow Area	a =	0.061 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.87"	for 25-Ye	ear event	
Inflow	=	0.33 cfs @	12.07 hrs,	Volume	= 0.025	af			
Outflow	=	0.03 cfs @	13.05 hrs,	Volume	= 0.021	af, Atte	en= 92%,	Lag= 58.6 m	in
Discarded	=	0.03 cfs @	13.05 hrs,	Volume	= 0.021	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 183.88' @ 13.05 hrs Surf.Area= 280 sf Storage= 467 cf

Plug-Flow detention time= 151.4 min calculated for 0.021 af (87% of inflow) Center-of-Mass det. time= 109.9 min (843.8 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	181.21'	314 cf	16.00'W x 17.50'L x 4.04'H Field A
			1,132 cf Overall - 346 cf Embedded = 785 cf x 40.0% Voids
#2A	182.21'	346 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		661 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	181.21'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Exf	Max=0.03 cfs	a @ 13.05 hrs HW=183.88' (Free Discharge) trols 0.03 cfs)

Pond IT11A: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

2 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 15.50' Row Length +12.0" End Stone x 2 = 17.50' Base Length 3 Rows x 52.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 16.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 346.5 cf Chamber Storage

1,131.7 cf Field - 346.5 cf Chambers = 785.2 cf Stone x 40.0% Voids = 314.1 cf Stone Storage

Chamber Storage + Stone Storage = 660.5 cf = 0.015 af Overall Storage Efficiency = 58.4%

6 Chambers 41.9 cy Field 29.1 cy Stone







Pond IT11A: 6 CULTEC R-330XL

Summary for Pond IT12: 14 CULTEC R-330XL

Inflow Area	ι =	0.129 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.87"	for 25-Ye	ear event	
Inflow	=	0.70 cfs @	12.07 hrs,	Volume	= 0.053	af			
Outflow	=	0.05 cfs @	13.09 hrs,	Volume	= 0.045	af, Atte	en= 92%,	Lag= 60.9 mii	n
Discarded	=	0.05 cfs @	13.09 hrs,	Volume	= 0.045	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 181.59' @ 13.09 hrs Surf.Area= 613 sf Storage= 1,000 cf

Plug-Flow detention time= 152.3 min calculated for 0.045 af (86% of inflow) Center-of-Mass det. time= 109.2 min (843.0 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.96'	689 cf	11.67'W x 52.50'L x 4.04'H Field A
			2,476 cf Overall - 753 cf Embedded = 1,723 cf x 40.0% Voids
#2A	179.96'	753 cf	Cultec R-330XL x 14 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,442 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	178.96'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.05 cfs	@ 13.09 hrs HW=181.58' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.05 cfs)

Pond IT12: 14 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

14 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 752.6 cf Chamber Storage

2,475.5 cf Field - 752.6 cf Chambers = 1,723.0 cf Stone x 40.0% Voids = 689.2 cf Stone Storage

Chamber Storage + Stone Storage = 1,441.7 cf = 0.033 af Overall Storage Efficiency = 58.2%

14 Chambers 91.7 cy Field 63.8 cy Stone







Pond IT12: 14 CULTEC R-330XL

Summary for Pond IT13: 12 CULTEC R-330XL

Inflow Area	ι =	0.116 ac,10	0.00% Impe	ervious,	Inflow	Depth >	4.87"	for 25-Ye	ear event	
Inflow	=	0.63 cfs @	12.07 hrs,	Volume	=	0.047	af			
Outflow	=	0.05 cfs @	13.10 hrs,	Volume	=	0.040	af, Atte	en= 93%,	Lag= 61.6 r	nin
Discarded	=	0.05 cfs @	13.10 hrs,	Volume	=	0.040	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.93' @ 13.10 hrs Surf.Area= 531 sf Storage= 900 cf

Plug-Flow detention time= 154.3 min calculated for 0.040 af (85% of inflow) Center-of-Mass det. time= 108.8 min (842.6 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.21'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	177.21'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.21'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.05 cfs	@ 13.10 hrs HW=178.93' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.05 cfs)

Pond IT13: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT13: 12 CULTEC R-330XL

Summary for Pond IT14: 12 CULTEC R-330XL

Inflow Area	ι =	0.116 ac,10	0.00% Impe	ervious,	Inflow	Depth >	4.87"	for 25-Ye	ear event	
Inflow	=	0.63 cfs @	12.07 hrs,	Volume	=	0.047	af			
Outflow	=	0.05 cfs @	13.10 hrs,	Volume	=	0.040	af, Atte	en= 93%,	Lag= 61.6 m	in
Discarded	=	0.05 cfs @	13.10 hrs,	Volume	=	0.040	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.68' @ 13.10 hrs Surf.Area= 531 sf Storage= 900 cf

Plug-Flow detention time= 154.3 min calculated for 0.040 af (85% of inflow) Center-of-Mass det. time= 108.8 min (842.6 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.96'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	176.96'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.96'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow I filtration (Exi	Max=0.05 cfs filtration Cont	@ 13.10 hrs HW=178.68' (Free Discharge) trols 0.05 cfs)

Pond IT14: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT14: 12 CULTEC R-330XL

Summary for Pond IT15: 14 CULTEC R-330XL

Inflow Area	a =	0.129 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.87"	for 25-Ye	ear event
Inflow	=	0.70 cfs @	12.07 hrs,	Volume	= 0.053	8 af		
Outflow	=	0.05 cfs @	13.09 hrs,	Volume	= 0.045	iaf, At	ten= 92%,	Lag= 60.9 min
Discarded	=	0.05 cfs @	13.09 hrs,	Volume	= 0.045	i af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.29' @ 13.09 hrs Surf.Area= 613 sf Storage= 1,000 cf

Plug-Flow detention time= 152.3 min calculated for 0.045 af (86% of inflow) Center-of-Mass det. time= 109.2 min (843.0 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.66'	689 cf	11.67'W x 52.50'L x 4.04'H Field A
			2,476 cf Overall - 753 cf Embedded = 1,723 cf x 40.0% Voids
#2A	177.66'	753 cf	Cultec R-330XL x 14 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,442 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.66'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Exf	Max=0.05 cfs	@ 13.09 hrs HW=179.28' (Free Discharge) rols 0.05 cfs)

Pond IT15: 14 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

14 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 752.6 cf Chamber Storage

2,475.5 cf Field - 752.6 cf Chambers = 1,723.0 cf Stone x 40.0% Voids = 689.2 cf Stone Storage

Chamber Storage + Stone Storage = 1,441.7 cf = 0.033 af Overall Storage Efficiency = 58.2%

14 Chambers 91.7 cy Field 63.8 cy Stone







Pond IT15: 14 CULTEC R-330XL

Summary for Pond IT16: 45 - 330XL

Inflow Area	ι =	0.394 ac,10	0.00% Impe	ervious, I	Inflow Depth >	4.87"	for 25-Ye	ear event
Inflow	=	2.13 cfs @	12.07 hrs,	Volume=	= 0.160) af		
Outflow	=	0.13 cfs @	13.61 hrs,	Volume=	= 0.123	8 af, Att	en= 94%,	Lag= 92.3 min
Discarded	=	0.13 cfs @	13.61 hrs,	Volume=	= 0.123	3 af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.19' @ 13.61 hrs Surf.Area= 1,840 sf Storage= 3,203 cf

Plug-Flow detention time= 160.0 min calculated for 0.122 af (76% of inflow) Center-of-Mass det. time= 100.8 min (834.7 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	2,013 cf	27.67'W x 66.50'L x 4.04'H Field A
			7,436 cf Overall - 2,403 cf Embedded = 5,033 cf x 40.0% Voids
#2A	176.46'	2,403 cf	Cultec R-330XL x 45 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 5 rows
		4,416 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Exf	Max=0.13 cfs	@ 13.61 hrs HW=178.19' (Free Discharge) trols 0.13 cfs)

Pond IT16: 45 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 5 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 5 Rows x 52.0" Wide + 12.0" Spacing x 4 + 12.0" Side Stone x 2 = 27.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

45 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 5 Rows = 2,402.9 cf Chamber Storage

7,436.0 cf Field - 2,402.9 cf Chambers = 5,033.0 cf Stone x 40.0% Voids = 2,013.2 cf Stone Storage

Chamber Storage + Stone Storage = 4,416.2 cf = 0.101 af Overall Storage Efficiency = 59.4%

45 Chambers 275.4 cy Field 186.4 cy Stone







Pond IT16: 45 - 330XL

Summary for Pond IT17: 24 - 330XL

Inflow Area	ι =	0.197 ac,10	0.00% Impe	ervious,	Inflow De	pth >	4.87"	for 25-Y	ear event	
Inflow	=	1.07 cfs @	12.07 hrs,	Volume	=	0.080	af			
Outflow	=	0.07 cfs @	13.25 hrs,	Volume	=	0.068	af, Atte	en= 93%,	Lag= 71.0 r	nin
Discarded	=	0.07 cfs @	13.25 hrs,	Volume	=	0.068	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 175.31' @ 13.25 hrs Surf.Area= 1,040 sf Storage= 1,511 cf

Plug-Flow detention time= 153.9 min calculated for 0.068 af (85% of inflow) Center-of-Mass det. time= 107.4 min (841.2 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	172.96'	1,153 cf	33.00'W x 31.50'L x 4.04'H Field A
			4,201 cf Overall - 1,319 cf Embedded = 2,882 cf x 40.0% Voids
#2A	173.96'	1,319 cf	Cultec R-330XL x 24 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		2,472 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	172.96'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Exf	Max=0.07 cfs	@ 13.25 hrs HW=175.31' (Free Discharge) trols 0.07 cfs)

Pond IT17: 24 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

24 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 1,318.8 cf Chamber Storage

4,201.3 cf Field - 1,318.8 cf Chambers = 2,882.5 cf Stone x 40.0% Voids = 1,153.0 cf Stone Storage

Chamber Storage + Stone Storage = 2,471.8 cf = 0.057 af Overall Storage Efficiency = 58.8%

24 Chambers 155.6 cy Field 106.8 cy Stone









Summary for Pond IT18: 48 - 330XL

Inflow Area	a =	0.394 ac,10	0.00% Impe	ervious,	Inflow I	Depth >	4.87"	for 25-Y	ear event	
Inflow	=	2.13 cfs @	12.07 hrs,	Volume	=	0.160	af			
Outflow	=	0.14 cfs @	13.53 hrs,	Volume	=	0.127	af, Att	en= 94%,	Lag= 87.4	min
Discarded	=	0.14 cfs @	13.53 hrs,	Volume	=	0.127	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 175.98' @ 13.53 hrs Surf.Area= 1,964 sf Storage= 3,135 cf

Plug-Flow detention time= 158.9 min calculated for 0.127 af (79% of inflow) Center-of-Mass det. time= 102.5 min (836.4 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	173.46'	2,146 cf	33.00'W x 59.50'L x 4.04'H Field A
			7,936 cf Overall - 2,571 cf Embedded = 5,365 cf x 40.0% Voids
#2A	174.46'	2,571 cf	Cultec R-330XL x 48 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		4,717 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	173.46'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.14 cfs	@ 13.53 hrs HW=175.98' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.14 cfs)

Pond IT18: 48 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

48 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 2,570.6 cf Chamber Storage

7,935.8 cf Field - 2,570.6 cf Chambers = 5,365.2 cf Stone x 40.0% Voids = 2,146.1 cf Stone Storage

Chamber Storage + Stone Storage = 4,716.7 cf = 0.108 af Overall Storage Efficiency = 59.4%

48 Chambers 293.9 cy Field 198.7 cy Stone







Pond IT18: 48 - 330XL

Summary for Pond IT19: 48 - 330XL

Inflow Area	ι =	0.390 ac,10	0.00% Impe	ervious,	Inflow	Depth >	4.87"	for 25-Ye	ear event
Inflow	=	2.12 cfs @	12.07 hrs,	Volume	=	0.159	af		
Outflow	=	0.14 cfs @	13.51 hrs,	Volume	=	0.126	af, Att	en= 94%,	Lag= 86.3 min
Discarded	=	0.14 cfs @	13.51 hrs,	Volume	=	0.126	af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 173.75' @ 13.51 hrs Surf.Area= 1,964 sf Storage= 3,096 cf

Plug-Flow detention time= 158.5 min calculated for 0.126 af (80% of inflow) Center-of-Mass det. time= 102.9 min (836.7 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	171.25'	2,146 cf	33.00'W x 59.50'L x 4.04'H Field A
			7,936 cf Overall - 2,571 cf Embedded = 5,365 cf x 40.0% Voids
#2A	172.25'	2,571 cf	Cultec R-330XL x 48 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		4,717 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	171.25'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.14 cfs	@ 13.51 hrs HW=173.75' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.14 cfs)

Pond IT19: 48 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

48 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 2,570.6 cf Chamber Storage

7,935.8 cf Field - 2,570.6 cf Chambers = 5,365.2 cf Stone x 40.0% Voids = 2,146.1 cf Stone Storage

Chamber Storage + Stone Storage = 4,716.7 cf = 0.108 af Overall Storage Efficiency = 59.4%

48 Chambers 293.9 cy Field 198.7 cy Stone







Pond IT19: 48 - 330XL
Summary for Pond IT20: 100 - 330XL

Inflow Area	I =	0.826 ac,10	0.00% Impervious,	Inflow Depth >	4.87" for	25-Year event
Inflow	=	4.48 cfs @	12.07 hrs, Volume	= 0.336	af	
Outflow	=	0.26 cfs @	13.75 hrs, Volume	= 0.251	af, Atten= 9	94%, Lag= 100.5 min
Discarded	=	0.26 cfs @	13.75 hrs, Volume	= 0.251	af	-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.10' @ 13.75 hrs Surf.Area= 3,994 sf Storage= 6,773 cf

Plug-Flow detention time= 159.5 min calculated for 0.250 af (74% of inflow) Center-of-Mass det. time= 97.6 min (831.5 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	4,325 cf	54.33'W x 73.50'L x 4.04'H Field A
			16,140 cf Overall - 5,327 cf Embedded = 10,813 cf x 40.0% Voids
#2A	176.46'	5,327 cf	Cultec R-330XL x 100 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 10 rows
		9,653 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Ext	Max=0.26 cfs filtration Cont	@ 13.75 hrs HW=178.10' (Free Discharge) rols 0.26 cfs)

Pond IT20: 100 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 10 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

10 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 71.50' Row Length +12.0" End Stone x 2 = 73.50' Base Length 10 Rows x 52.0" Wide + 12.0" Spacing x 9 + 12.0" Side Stone x 2 = 54.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

100 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 10 Rows = 5,327.5 cf Chamber Storage

16,140.4 cf Field - 5,327.5 cf Chambers = 10,812.9 cf Stone x 40.0% Voids = 4,325.2 cf Stone Storage

Chamber Storage + Stone Storage = 9,652.6 cf = 0.222 af Overall Storage Efficiency = 59.8%

100 Chambers 597.8 cy Field 400.5 cy Stone







Pond IT20: 100 - 330XL

Summary for Pond IT21: 25 CULTEC R-330XL

Inflow Area	a =	0.237 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.87"	for 25-Ye	ear event
Inflow	=	1.28 cfs @	12.07 hrs,	Volume	= 0.096	af		
Outflow	=	0.08 cfs @	13.56 hrs,	Volume	= 0.074	af, Atte	en= 94%,	Lag= 89.4 min
Discarded	=	0.08 cfs @	13.56 hrs,	Volume	= 0.074	af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 172.55' @ 13.56 hrs Surf.Area= 1,065 sf Storage= 1,933 cf

Plug-Flow detention time= 161.5 min calculated for 0.074 af (77% of inflow) Center-of-Mass det. time= 101.8 min (835.6 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	169.69'	1,178 cf	27.67'W x 38.50'L x 4.04'H Field A
			4,305 cf Overall - 1,360 cf Embedded = 2,945 cf x 40.0% Voids
#2A	170.69'	1,360 cf	Cultec R-330XL x 25 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 5 rows
		2,538 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	169.69'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.08 cfs	@ 13.56 hrs HW=172.55' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond IT21: 25 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 5 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 5 Rows x 52.0" Wide + 12.0" Spacing x 4 + 12.0" Side Stone x 2 = 27.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

25 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 5 Rows = 1,359.8 cf Chamber Storage

4,305.0 cf Field - 1,359.8 cf Chambers = 2,945.2 cf Stone x 40.0% Voids = 1,178.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,537.9 cf = 0.058 af Overall Storage Efficiency = 59.0%

25 Chambers 159.4 cy Field 109.1 cy Stone







Pond IT21: 25 CULTEC R-330XL

Summary for Pond IT22A: 6 CULTEC R-330XL

Inflow Area	a =	0.055 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.87"	for 25-Ye	ear event	
Inflow	=	0.30 cfs @	12.07 hrs,	Volume	= 0.022	af			
Outflow	=	0.03 cfs @	12.86 hrs,	Volume	= 0.022	af, Atte	en= 91%,	Lag= 47.6 r	min
Discarded	=	0.03 cfs @	12.86 hrs,	Volume	= 0.022	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.57' @ 12.86 hrs Surf.Area= 288 sf Storage= 395 cf

Plug-Flow detention time= 125.1 min calculated for 0.022 af (96% of inflow) Center-of-Mass det. time= 110.9 min (844.8 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	177.46'	279 cf	6.33'W x 45.50'L x 3.54'H Field A
			1,021 cf Overall - 324 cf Embedded = 696 cf x 40.0% Voids
#2A	177.96'	324 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 1 rows
		603 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	177.46'	2.410 in/hr Exfiltration over Wetted area	
Discard	ed OutFlow I filtration (Ext	Max=0.03 cfs filtration Cont	@ 12.86 hrs HW=179.57' (Free Discharge) rols 0.03 cfs)	

Pond IT22A: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 1 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 1 Rows x 52.0" Wide + 12.0" Side Stone x 2 = 6.33' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 1 Rows = 324.1 cf Chamber Storage

1,020.6 cf Field - 324.1 cf Chambers = 696.5 cf Stone x 40.0% Voids = 278.6 cf Stone Storage

Chamber Storage + Stone Storage = 602.7 cf = 0.014 af Overall Storage Efficiency = 59.1%

6 Chambers 37.8 cy Field 25.8 cy Stone







Pond IT22A: 6 CULTEC R-330XL

Summary for Pond IT23: 88 - 330XL

Inflow Area	=	0.729 ac,10	0.00% Impe	ervious,	Inflow De	epth >	4.87"	for 25-Y	ear event
Inflow	=	3.95 cfs @	12.07 hrs,	Volume	=	0.296	af		
Outflow	=	0.23 cfs @	13.71 hrs,	Volume	=	0.223	af, Atte	en= 94%,	Lag= 98.6 min
Discarded	=	0.23 cfs @	13.71 hrs,	Volume	=	0.223	af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.08' @ 13.71 hrs Surf.Area= 3,550 sf Storage= 5,943 cf

Plug-Flow detention time= 159.4 min calculated for 0.222 af (75% of inflow) Center-of-Mass det. time= 98.4 min (832.3 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	3,854 cf	59.67'W x 59.50'L x 4.04'H Field A
			14,349 cf Overall - 4,713 cf Embedded = 9,636 cf x 40.0% Voids
#2A	176.46'	4,713 cf	Cultec R-330XL x 88 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 11 rows
		8,567 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow I filtration (Exi	Max=0.23 cfs filtration Cont	@ 13.71 hrs HW=178.08' (Free Discharge) trols 0.23 cfs)

Pond IT23: 88 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 11 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 11 Rows x 52.0" Wide + 12.0" Spacing x 10 + 12.0" Side Stone x 2 = 59.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

88 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 11 Rows = 4,712.8 cf Chamber Storage

14,348.6 cf Field - 4,712.8 cf Chambers = 9,635.8 cf Stone x 40.0% Voids = 3,854.3 cf Stone Storage

Chamber Storage + Stone Storage = 8,567.1 cf = 0.197 af Overall Storage Efficiency = 59.7%

88 Chambers 531.4 cy Field 356.9 cy Stone







Pond IT23: 88 - 330XL

Summary for Pond IT24: 8 CULTEC R-330XL

Inflow Area	1 =	0.069 ac,10	0.00% Impe	ervious,	Inflow D)epth >	4.87"	for 25-Y	ear event	
Inflow	=	0.37 cfs @	12.07 hrs,	Volume	=	0.028	af			
Outflow	=	0.03 cfs @	13.02 hrs,	Volume	=	0.025	af, Att	en= 92%,	Lag= 56.9 r	nin
Discarded	=	0.03 cfs @	13.02 hrs,	Volume	=	0.025	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 178.37' @ 13.02 hrs Surf.Area= 352 sf Storage= 516 cf

Plug-Flow detention time= 144.9 min calculated for 0.025 af (89% of inflow) Center-of-Mass det. time= 109.6 min (843.4 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.21'	322 cf	11.17'W x 31.50'L x 3.54'H Field A
			1,246 cf Overall - 440 cf Embedded = 806 cf x 40.0% Voids
#2A	176.71'	440 cf	Cultec R-330XL x 8 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		762 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	176.21'	2.410 in/hr Exfiltration over Wetted area	
Discard	ed OutFlow I filtration (Ext	Max=0.03 cfs filtration Cont	@ 13.02 hrs HW=178.37' (Free Discharge) trols 0.03 cfs)	

Pond IT24: 8 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 2 Rows x 52.0" Wide + 6.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.17' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

8 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 439.6 cf Chamber Storage

1,245.8 cf Field - 439.6 cf Chambers = 806.2 cf Stone x 40.0% Voids = 322.5 cf Stone Storage

Chamber Storage + Stone Storage = 762.1 cf = 0.017 afOverall Storage Efficiency = 61.2%

8 Chambers 46.1 cy Field 29.9 cy Stone







Pond IT24: 8 CULTEC R-330XL

Summary for Pond IT25: 12 CULTEC R-330XL

Inflow Area	ι =	0.121 ac,10	0.00% Impe	ervious,	Inflow	Depth >	4.87	" for 25-Ye	ear event
Inflow	=	0.66 cfs @	12.07 hrs,	Volume	=	0.049	af		
Outflow	=	0.05 cfs @	13.14 hrs,	Volume	=	0.041	af, A	tten= 93%,	Lag= 64.4 min
Discarded	=	0.05 cfs @	13.14 hrs,	Volume	=	0.041	af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 190.35' @ 13.14 hrs Surf.Area= 531 sf Storage= 958 cf

Plug-Flow detention time= 156.5 min calculated for 0.041 af (83% of inflow) Center-of-Mass det. time= 107.9 min (841.7 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	187.46'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	188.46'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	187.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.05 cfs	@ 13.14 hrs HW=190.35' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.05 cfs)

Pond IT25: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT25: 12 CULTEC R-330XL

Summary for Pond IT26: 18 CULTEC R-330XL

Inflow Area	a =	0.171 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.87"	for 25-Y	ear event	
Inflow	=	0.93 cfs @	12.07 hrs,	Volume	= 0.069	af			
Outflow	=	0.06 cfs @	13.36 hrs,	Volume	= 0.056	af, Atte	en= 93%,	Lag= 77.1	min
Discarded	=	0.06 cfs @	13.36 hrs,	Volume	= 0.056	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 185.66' @ 13.36 hrs Surf.Area= 774 sf Storage= 1,365 cf

Plug-Flow detention time= 159.5 min calculated for 0.056 af (80% of inflow) Center-of-Mass det. time= 105.2 min (839.1 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	182.86'	862 cf	17.00'W x 45.50'L x 4.04'H Field A
			3,126 cf Overall - 972 cf Embedded = 2,154 cf x 40.0% Voids
#2A	183.86'	972 cf	Cultec R-330XL x 18 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,834 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	182.86'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.06 cfs	@ 13.36 hrs HW=185.66' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.06 cfs)

Pond IT26: 18 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

18 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 972.4 cf Chamber Storage

3,126.2 cf Field - 972.4 cf Chambers = 2,153.9 cf Stone x 40.0% Voids = 861.5 cf Stone Storage

Chamber Storage + Stone Storage = 1,833.9 cf = 0.042 af Overall Storage Efficiency = 58.7%

18 Chambers 115.8 cy Field 79.8 cy Stone







Pond IT26: 18 CULTEC R-330XL

Summary for Pond IT29: 27 CULTEC R-330XL

Inflow Area	a =	0.242 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.87"	for 25-Ye	ear event	
Inflow	=	1.31 cfs @	12.07 hrs,	Volume	= 0.098	af			
Outflow	=	0.09 cfs @	13.38 hrs,	Volume	= 0.079	af, Atte	en= 93%,	Lag= 78.5 m	nin
Discarded	=	0.09 cfs @	13.38 hrs,	Volume	= 0.079	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 186.16' @ 13.38 hrs Surf.Area= 1,131 sf Storage= 1,930 cf

Plug-Flow detention time= 158.2 min calculated for 0.079 af (80% of inflow) Center-of-Mass det. time= 104.9 min (838.8 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	183.46'	1,251 cf	17.00'W x 66.50'L x 4.04'H Field A
			4,569 cf Overall - 1,442 cf Embedded = 3,127 cf x 40.0% Voids
#2A	184.46'	1,442 cf	Cultec R-330XL x 27 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		2,693 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	183.46'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.09 cfs	@ 13.38 hrs HW=186.16' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.09 cfs)

Pond IT29: 27 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

27 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 1,441.8 cf Chamber Storage

4,569.1 cf Field - 1,441.8 cf Chambers = 3,127.3 cf Stone x 40.0% Voids = 1,250.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,692.7 cf = 0.062 af Overall Storage Efficiency = 58.9%

27 Chambers 169.2 cy Field 115.8 cy Stone







Pond IT29: 27 CULTEC R-330XL

Summary for Pond IT30: 15 CULTEC R-330XL

Inflow Area	a =	0.116 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.87"	for 25-Y	ear event	
Inflow	=	0.63 cfs @	12.07 hrs,	Volume	= 0.047	af			
Outflow	=	0.05 cfs @	13.03 hrs,	Volume	= 0.043	af, Atte	en= 92%,	Lag= 57.3 m	າin
Discarded	=	0.05 cfs @	13.03 hrs,	Volume	= 0.043	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 183.12' @ 13.03 hrs Surf.Area= 655 sf Storage= 851 cf

Plug-Flow detention time= 142.1 min calculated for 0.043 af (92% of inflow) Center-of-Mass det. time= 112.1 min (845.9 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	180.96'	732 cf	17.00'W x 38.50'L x 4.04'H Field A
			2,645 cf Overall - 816 cf Embedded = 1,829 cf x 40.0% Voids
#2A	181.96'	816 cf	Cultec R-330XL x 15 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,548 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	180.96'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.05 cfs	@ 13.03 hrs HW=183.12' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.05 cfs)

Pond IT30: 15 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

15 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 815.9 cf Chamber Storage

2,645.3 cf Field - 815.9 cf Chambers = 1,829.4 cf Stone x 40.0% Voids = 731.8 cf Stone Storage

Chamber Storage + Stone Storage = 1,547.6 cf = 0.036 af Overall Storage Efficiency = 58.5%

15 Chambers 98.0 cy Field 67.8 cy Stone







Pond IT30: 15 CULTEC R-330XL

Summary for Pond IT31: 27 CULTEC R-330XL

Inflow Area	ι =	0.237 ac,10	0.00% Impe	ervious,	Inflow Depth >	4.87"	for 25-Ye	ear event	
Inflow	=	1.28 cfs @	12.07 hrs,	Volume	= 0.096	af			
Outflow	=	0.09 cfs @	13.34 hrs,	Volume	= 0.079	af, Att	en= 93%,	Lag= 76.0 m	in
Discarded	=	0.09 cfs @	13.34 hrs,	Volume	= 0.079	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.09' @ 13.34 hrs Surf.Area= 1,131 sf Storage= 1,870 cf

Plug-Flow detention time= 157.9 min calculated for 0.079 af (82% of inflow) Center-of-Mass det. time= 105.6 min (839.5 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.46'	1,251 cf	17.00'W x 66.50'L x 4.04'H Field A
			4,569 cf Overall - 1,442 cf Embedded = 3,127 cf x 40.0% Voids
#2A	177.46'	1,442 cf	Cultec R-330XL x 27 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		2,693 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.09 cfs filtration Cont	@ 13.34 hrs HW=179.09' (Free Discharge) trols 0.09 cfs)

Pond IT31: 27 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

27 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 1,441.8 cf Chamber Storage

4,569.1 cf Field - 1,441.8 cf Chambers = 3,127.3 cf Stone x 40.0% Voids = 1,250.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,692.7 cf = 0.062 af Overall Storage Efficiency = 58.9%

27 Chambers 169.2 cy Field 115.8 cy Stone







Pond IT31: 27 CULTEC R-330XL

Summary for Pond IT8: 20 CULTEC R-330XL

Inflow Area	I =	0.182 ac,10	0.00% Impe	ervious,	Inflow	Depth >	4.87"	for 25-Ye	ear event	
Inflow	=	0.99 cfs @	12.07 hrs,	Volume	=	0.074	af			
Outflow	=	0.07 cfs @	13.12 hrs,	Volume	=	0.063	af, Att	en= 93%,	Lag= 62.9 mi	n
Discarded	=	0.07 cfs @	13.12 hrs,	Volume	=	0.063	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 180.35' @ 13.12 hrs Surf.Area= 858 sf Storage= 1,411 cf

Plug-Flow detention time= 154.3 min calculated for 0.063 af (85% of inflow) Center-of-Mass det. time= 108.5 min (842.4 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	177.71'	960 cf	11.67'W x 73.50'L x 4.04'H Field A
			3,466 cf Overall - 1,065 cf Embedded = 2,400 cf x 40.0% Voids
#2A	178.71'	1,065 cf	Cultec R-330XL x 20 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		2,026 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	177.71'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow	Max=0.07 cfs	s@ 13.12 hrs HW=180.35' (Free Discharge)	

1=Exfiltration (Exfiltration Controls 0.07 cfs)

Pond IT8: 20 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

10 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 71.50' Row Length +12.0" End Stone x 2 = 73.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

20 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 1,065.5 cf Chamber Storage

3,465.7 cf Field - 1,065.5 cf Chambers = 2,400.2 cf Stone x 40.0% Voids = 960.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,025.6 cf = 0.047 af Overall Storage Efficiency = 58.4%

20 Chambers 128.4 cy Field 88.9 cy Stone







Pond IT8: 20 CULTEC R-330XL

Summary for Pond IT9: 6 CULTEC R-330XL

Inflow Area	ι =	0.055 ac,10	0.00% Impe	ervious,	Inflow Depth	> 4.8	7" for	25-Yeaı	r event	
Inflow	=	0.30 cfs @	12.07 hrs,	Volume	= 0.0	22 af				
Outflow	=	0.02 cfs @	13.02 hrs,	Volume	= 0.0	20 af,	Atten= 9	2%, La	g= 57.2 r	nin
Discarded	=	0.02 cfs @	13.02 hrs,	Volume	= 0.0	20 af				

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 181.15' @ 13.02 hrs Surf.Area= 280 sf Storage= 414 cf

Plug-Flow detention time= 146.0 min calculated for 0.020 af (89% of inflow) Center-of-Mass det. time= 109.4 min (843.3 - 733.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.96'	258 cf	16.00'W x 17.50'L x 3.54'H Field A
			992 cf Overall - 346 cf Embedded = 645 cf x 40.0% Voids
#2A	179.46'	346 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		605 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	178.96'	2.410 in/hr Exfiltration over Wetted area	
Discard	ed OutFlow I filtration (Exi	Max=0.02 cfs filtration Cont	@ 13.02 hrs HW=181.15' (Free Discharge) rols 0.02 cfs)	

Pond IT9: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

2 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 15.50' Row Length +12.0" End Stone x 2 = 17.50' Base Length 3 Rows x 52.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 16.00' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 346.5 cf Chamber Storage

991.7 cf Field - 346.5 cf Chambers = 645.2 cf Stone x 40.0% Voids = 258.1 cf Stone Storage

Chamber Storage + Stone Storage = 604.5 cf = 0.014 afOverall Storage Efficiency = 61.0%

6 Chambers 36.7 cy Field 23.9 cy Stone







Pond IT9: 6 CULTEC R-330XL
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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1BW:1BW	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.36 cfs 0.027 af
Subcatchment1LP:1 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 2BW: 2 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 2LP: 2 LP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.36 cfs 0.027 af
Subcatchment 2WS: 2 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment3BW: 3 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 3LP: 3 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 4BW: 4 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 4LP: 4 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 4WS: 4 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 5BW: 5 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 5LP: 5LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment6BW: 6 BW	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 6LP: 6 LP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 6WS: 6 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment7LP:7 LP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.36 cfs 0.027 af

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Subcatchment 8LP: 8 LP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.46 cfs 0.034 af
Subcatchment10WS:10WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.36 cfs 0.027 af
Subcatchment 12WP: 12 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 12WS: 12 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 14WP: 14 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 14WS: 14 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 16WP: 16 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 16WS: 16 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 18WP: 18 WP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.46 cfs 0.034 af
Subcatchment 18WS: 18 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 19WP: 19 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 20WP: 20 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 20WS: 20 WS	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.36 cfs 0.027 af
Subcatchment 21WP: 21 WP	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 22WP: 22 WP	Runoff Area=3,000 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.46 cfs 0.034 af
Subcatchment 22WS: 22 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af
Subcatchment 23WP: 23 WP	Runoff Area=2,400 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.36 cfs 0.027 af
Subcatchment 24WS: 24 WS	Runoff Area=2,640 sf 100.00% Impervious Runoff Depth>5.97" Tc=5.0 min CN=98 Runoff=0.40 cfs 0.030 af

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Subcatchment 25WP: 25 WP	Runoff Area=2,640 s To	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =0.40 cfs	epth>5.97" s_0.030 af
Subcatchment 26WS: 26 WS	Runoff Area=2,640 s To	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =0.40 cfs	epth>5.97" s_0.030 af
Subcatchment 27WP: 27 WP	Runoff Area=2,400 s	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =0.36 cfs	epth>5.97" s_0.027 af
Subcatchment 28WS: 28 WS	Runoff Area=2,640 s To	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =0.40 cfs	epth>5.97" s_0.030 af
Subcatchment 29WP: 29 WP	Runoff Area=2,640 s	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =0.40 cfs	epth>5.97" s_0.030 af
Subcatchment 30WS: 30 WS	Runoff Area=2,400 s	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =0.36 cfs	epth>5.97" s_0.027 af
Subcatchment 31WP: 31 WP	Runoff Area=2,640 s	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =0.40 cfs	epth>5.97" s_0.030 af
Subcatchment 33WP: 33 WP	Runoff Area=3,000 s	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =0.46 cfs	epth>5.97" s_0.034 af
Subcatchment 88S: 8WS	Runoff Area=2,400 s	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =0.36 cfs	epth>5.97" s_0.027 af
Subcatchment CEC: Central East -	Runoff Area=17,152 s	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =2.60 cfs	epth>5.97" s_0.196 af
Subcatchment CWC: Central West -	Runoff Area=36,000 s	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =5.47 cfs	epth>5.97" s_0.411 af
Subcatchment ILC: IL Attached - Campus	Runoff Area=17,150 s	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =2.60 cfs	epth>5.97" s_0.196 af
Subcatchment ILE: IL Attached - Campus	• Runoff Area=8,575 s To	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =1.30 cf:	epth>5.97" s_0.098 af
Subcatchment ILW: IL Attached - Campus	Runoff Area=17,000 s	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =2.58 cfs	epth>5.97" s_0.194 af
Subcatchment NC: North - Campus	Runoff Area=31,750 s	sf 100.00 c=5.0 min)% Imperv CN=98	/ious R Runoff=	unoff De =4.82 cfs	epth>5.97" s_0.362 af
Pond IT 22: 20 CULTEC R-330XL	Peak Elev=179.39	' Storage	=2,006 cf	Inflow= Outflow=	=1.26 cfs =0.07 cfs	s 0.094 af s 0.067 af
Pond IT10: 12 CULTEC R-330XL	Peak Elev=183.49	' Storage	=1,260 cf	Inflow= Outflow=	=0.80 cfs =0.05 cfs	s 0.060 af s 0.045 af

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Pond IT11: 28 CULTEC R-330XL	Peak Elev=182.30' Storage=2,515 cf Inflow=1.60 cf Outflow=0.09 cf	s 0.121 af s 0.087 af
Pond IT11A: 6 CULTEC R-330XL	Peak Elev=184.77' Storage=606 cf Inflow=0.40 cf Outflow=0.03 cf	s 0.030 af s 0.024 af
Pond IT12: 14 CULTEC R-330XL	Peak Elev=182.43' Storage=1,302 cf Inflow=0.86 cf Outflow=0.06 cf	s 0.064 af s 0.050 af
Pond IT13: 12 CULTEC R-330XL	Peak Elev=179.89' Storage=1,171 cf Inflow=0.77 cf Outflow=0.05 cf	s 0.058 af s 0.045 af
Pond IT14: 12 CULTEC R-330XL	Peak Elev=179.64' Storage=1,171 cf Inflow=0.77 cf Outflow=0.05 cf	s 0.058 af s 0.045 af
Pond IT15: 14 CULTEC R-330XL	Peak Elev=180.13' Storage=1,302 cf Inflow=0.86 cf Outflow=0.06 cf	s 0.064 af s 0.050 af
Pond IT16: 45 - 330XL	Peak Elev=179.22' Storage=4,212 cf Inflow=2.60 cf Outflow=0.14 cf	s 0.196 af s 0.134 af
Pond IT17: 24 - 330XL	Peak Elev=175.98' Storage=1,990 cf Inflow=1.30 cf Outflow=0.08 cf	s 0.098 af s 0.074 af
Pond IT18: 48 - 330XL	Peak Elev=176.78' Storage=4,137 cf Inflow=2.60 cf Outflow=0.14 cf	s 0.196 af s 0.137 af
Pond IT19: 48 - 330XL	Peak Elev=174.52' Storage=4,087 cf Inflow=2.58 cf Outflow=0.14 cf	s 0.194 af s 0.137 af
Pond IT20: 100 - 330XL	Peak Elev=179.07' Storage=8,956 cf Inflow=5.47 cf Outflow=0.27 cf	s 0.411 af s 0.269 af
Pond IT21: 25 CULTEC R-330XL	Peak Elev=173.72' Storage=2,531 cf Inflow=1.57 cf Outflow=0.09 cf	s 0.118 af s 0.082 af
Pond IT22A: 6 CULTEC R-330XL	Peak Elev=180.24' Storage=512 cf Inflow=0.36 cf Outflow=0.03 cf	s 0.027 af s 0.025 af
Pond IT23: 88 - 330XL	Peak Elev=179.00' Storage=7,859 cf Inflow=4.82 cf Outflow=0.25 cf	s 0.362 af s 0.240 af
Pond IT24: 8 CULTEC R-330XL	Peak Elev=179.12' Storage=672 cf Inflow=0.46 cf Outflow=0.03 cf	s 0.034 af s 0.028 af
Pond IT25: 12 CULTEC R-330XL	Peak Elev=191.48' Storage=1,242 cf Inflow=0.80 cf Outflow=0.06 cf	s 0.060 af s 0.046 af
Pond IT26: 18 CULTEC R-330XL	Peak Elev=186.73' Storage=1,782 cf Inflow=1.13 cf Outflow=0.07 cf	s 0.085 af s 0.062 af
Pond IT29: 27 CULTEC R-330XL	Peak Elev=187.13' Storage=2,527 cf Inflow=1.60 cf Outflow=0.10 cf	s 0.121 af s 0.087 af

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Pond IT30: 15 CULTEC R-330XL	Peak Elev=183.68' Storage=1,116 cf Inflow=0.77 cfs 0.058 af Outflow=0.05 cfs 0.047 af				
Pond IT31: 27 CULTEC R-330XL	Peak Elev=179.97' Storage=2,451 cf Inflow=1.57 cfs 0.118 af Outflow=0.10 cfs 0.086 af				
Pond IT8: 20 CULTEC R-330XL	Peak Elev=181.21' Storage=1,840 cf Inflow=1.20 cfs 0.090 af Outflow=0.08 cfs 0.070 af				
Pond IT9: 6 CULTEC R-330XL	Peak Elev=181.91' Storage=539 cf Inflow=0.36 cfs 0.027 af Outflow=0.03 cfs 0.022 af				
Total Runoff Area = 5.519 ac Runoff Volume = 2.744 af Average Runoff Depth = 5.97" 0.00% Pervious = 0.000 ac 100.00% Impervious = 5.519 ac					

Summary for Subcatchment 1BW: 1BW

Runoff = 0.36 cfs @ 12.07 hrs, Volume= 0.027 af, Depth> 5.97"



Summary for Subcatchment 1LP: 1 LP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



Time (hours)

Summary for Subcatchment 2BW: 2 BW

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"



Summary for Subcatchment 2LP: 2 LP

Runoff = 0.36 cfs @ 12.07 hrs, Volume= 0.027 af, Depth> 5.97"



Summary for Subcatchment 2WS: 2 WS

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"



Summary for Subcatchment 3BW: 3 BW

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"



Summary for Subcatchment 3LP: 3 LP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 4BW: 4 BW

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"



Summary for Subcatchment 4LP: 4 LP

0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97" Runoff =

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Time (hours)

Summary for Subcatchment 4WS: 4 WS

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"



Summary for Subcatchment 5BW: 5 BW

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"



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Summary for Subcatchment 5LP: 5LP

0.40 cfs @ 12.07 hrs, Volume= Runoff 0.030 af, Depth> 5.97" =

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Time (hours)

Summary for Subcatchment 6BW: 6 BW

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"



Summary for Subcatchment 6LP: 6 LP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 6WS: 6 WS

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"



Summary for Subcatchment 7LP: 7 LP

Runoff = 0.36 cfs @ 12.07 hrs, Volume= 0.027 af, Depth> 5.97"



Summary for Subcatchment 8LP: 8 LP

Runoff = 0.46 cfs @ 12.07 hrs, Volume= 0.034 af, Depth> 5.97"



Summary for Subcatchment 10WS: 10 WS

Runoff = 0.36 cfs @ 12.07 hrs, Volume= 0.027 af, Depth> 5.97"



Summary for Subcatchment 12WP: 12 WP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

0.06 0.04 0.02

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 12WS: 12 WS

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 14WP: 14 WP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 14WS: 14 WS

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 16WP: 16 WP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 16WS: 16 WS

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 18WP: 18 WP

Runoff = 0.46 cfs @ 12.07 hrs, Volume= 0.034 af, Depth> 5.97"



Summary for Subcatchment 18WS: 18 WS

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

0.06 0.04 0.02

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 19WP: 19 WP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 20WP: 20 WP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 20WS: 20 WS

Runoff = 0.36 cfs @ 12.07 hrs, Volume= 0.027 af, Depth> 5.97"



Summary for Subcatchment 21WP: 21 WP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 22WP: 22 WP

Runoff = 0.46 cfs @ 12.07 hrs, Volume= 0.034 af, Depth> 5.97"


Summary for Subcatchment 22WS: 22 WS

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 23WP: 23 WP

Runoff = 0.36 cfs @ 12.07 hrs, Volume= 0.027 af, Depth> 5.97"



Summary for Subcatchment 24WS: 24 WS

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 25WP: 25 WP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 26WS: 26 WS

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 27WP: 27 WP

Runoff = 0.36 cfs @ 12.07 hrs, Volume= 0.027 af, Depth> 5.97"



Summary for Subcatchment 28WS: 28 WS

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 29WP: 29 WP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 30WS: 30 WS

Runoff = 0.36 cfs @ 12.07 hrs, Volume= 0.027 af, Depth> 5.97"



Summary for Subcatchment 31WP: 31 WP

Runoff = 0.40 cfs @ 12.07 hrs, Volume= 0.030 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment 33WP: 33 WP

Runoff = 0.46 cfs @ 12.07 hrs, Volume= 0.034 af, Depth> 5.97"



Summary for Subcatchment 88S: 8WS

Runoff = 0.36 cfs @ 12.07 hrs, Volume= 0.027 af, Depth> 5.97"

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Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=6.70"



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Summary for Subcatchment CEC: Central East - Campus

Runoff = 2.60 cfs @ 12.07 hrs, Volume= 0.196 af, Depth> 5.97"



Summary for Subcatchment CWC: Central West - Campus

Runoff = 5.47 cfs @ 12.07 hrs, Volume= 0.411 af, Depth> 5.97"

Area (sf)	CN Description						
36,000	98 Roofs, HSG A						
36,000	100.00% Impervious Area						
Tc Length (min) (feet)	Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs)						
5.0	Direct Entry,						
Subcatchment CWC: Central West - Campus							
6-							



Summary for Subcatchment ILC: IL Attached - Campus - 6 units (center)

Runoff = 2.60 cfs @ 12.07 hrs, Volume= 0.196 af, Depth> 5.97"



Summary for Subcatchment ILE: IL Attached - Campus - 3 units (east)

Runoff = 1.30 cfs @ 12.07 hrs, Volume= 0.098 af, Depth> 5.97"



Summary for Subcatchment ILW: IL Attached - Campus - 6 units (west)

Runoff = 2.58 cfs @ 12.07 hrs, Volume= 0.194 af, Depth> 5.97"



Summary for Subcatchment NC: North - Campus

Runoff = 4.82 cfs @ 12.07 hrs, Volume= 0.362 af, Depth> 5.97"



Summary for Pond IT 22: 20 CULTEC R-330XL

Inflow Area	ι =	0.190 ac,10	0.00% Impe	ervious,	Inflow Dep	oth >	5.97" fo	or 100-`	lear event	
Inflow	=	1.26 cfs @	12.07 hrs,	Volume	= 0).094 a	af			
Outflow	=	0.07 cfs @	13.69 hrs,	Volume	= C).067 a	af, Atten:	= 94%,	Lag= 97.3 m	nin
Discarded	=	0.07 cfs @	13.69 hrs,	Volume	= C).067 a	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.39' @ 13.69 hrs Surf.Area= 860 sf Storage= 2,006 cf

Plug-Flow detention time= 166.3 min calculated for 0.067 af (71% of inflow) Center-of-Mass det. time= 98.7 min (831.6 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	955 cf	22.33'W x 38.50'L x 4.04'H Field A
			3,475 cf Overall - 1,088 cf Embedded = 2,387 cf x 40.0% Voids
#2A	176.46'	1,088 cf	Cultec R-330XL x 20 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 4 rows
		2,043 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.07 cfs	© 13.69 hrs HW=179.39' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.07 cfs)

Pond IT 22: 20 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 4 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 4 Rows x 52.0" Wide + 12.0" Spacing x 3 + 12.0" Side Stone x 2 = 22.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

20 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 4 Rows = 1,087.8 cf Chamber Storage

3,475.2 cf Field - 1,087.8 cf Chambers = 2,387.3 cf Stone x 40.0% Voids = 954.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,042.8 cf = 0.047 af Overall Storage Efficiency = 58.8%

20 Chambers 128.7 cy Field 88.4 cy Stone







Pond IT 22: 20 CULTEC R-330XL

Summary for Pond IT10: 12 CULTEC R-330XL

Inflow Area	ι =	0.121 ac,10	0.00% Impe	ervious,	Inflow Depth >	5.97"	for 100-`	Year event	
Inflow	=	0.80 cfs @	12.07 hrs,	Volume	= 0.060	af			
Outflow	=	0.05 cfs @	13.48 hrs,	Volume	= 0.045	af, Att	ten= 94%,	Lag= 84.8 mi	n
Discarded	=	0.05 cfs @	13.48 hrs,	Volume	= 0.045	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 183.49' @ 13.48 hrs Surf.Area= 536 sf Storage= 1,260 cf

Plug-Flow detention time= 166.2 min calculated for 0.045 af (74% of inflow) Center-of-Mass det. time= 102.3 min (835.2 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	179.46'	602 cf	17.00'W x 31.50'L x 4.04'H Field A
			2,164 cf Overall - 659 cf Embedded = 1,505 cf x 40.0% Voids
#2A	180.46'	659 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,261 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	179.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.05 cfs	@ 13.48 hrs HW=183.49' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.05 cfs)

Pond IT10: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 659.4 cf Chamber Storage

2,164.3 cf Field - 659.4 cf Chambers = 1,504.9 cf Stone x 40.0% Voids = 602.0 cf Stone Storage

Chamber Storage + Stone Storage = 1,261.4 cf = 0.029 af Overall Storage Efficiency = 58.3%

12 Chambers 80.2 cy Field 55.7 cy Stone







Pond IT10: 12 CULTEC R-330XL

Summary for Pond IT11: 28 CULTEC R-330XL

Inflow Area	=	0.242 ac,10	0.00% Impervious,	Inflow Depth >	5.97" fo	r 100-Year event
Inflow	=	1.60 cfs @	12.07 hrs, Volume	.121	af	
Outflow	=	0.09 cfs @	13.74 hrs, Volume	= 0.087	af, Atten=	94%, Lag= 100.4 min
Discarded	=	0.09 cfs @	13.74 hrs, Volume	= 0.087	af	-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 182.30' @ 13.74 hrs Surf.Area= 1,207 sf Storage= 2,515 cf

Plug-Flow detention time= 163.0 min calculated for 0.087 af (72% of inflow) Center-of-Mass det. time= 97.6 min (830.6 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.98'	1,337 cf	38.33'W x 31.50'L x 4.04'H Field A
			4,880 cf Overall - 1,539 cf Embedded = 3,342 cf x 40.0% Voids
#2A	179.98'	1,539 cf	Cultec R-330XL x 28 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 7 rows
		2,875 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	178.98'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.09 cfs	@ 13.74 hrs HW=182.30' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.09 cfs)

Pond IT11: 28 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 7 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 7 Rows x 52.0" Wide + 12.0" Spacing x 6 + 12.0" Side Stone x 2 = 38.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

28 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 7 Rows = 1,538.6 cf Chamber Storage

4,880.3 cf Field - 1,538.6 cf Chambers = 3,341.7 cf Stone x 40.0% Voids = 1,336.7 cf Stone Storage

Chamber Storage + Stone Storage = 2,875.3 cf = 0.066 af Overall Storage Efficiency = 58.9%

28 Chambers 180.8 cy Field 123.8 cy Stone





8548.0 - Salmon Senior Community - Medway - PropType III 24-hr100-Year Rainfall=6.70"Prepared by MicrosoftPrinted 10/9/2015HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLCPage 445



Pond IT11: 28 CULTEC R-330XL

Summary for Pond IT11A: 6 CULTEC R-330XL

Inflow Area	a =	0.061 ac,10	0.00% Impe	ervious,	Inflow Depth >	5.97"	for 100-	Year event	
Inflow	=	0.40 cfs @	12.07 hrs,	Volume	= 0.030	af			
Outflow	=	0.03 cfs @	13.17 hrs,	Volume	= 0.024	af, At	tten= 93%,	Lag= 66.3 m	nin
Discarded	=	0.03 cfs @	13.17 hrs,	Volume	= 0.024	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 184.77' @ 13.17 hrs Surf.Area= 280 sf Storage= 606 cf

Plug-Flow detention time= 162.1 min calculated for 0.024 af (80% of inflow) Center-of-Mass det. time= 106.6 min (839.6 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	181.21'	314 cf	16.00'W x 17.50'L x 4.04'H Field A
			1,132 cf Overall - 346 cf Embedded = 785 cf x 40.0% Voids
#2A	182.21'	346 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		661 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	181.21'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.03 cfs	@ 13.17 hrs HW=184.77' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.03 cfs)

Pond IT11A: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

2 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 15.50' Row Length +12.0" End Stone x 2 = 17.50' Base Length 3 Rows x 52.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 16.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 346.5 cf Chamber Storage

1,131.7 cf Field - 346.5 cf Chambers = 785.2 cf Stone x 40.0% Voids = 314.1 cf Stone Storage

Chamber Storage + Stone Storage = 660.5 cf = 0.015 af Overall Storage Efficiency = 58.4%

6 Chambers 41.9 cy Field 29.1 cy Stone







Pond IT11A: 6 CULTEC R-330XL

Summary for Pond IT12: 14 CULTEC R-330XL

Inflow Area	ι =	0.129 ac,10	0.00% Impe	ervious,	Inflow Depth >	5.97	7" for 10	0-Year ev	rent
Inflow	=	0.86 cfs @	12.07 hrs,	Volume	= 0.06	4 af			
Outflow	=	0.06 cfs @	13.30 hrs,	Volume	= 0.05	0 af, 1	Atten= 93%	%, Lag= 7	'3.9 min
Discarded	=	0.06 cfs @	13.30 hrs,	Volume	= 0.05	0 af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 182.43' @ 13.30 hrs Surf.Area= 613 sf Storage= 1,302 cf

Plug-Flow detention time= 162.1 min calculated for 0.050 af (78% of inflow) Center-of-Mass det. time= 105.2 min (838.2 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.96'	689 cf	11.67'W x 52.50'L x 4.04'H Field A
			2,476 cf Overall - 753 cf Embedded = 1,723 cf x 40.0% Voids
#2A	179.96'	753 cf	Cultec R-330XL x 14 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,442 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	178.96'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.06 cfs	@ 13.30 hrs HW=182.43' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.06 cfs)

Pond IT12: 14 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

14 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 752.6 cf Chamber Storage

2,475.5 cf Field - 752.6 cf Chambers = 1,723.0 cf Stone x 40.0% Voids = 689.2 cf Stone Storage

Chamber Storage + Stone Storage = 1,441.7 cf = 0.033 af Overall Storage Efficiency = 58.2%

14 Chambers 91.7 cy Field 63.8 cy Stone







Pond IT12: 14 CULTEC R-330XL

Summary for Pond IT13: 12 CULTEC R-330XL

Inflow Area	a =	0.116 ac,10	0.00% Impe	ervious,	Inflow Depth >	5.97"	for 100-`	Year event	
Inflow	=	0.77 cfs @	12.07 hrs,	Volume	= 0.058	3 af			
Outflow	=	0.05 cfs @	13.28 hrs,	Volume	= 0.045	5 af, At	ten= 93%,	Lag= 72.9 n	nin
Discarded	=	0.05 cfs @	13.28 hrs,	Volume	= 0.045	5 af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.89' @ 13.28 hrs Surf.Area= 531 sf Storage= 1,171 cf

Plug-Flow detention time= 163.7 min calculated for 0.045 af (78% of inflow) Center-of-Mass det. time= 105.2 min (838.2 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.21'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	177.21'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.21'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.05 cfs	@ 13.28 hrs HW=179.89' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.05 cfs)

Pond IT13: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT13: 12 CULTEC R-330XL
Summary for Pond IT14: 12 CULTEC R-330XL

Inflow Area	a =	0.116 ac,10	0.00% Impe	ervious,	Inflow Depth >	5.97	" for 100-	Year event	
Inflow	=	0.77 cfs @	12.07 hrs,	Volume	= 0.058	af			
Outflow	=	0.05 cfs @	13.28 hrs,	Volume	= 0.045	af, A	Atten= 93%,	Lag= 72.9 n	nin
Discarded	=	0.05 cfs @	13.28 hrs,	Volume	= 0.045	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.64' @ 13.28 hrs Surf.Area= 531 sf Storage= 1,171 cf

Plug-Flow detention time= 163.7 min calculated for 0.045 af (78% of inflow) Center-of-Mass det. time= 105.2 min (838.2 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.96'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	176.96'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices				
#1	Discarded	175.96'	2.410 in/hr Exfiltration over Wetted area				
Discard	Discarded OutFlow Max=0.05 cfs @ 13.28 hrs HW=179.64' (Free Discharge)						

Pond IT14: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT14: 12 CULTEC R-330XL

Summary for Pond IT15: 14 CULTEC R-330XL

Inflow Area	ι =	0.129 ac,10	0.00% Impe	ervious,	Inflow Depth >	5.97	7" for 100-	Year event	
Inflow	=	0.86 cfs @	12.07 hrs,	Volume	= 0.064	1 af			
Outflow	=	0.06 cfs @	13.30 hrs,	Volume	= 0.050	Daf, A	Atten= 93%,	Lag= 73.9	min
Discarded	=	0.06 cfs @	13.30 hrs,	Volume	= 0.050) af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 180.13' @ 13.30 hrs Surf.Area= 613 sf Storage= 1,302 cf

Plug-Flow detention time= 162.1 min calculated for 0.050 af (78% of inflow) Center-of-Mass det. time= 105.2 min (838.2 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.66'	689 cf	11.67'W x 52.50'L x 4.04'H Field A
			2,476 cf Overall - 753 cf Embedded = 1,723 cf x 40.0% Voids
#2A	177.66'	753 cf	Cultec R-330XL x 14 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,442 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.66'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.06 cfs	@ 13.30 hrs HW=180.13' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.06 cfs)

Pond IT15: 14 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

7 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 50.50' Row Length +12.0" End Stone x 2 = 52.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

14 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 752.6 cf Chamber Storage

2,475.5 cf Field - 752.6 cf Chambers = 1,723.0 cf Stone x 40.0% Voids = 689.2 cf Stone Storage

Chamber Storage + Stone Storage = 1,441.7 cf = 0.033 af Overall Storage Efficiency = 58.2%

14 Chambers 91.7 cy Field 63.8 cy Stone







Pond IT15: 14 CULTEC R-330XL

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Summary for Pond IT16: 45 - 330XL

Inflow Area	I =	0.394 ac,10	0.00% Impervious,	Inflow Depth >	5.97" for	100-Year event
Inflow	=	2.60 cfs @	12.07 hrs, Volume	= 0.196	af	
Outflow	=	0.14 cfs @	13.89 hrs, Volume	= 0.134	af, Atten= 9	95%, Lag= 109.1 min
Discarded	=	0.14 cfs @	13.89 hrs, Volume	≔ 0.134	af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.22' @ 13.89 hrs Surf.Area= 1,840 sf Storage= 4,212 cf

Plug-Flow detention time= 164.2 min calculated for 0.133 af (68% of inflow) Center-of-Mass det. time= 94.2 min (827.1 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	2,013 cf	27.67'W x 66.50'L x 4.04'H Field A
			7,436 cf Overall - 2,403 cf Embedded = 5,033 cf x 40.0% Voids
#2A	176.46'	2,403 cf	Cultec R-330XL x 45 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 5 rows
		4,416 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.14 cfs	@ 13.89 hrs HW=179.22' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.14 cfs)

Pond IT16: 45 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 5 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 5 Rows x 52.0" Wide + 12.0" Spacing x 4 + 12.0" Side Stone x 2 = 27.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

45 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 5 Rows = 2,402.9 cf Chamber Storage

7,436.0 cf Field - 2,402.9 cf Chambers = 5,033.0 cf Stone x 40.0% Voids = 2,013.2 cf Stone Storage

Chamber Storage + Stone Storage = 4,416.2 cf = 0.101 af Overall Storage Efficiency = 59.4%

45 Chambers 275.4 cy Field 186.4 cy Stone





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Pond IT16: 45 - 330XL

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Summary for Pond IT17: 24 - 330XL

Inflow Area	a =	0.197 ac,10	0.00% Impe	ervious,	Inflow Depth >	5.97	" for 100)-Year event	
Inflow	=	1.30 cfs @	12.07 hrs,	Volume	= 0.098	af			
Outflow	=	0.08 cfs @	13.62 hrs,	Volume	= 0.074	af, A	tten= 94%	, Lag= 92.8	min
Discarded	=	0.08 cfs @	13.62 hrs,	Volume	= 0.074	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 175.98' @ 13.62 hrs Surf.Area= 1,040 sf Storage= 1,990 cf

Plug-Flow detention time= 161.4 min calculated for 0.073 af (75% of inflow) Center-of-Mass det. time= 100.2 min (833.2 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	172.96'	1,153 cf	33.00'W x 31.50'L x 4.04'H Field A
			4,201 cf Overall - 1,319 cf Embedded = 2,882 cf x 40.0% Voids
#2A	173.96'	1,319 cf	Cultec R-330XL x 24 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		2,472 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	172.96'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.08 cfs	@ 13.62 hrs HW=175.98' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond IT17: 24 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

24 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 1,318.8 cf Chamber Storage

4,201.3 cf Field - 1,318.8 cf Chambers = 2,882.5 cf Stone x 40.0% Voids = 1,153.0 cf Stone Storage

Chamber Storage + Stone Storage = 2,471.8 cf = 0.057 af Overall Storage Efficiency = 58.8%

24 Chambers 155.6 cy Field 106.8 cy Stone





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Pond IT17: 24 - 330XL

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Summary for Pond IT18: 48 - 330XL

Inflow Area	=	0.394 ac,10	0.00% Imperviou	us, Inflow De	epth > 5	5.97" for	100-Year ev	vent
Inflow	=	2.60 cfs @	12.07 hrs, Volu	me=	0.196 a	f		
Outflow	=	0.14 cfs @	13.86 hrs, Volu	me=	0.137 a	f, Atten= 9	94%, Lag= [·]	107.5 min
Discarded	=	0.14 cfs @	13.86 hrs, Volu	me=	0.137 a	f	-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 176.78' @ 13.86 hrs Surf.Area= 1,964 sf Storage= 4,137 cf

Plug-Flow detention time= 163.6 min calculated for 0.137 af (70% of inflow) Center-of-Mass det. time= 94.7 min (827.7 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	173.46'	2,146 cf	33.00'W x 59.50'L x 4.04'H Field A
			7,936 cf Overall - 2,571 cf Embedded = 5,365 cf x 40.0% Voids
#2A	174.46'	2,571 cf	Cultec R-330XL x 48 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		4,717 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	173.46'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.14 cfs	@ 13.86 hrs HW=176.78' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.14 cfs)

Pond IT18: 48 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

48 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 2,570.6 cf Chamber Storage

7,935.8 cf Field - 2,570.6 cf Chambers = 5,365.2 cf Stone x 40.0% Voids = 2,146.1 cf Stone Storage

Chamber Storage + Stone Storage = 4,716.7 cf = 0.108 af Overall Storage Efficiency = 59.4%

48 Chambers 293.9 cy Field 198.7 cy Stone





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Pond IT18: 48 - 330XL

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Summary for Pond IT19: 48 - 330XL

Inflow Area	a =	0.390 ac,10	0.00% Impervious	, Inflow Depth >	5.97" 1	for 100-`	Year event
Inflow	=	2.58 cfs @	12.07 hrs, Volum	e= 0.194	l af		
Outflow	=	0.14 cfs @	13.85 hrs, Volum	e= 0.137	af, Atter	n= 94%,	Lag= 106.8 min
Discarded	=	0.14 cfs @	13.85 hrs, Volum	e= 0.137	' af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 174.52' @ 13.85 hrs Surf.Area= 1,964 sf Storage= 4,087 cf

Plug-Flow detention time= 162.5 min calculated for 0.136 af (70% of inflow) Center-of-Mass det. time= 95.0 min (828.0 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	171.25'	2,146 cf	33.00'W x 59.50'L x 4.04'H Field A
			7,936 cf Overall - 2,571 cf Embedded = 5,365 cf x 40.0% Voids
#2A	172.25'	2,571 cf	Cultec R-330XL x 48 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 6 rows
		4,717 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	171.25'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.14 cfs	@ 13.85 hrs_HW=174.52' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.14 cfs)

Pond IT19: 48 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 6 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 6 Rows x 52.0" Wide + 12.0" Spacing x 5 + 12.0" Side Stone x 2 = 33.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

48 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 6 Rows = 2,570.6 cf Chamber Storage

7,935.8 cf Field - 2,570.6 cf Chambers = 5,365.2 cf Stone x 40.0% Voids = 2,146.1 cf Stone Storage

Chamber Storage + Stone Storage = 4,716.7 cf = 0.108 af Overall Storage Efficiency = 59.4%

48 Chambers 293.9 cy Field 198.7 cy Stone





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Pond IT19: 48 - 330XL

Summary for Pond IT20: 100 - 330XL

Inflow Area	=	0.826 ac,10	0.00% Impervious	, Inflow Depth >	5.97" f	or 100-۱	ear event
Inflow	=	5.47 cfs @	12.07 hrs, Volum	e= 0.411	l af		
Outflow	=	0.27 cfs @	14.08 hrs, Volume	e= 0.269	9 af, Atten	i= 95%,	Lag= 120.6 min
Discarded	=	0.27 cfs @	14.08 hrs, Volume	e= 0.269	9 af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.07' @ 14.08 hrs Surf.Area= 3,994 sf Storage= 8,956 cf

Plug-Flow detention time= 162.1 min calculated for 0.268 af (65% of inflow) Center-of-Mass det. time= 88.8 min (821.7 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	4,325 cf	54.33'W x 73.50'L x 4.04'H Field A
			16,140 cf Overall - 5,327 cf Embedded = 10,813 cf x 40.0% Voids
#2A	176.46'	5,327 cf	Cultec R-330XL x 100 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 10 rows
		9,653 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area	
Discarded OutFlow Max=0.27 cfs @ 14.08 hrs HW=179.07' (Free Discharge) 				

Pond IT20: 100 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 10 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

10 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 71.50' Row Length +12.0" End Stone x 2 = 73.50' Base Length 10 Rows x 52.0" Wide + 12.0" Spacing x 9 + 12.0" Side Stone x 2 = 54.33' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

100 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 10 Rows = 5,327.5 cf Chamber Storage

16,140.4 cf Field - 5,327.5 cf Chambers = 10,812.9 cf Stone x 40.0% Voids = 4,325.2 cf Stone Storage

Chamber Storage + Stone Storage = 9,652.6 cf = 0.222 af Overall Storage Efficiency = 59.8%

100 Chambers 597.8 cy Field 400.5 cy Stone





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Pond IT20: 100 - 330XL

Summary for Pond IT21: 25 CULTEC R-330XL

Inflow Area	=	0.237 ac,10	0.00% Impervious,	Inflow Depth >	5.97" for	100-Year event
Inflow	=	1.57 cfs @	12.07 hrs, Volume	e 0.118	af	
Outflow	=	0.09 cfs @	13.80 hrs, Volume	⇒ 0.082	af, Atten=	94%, Lag= 103.5 min
Discarded	=	0.09 cfs @	13.80 hrs, Volume	⊭ 0.082	af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 173.72' @ 13.80 hrs Surf.Area= 1,065 sf Storage= 2,531 cf

Plug-Flow detention time= 165.4 min calculated for 0.081 af (69% of inflow) Center-of-Mass det. time= 96.5 min (829.5 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	169.69'	1,178 cf	27.67'W x 38.50'L x 4.04'H Field A
			4,305 cf Overall - 1,360 cf Embedded = 2,945 cf x 40.0% Voids
#2A	170.69'	1,360 cf	Cultec R-330XL x 25 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 5 rows
		2,538 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	169.69'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.09 cfs	@ 13.80 hrs HW=173.72' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.09 cfs)

Pond IT21: 25 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 5 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 5 Rows x 52.0" Wide + 12.0" Spacing x 4 + 12.0" Side Stone x 2 = 27.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

25 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 5 Rows = 1,359.8 cf Chamber Storage

4,305.0 cf Field - 1,359.8 cf Chambers = 2,945.2 cf Stone x 40.0% Voids = 1,178.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,537.9 cf = 0.058 af Overall Storage Efficiency = 59.0%

25 Chambers 159.4 cy Field 109.1 cy Stone





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Pond IT21: 25 CULTEC R-330XL

Summary for Pond IT22A: 6 CULTEC R-330XL

Inflow Area	ι =	0.055 ac,10	0.00% Impe	ervious,	Inflow [Depth >	5.97"	for	100-Y	'ear eve	nt
Inflow	=	0.36 cfs @	12.07 hrs,	Volume	=	0.027	af				
Outflow	=	0.03 cfs @	12.93 hrs,	Volume	=	0.025	af, Atte	en= 9	1%, l	_ag= 51	.6 min
Discarded	=	0.03 cfs @	12.93 hrs,	Volume	=	0.025	af				

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 180.24' @ 12.93 hrs Surf.Area= 288 sf Storage= 512 cf

Plug-Flow detention time= 143.9 min calculated for 0.025 af (90% of inflow) Center-of-Mass det. time= 108.7 min (841.7 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	177.46'	279 cf	6.33'W x 45.50'L x 3.54'H Field A
			1,021 cf Overall - 324 cf Embedded = 696 cf x 40.0% Voids
#2A	177.96'	324 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 1 rows
		603 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	177.46'	2.410 in/hr Exfiltration over Wetted area	
Discard	ed OutFlow M filtration (Ext	Max=0.03 cfs filtration Cont	@ 12.93 hrs HW=180.24' (Free Discharge) rols 0.03 cfs)	

Pond IT22A: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 1 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 1 Rows x 52.0" Wide + 12.0" Side Stone x 2 = 6.33' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 1 Rows = 324.1 cf Chamber Storage

1,020.6 cf Field - 324.1 cf Chambers = 696.5 cf Stone x 40.0% Voids = 278.6 cf Stone Storage

Chamber Storage + Stone Storage = 602.7 cf = 0.014 af Overall Storage Efficiency = 59.1%

6 Chambers 37.8 cy Field 25.8 cy Stone







Pond IT22A: 6 CULTEC R-330XL

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Summary for Pond IT23: 88 - 330XL

Inflow Area	ι =	0.729 ac,10	0.00% Impervious,	Inflow Depth >	5.97" for	100-Year event
Inflow	=	4.82 cfs @	12.07 hrs, Volume	e 0.362	af	
Outflow	=	0.25 cfs @	14.05 hrs, Volume	e= 0.240	af, Atten=	95%, Lag= 118.6 min
Discarded	=	0.25 cfs @	14.05 hrs, Volume	e= 0.240	af	-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.00' @ 14.05 hrs Surf.Area= 3,550 sf Storage= 7,859 cf

Plug-Flow detention time= 162.2 min calculated for 0.239 af (66% of inflow) Center-of-Mass det. time= 89.6 min (822.6 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	175.46'	3,854 cf	59.67'W x 59.50'L x 4.04'H Field A
			14,349 cf Overall - 4,713 cf Embedded = 9,636 cf x 40.0% Voids
#2A	176.46'	4,713 cf	Cultec R-330XL x 88 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 11 rows
		8,567 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices				
#1	Discarded	175.46'	2.410 in/hr Exfiltration over Wetted area				
Discarded OutFlow Max=0.25 cfs @ 14.05 hrs HW=179.00' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.25 cfs)							

Pond IT23: 88 - 330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 11 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

8 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 57.50' Row Length +12.0" End Stone x 2 = 59.50' Base Length 11 Rows x 52.0" Wide + 12.0" Spacing x 10 + 12.0" Side Stone x 2 = 59.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

88 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 11 Rows = 4,712.8 cf Chamber Storage

14,348.6 cf Field - 4,712.8 cf Chambers = 9,635.8 cf Stone x 40.0% Voids = 3,854.3 cf Stone Storage

Chamber Storage + Stone Storage = 8,567.1 cf = 0.197 af Overall Storage Efficiency = 59.7%

88 Chambers 531.4 cy Field 356.9 cy Stone





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Pond IT23: 88 - 330XL

Summary for Pond IT24: 8 CULTEC R-330XL

Inflow Area	1 =	0.069 ac,10	0.00% Impe	ervious,	Inflow Depth >	5.97	" for 100-`	Year event
Inflow	=	0.46 cfs @	12.07 hrs,	Volume	= 0.034	af		
Outflow	=	0.03 cfs @	13.13 hrs,	Volume	= 0.028	8 af, A	tten= 93%,	Lag= 63.6 min
Discarded	=	0.03 cfs @	13.13 hrs,	Volume	= 0.028	8 af		-

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.12' @ 13.13 hrs Surf.Area= 352 sf Storage= 672 cf

Plug-Flow detention time= 157.6 min calculated for 0.028 af (82% of inflow) Center-of-Mass det. time= 105.7 min (838.7 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.21'	322 cf	11.17'W x 31.50'L x 3.54'H Field A
			1,246 cf Overall - 440 cf Embedded = 806 cf x 40.0% Voids
#2A	176.71'	440 cf	Cultec R-330XL x 8 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		762 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.21'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.03 cfs	@ 13.13 hrs HW=179.12' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.03 cfs)

Pond IT24: 8 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

4 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 29.50' Row Length +12.0" End Stone x 2 = 31.50' Base Length 2 Rows x 52.0" Wide + 6.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.17' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

8 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 439.6 cf Chamber Storage

1,245.8 cf Field - 439.6 cf Chambers = 806.2 cf Stone x 40.0% Voids = 322.5 cf Stone Storage

Chamber Storage + Stone Storage = 762.1 cf = 0.017 afOverall Storage Efficiency = 61.2%

8 Chambers 46.1 cy Field 29.9 cy Stone







Pond IT24: 8 CULTEC R-330XL

Summary for Pond IT25: 12 CULTEC R-330XL

Inflow Area	ι =	0.121 ac,10	0.00% Impe	ervious,	Inflow Depth >	· 5.97	7" for 1	00-Year e	vent
Inflow	=	0.80 cfs @	12.07 hrs,	Volume	= 0.06	0 af			
Outflow	=	0.06 cfs @	13.30 hrs,	Volume	= 0.04	6 af, 7	Atten= 93	8%, Lag=	74.0 min
Discarded	=	0.06 cfs @	13.30 hrs,	Volume	= 0.04	6 af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 191.48' @ 13.30 hrs Surf.Area= 531 sf Storage= 1,242 cf

Plug-Flow detention time= 164.2 min calculated for 0.046 af (76% of inflow) Center-of-Mass det. time= 104.7 min (837.7 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	187.46'	599 cf	11.67'W x 45.50'L x 4.04'H Field A
			2,145 cf Overall - 648 cf Embedded = 1,497 cf x 40.0% Voids
#2A	188.46'	648 cf	Cultec R-330XL x 12 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		1,247 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	187.46'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow	Max=0.06 cfs	@ 13.30 hrs HW=191.48' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.06 cfs)

Pond IT25: 12 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

12 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 648.2 cf Chamber Storage

2,145.5 cf Field - 648.2 cf Chambers = 1,497.2 cf Stone x 40.0% Voids = 598.9 cf Stone Storage

Chamber Storage + Stone Storage = 1,247.1 cf = 0.029 af Overall Storage Efficiency = 58.1%

12 Chambers 79.5 cy Field 55.5 cy Stone







Pond IT25: 12 CULTEC R-330XL
Summary for Pond IT26: 18 CULTEC R-330XL

Inflow Area	ι =	0.171 ac,10	0.00% Imp	ervious,	Inflow Depth >	5.9	7" for	100-Y	ear event	t
Inflow	=	1.13 cfs @	12.07 hrs,	Volume	= 0.08	5 af				
Outflow	=	0.07 cfs @	13.58 hrs,	Volume	= 0.062	2 af, 7	Atten= 9	94%, I	Lag= 90.7	' min
Discarded	=	0.07 cfs @	13.58 hrs,	Volume	= 0.062	2 af				

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 186.73' @ 13.58 hrs Surf.Area= 774 sf Storage= 1,782 cf

Plug-Flow detention time= 166.0 min calculated for 0.062 af (73% of inflow) Center-of-Mass det. time= 100.8 min (833.7 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	182.86'	862 cf	17.00'W x 45.50'L x 4.04'H Field A
			3,126 cf Overall - 972 cf Embedded = 2,154 cf x 40.0% Voids
#2A	183.86'	972 cf	Cultec R-330XL x 18 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,834 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	182.86'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.07 cfs	a@ 13.58 hrs HW=186.73' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.07 cfs)

Pond IT26: 18 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

6 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 43.50' Row Length +12.0" End Stone x 2 = 45.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

18 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 972.4 cf Chamber Storage

3,126.2 cf Field - 972.4 cf Chambers = 2,153.9 cf Stone x 40.0% Voids = 861.5 cf Stone Storage

Chamber Storage + Stone Storage = 1,833.9 cf = 0.042 af Overall Storage Efficiency = 58.7%

18 Chambers 115.8 cy Field 79.8 cy Stone





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Pond IT26: 18 CULTEC R-330XL

Summary for Pond IT29: 27 CULTEC R-330XL

Inflow Area	I =	0.242 ac,10	0.00% Impe	ervious,	Inflow	Depth >	5.97"	for 100-`	Year event	
Inflow	=	1.60 cfs @	12.07 hrs,	Volume	=	0.121	af			
Outflow	=	0.10 cfs @	13.64 hrs,	Volume	=	0.087	af, Att	ten= 94%,	Lag= 94.2	min
Discarded	=	0.10 cfs @	13.64 hrs,	Volume	=	0.087	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 187.13' @ 13.64 hrs Surf.Area= 1,131 sf Storage= 2,527 cf

Plug-Flow detention time= 165.5 min calculated for 0.087 af (73% of inflow) Center-of-Mass det. time= 99.8 min (832.7 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	183.46'	1,251 cf	17.00'W x 66.50'L x 4.04'H Field A
			4,569 cf Overall - 1,442 cf Embedded = 3,127 cf x 40.0% Voids
#2A	184.46'	1,442 cf	Cultec R-330XL x 27 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		2,693 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	183.46'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.10 cfs	@ 13.64 hrs HW=187.13' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.10 cfs)

Pond IT29: 27 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

27 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 1,441.8 cf Chamber Storage

4,569.1 cf Field - 1,441.8 cf Chambers = 3,127.3 cf Stone x 40.0% Voids = 1,250.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,692.7 cf = 0.062 af Overall Storage Efficiency = 58.9%

27 Chambers 169.2 cy Field 115.8 cy Stone







Pond IT29: 27 CULTEC R-330XL

Summary for Pond IT30: 15 CULTEC R-330XL

Inflow Area	a =	0.116 ac,10	0.00% Impe	ervious,	Inflow Depth >	5.97	" for 10	00-Year ev	/ent
Inflow	=	0.77 cfs @	12.07 hrs,	Volume	= 0.058	af			
Outflow	=	0.05 cfs @	13.27 hrs,	Volume	= 0.047	af, A	tten= 93	%, Lag=7	2.0 min
Discarded	=	0.05 cfs @	13.27 hrs,	Volume	= 0.047	af		-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 183.68' @ 13.27 hrs Surf.Area= 655 sf Storage= 1,116 cf

Plug-Flow detention time= 157.4 min calculated for 0.047 af (82% of inflow) Center-of-Mass det. time= 106.0 min (839.0 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	180.96'	732 cf	17.00'W x 38.50'L x 4.04'H Field A
			2,645 cf Overall - 816 cf Embedded = 1,829 cf x 40.0% Voids
#2A	181.96'	816 cf	Cultec R-330XL x 15 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		1,548 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	180.96'	2.410 in/hr Exfiltration over Wetted area	_
Discard	ed OutFlow M filtration (Exf	Max=0.05 cfs	@ 13.27 hrs HW=183.68' (Free Discharge) trols 0.05 cfs)	

Pond IT30: 15 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

5 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 36.50' Row Length +12.0" End Stone x 2 = 38.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

15 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 815.9 cf Chamber Storage

2,645.3 cf Field - 815.9 cf Chambers = 1,829.4 cf Stone x 40.0% Voids = 731.8 cf Stone Storage

Chamber Storage + Stone Storage = 1,547.6 cf = 0.036 af Overall Storage Efficiency = 58.5%

15 Chambers 98.0 cy Field 67.8 cy Stone







Pond IT30: 15 CULTEC R-330XL

Summary for Pond IT31: 27 CULTEC R-330XL

Inflow Area	I =	0.237 ac,10	0.00% Impe	ervious,	Inflow	Depth >	5.97'	' for 100-	Year eve	nt
Inflow	=	1.57 cfs @	12.07 hrs,	Volume	=	0.118	af			
Outflow	=	0.10 cfs @	13.62 hrs,	Volume	=	0.086	af, A	tten= 94%,	Lag= 93	.2 min
Discarded	=	0.10 cfs @	13.62 hrs,	Volume	=	0.086	af			

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 179.97' @ 13.62 hrs Surf.Area= 1,131 sf Storage= 2,451 cf

Plug-Flow detention time= 164.0 min calculated for 0.086 af (73% of inflow) Center-of-Mass det. time= 100.2 min (833.2 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	176.46'	1,251 cf	17.00'W x 66.50'L x 4.04'H Field A
			4,569 cf Overall - 1,442 cf Embedded = 3,127 cf x 40.0% Voids
#2A	177.46'	1,442 cf	Cultec R-330XL x 27 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		2,693 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	176.46'	2.410 in/hr Exfiltration over Wetted area
Discard	led OutFlow	Max=0.10 cfs	@ 13.62 hrs HW=179.97' (Free Discharge)

1=Exfiltration (Exfiltration Controls 0.10 cfs)

Pond IT31: 27 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

9 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 64.50' Row Length +12.0" End Stone x 2 = 66.50' Base Length 3 Rows x 52.0" Wide + 12.0" Spacing x 2 + 12.0" Side Stone x 2 = 17.00' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

27 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 1,441.8 cf Chamber Storage

4,569.1 cf Field - 1,441.8 cf Chambers = 3,127.3 cf Stone x 40.0% Voids = 1,250.9 cf Stone Storage

Chamber Storage + Stone Storage = 2,692.7 cf = 0.062 af Overall Storage Efficiency = 58.9%

27 Chambers 169.2 cy Field 115.8 cy Stone





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Pond IT31: 27 CULTEC R-330XL

Summary for Pond IT8: 20 CULTEC R-330XL

Inflow Area	a =	0.182 ac,10	0.00% Impe	ervious,	Inflow Depth >	> 5.9	7" for	100-\	lear ev	ent
Inflow	=	1.20 cfs @	12.07 hrs,	Volume	= 0.09	0 af				
Outflow	=	0.08 cfs @	13.36 hrs,	Volume	= 0.07	0 af,	Atten= 9	93%,	Lag= 7	7.6 min
Discarded	=	0.08 cfs @	13.36 hrs,	Volume	= 0.07	0 af				

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 181.21' @ 13.36 hrs Surf.Area= 858 sf Storage= 1,840 cf

Plug-Flow detention time= 162.8 min calculated for 0.070 af (77% of inflow) Center-of-Mass det. time= 104.4 min (837.4 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	177.71'	960 cf	11.67'W x 73.50'L x 4.04'H Field A
			3,466 cf Overall - 1,065 cf Embedded = 2,400 cf x 40.0% Voids
#2A	178.71'	1,065 cf	Cultec R-330XL x 20 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 2 rows
		2,026 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices	
#1	Discarded	177.71'	2.410 in/hr Exfiltration over Wetted area	
Discard	led OutFlow	Max=0.08 cfs	@ 13.36 hrs HW=181.21' (Free Discharge)	

1=Exfiltration (Exfiltration Controls 0.08 cfs)

Pond IT8: 20 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 2 rows

52.0" Wide + 12.0" Spacing = 64.0" C-C Row Spacing

10 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 71.50' Row Length +12.0" End Stone x 2 = 73.50' Base Length 2 Rows x 52.0" Wide + 12.0" Spacing x 1 + 12.0" Side Stone x 2 = 11.67' Base Width 12.0" Base + 30.5" Chamber Height + 6.0" Cover = 4.04' Field Height

20 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 2 Rows = 1,065.5 cf Chamber Storage

3,465.7 cf Field - 1,065.5 cf Chambers = 2,400.2 cf Stone x 40.0% Voids = 960.1 cf Stone Storage

Chamber Storage + Stone Storage = 2,025.6 cf = 0.047 af Overall Storage Efficiency = 58.4%

20 Chambers 128.4 cy Field 88.9 cy Stone





8548.0 - Salmon Senior Community - Medway - PropType III 24-hr100-Year Rainfall=6.70"Prepared by MicrosoftPrinted 10/9/2015HydroCAD® 10.00 s/n 03074 © 2013 HydroCAD Software Solutions LLCPage 505



Pond IT8: 20 CULTEC R-330XL

Summary for Pond IT9: 6 CULTEC R-330XL

Inflow Area	a =	0.055 ac,10	0.00% Impe	ervious,	Inflow Depth	າ> 5.9	97" for	100-Y	ear event	t
Inflow	=	0.36 cfs @	12.07 hrs,	Volume	= 0.0)27 af				
Outflow	=	0.03 cfs @	13.14 hrs,	Volume	= 0.0)22 af,	Atten= 9	33% , I	Lag= 64.2	min
Discarded	=	0.03 cfs @	13.14 hrs,	Volume	= 0.0)22 af			-	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 181.91' @ 13.14 hrs Surf.Area= 280 sf Storage= 539 cf

Plug-Flow detention time= 157.2 min calculated for 0.022 af (81% of inflow) Center-of-Mass det. time= 105.5 min (838.5 - 733.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	178.96'	258 cf	16.00'W x 17.50'L x 3.54'H Field A
			992 cf Overall - 346 cf Embedded = 645 cf x 40.0% Voids
#2A	179.46'	346 cf	Cultec R-330XL x 6 Inside #1
			Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf
			Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap
			Row Length Adjustment= +1.50' x 7.45 sf x 3 rows
		605 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	178.96'	2.410 in/hr Exfiltration over Wetted area
Discard	ed OutFlow M filtration (Exf	/lax=0.03 cfs	@ 13.14 hrs HW=181.91' (Free Discharge) trols 0.03 cfs)

Pond IT9: 6 CULTEC R-330XL - Chamber Wizard Field A

Chamber Model = Cultec R-330XL

Effective Size= 47.8"W x 30.0"H => 7.45 sf x 7.00'L = 52.2 cf Overall Size= 52.0"W x 30.5"H x 8.50'L with 1.50' Overlap Row Length Adjustment= +1.50' x 7.45 sf x 3 rows

52.0" Wide + 6.0" Spacing = 58.0" C-C Row Spacing

2 Chambers/Row x 7.00' Long +1.50' Row Adjustment = 15.50' Row Length +12.0" End Stone x 2 = 17.50' Base Length 3 Rows x 52.0" Wide + 6.0" Spacing x 2 + 12.0" Side Stone x 2 = 16.00' Base Width 6.0" Base + 30.5" Chamber Height + 6.0" Cover = 3.54' Field Height

6 Chambers x 52.2 cf +1.50' Row Adjustment x 7.45 sf x 3 Rows = 346.5 cf Chamber Storage

991.7 cf Field - 346.5 cf Chambers = 645.2 cf Stone x 40.0% Voids = 258.1 cf Stone Storage

Chamber Storage + Stone Storage = 604.5 cf = 0.014 afOverall Storage Efficiency = 61.0%

6 Chambers 36.7 cy Field 23.9 cy Stone







Pond IT9: 6 CULTEC R-330XL